

# VATNAJÖKULL:

**Mass balance, meltwater  
drainage and surface  
velocity of the glacial  
year 2022-23**



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## Mass balance, meltwater drainage and surface velocity of the glacial year 2022-23

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### Dagsetning

Febrúar 2024

# Lykilsíða

|                    |  |            |                           |
|--------------------|--|------------|---------------------------|
| Skýrsla LV nr      | LV-2024-010  | Dagsetning | Febrúar 2024              |
| Fjöldi Síðna       | 0  | Upplag     | 1                         |
| Dreifing           | [ x] Birt á vef LV   | [X] Opin   | [ ] Takmörkuð til [Dags.] |
| Titill             | VATNAJÖKULL: Mass balance, meltwater drainage and surface velocity of the glacial year 2022-23   |            |                           |
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| Verkefnisstjóri    | Andri Gunnarsson   |            |                           |
| Unnið fyrir        | Landsvirkjun   |            |                           |
| Samvinnuaðilar     | —  |            |                           |
| Útdráttur          | Afkoma Vatnajökuls jökulárið 2022-2023 var neikvæð, -1,01 m að vatnsgildi eða nærrí tvöfalt meira massatap en í meðalári frá upphafi mælinga. Þetta má að hluta rekja til lítillar vetrarafkomu sem var um 0,26 m undir meðaltali. Fyrri hluti sumars var fremur hlýr og bjartur á austurhluta Vatnajökuls. Sumarleysing var nærrí meðaltali á safnsvæðum Vatnajökuls en vel yfir meðallagi á leysingarsvæðum. Leysing á Vatnajökli mældist um 18% umfram meðallag og sumar afkoma jökulsins 2023 reiknaðist -2,5 m eða um 0,4 m undir meðaltali mælitímabilsins 1997–2022, sem er -2,1 m. |            |                           |
| Lykilorð           | Afkoma, Vatnajökull, leysing, jöklar   |            |                           |

Samþykki verkefnisstjóra  
Landsvirkjunar



# VATNAJÖKULL: Mass balance, meltwater drainage and surface velocity of the glacial year 2022\_23



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RH-02-23



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## 1. INTRODUCTION

In 1992 (glacial year 1991\_92) a program of surface mass balance measurements was started for Vatnajökull by the Science Institute University of Iceland (now Institute of Earth Sciences, IES) in collaboration with the National Power Company (NPC). For the first year the program was limited to the western part of the glacier, but then expanded to include the northern outlets as well. In 1996 this study was further expanded to include southern outlets, with support from The European Union (Framework IV - Environment and Climate, TEMBA project 1996-1997). This program was extended 1998–2000 with further support from EU (Framework IV - Environment and Climate, ICEMASS project, 1998-2000). In 2000-2002 NPC and IES continued the program. In 2003-2005 IES participated in a multinational research project, which was financially supported by The European Union (EVK2-CT-2002-00152 SPICE). IES was responsible for obtaining data sets for calibration of models of the mass balance and dynamics of Vatnajökull. This work was also supported by The National Power Company of Iceland and The National Road Authority and was a continuation of the TEMBA-project of 1996-97 and ICEMASS project 1998-2001.

Since then, IES and NPC have continued a similar program. Mass balance measurements on the southeast outlet Breiðamerkurjökull is financially supported by the National Road Authority.

The aim of the collaborative work of NPC and IES is to improve understanding of the mass balance and melt water runoff from glaciers. This work in combination with energy balance measurements by NPC and IES on Vatnajökull will be used for calibration of models of the surface energy and mass balance of Vatnajökull.

This report describes the field measurements, mass balance, melt water runoff and GNSS survey, for the glaciological year 2022\_23.

## 2. DIARY

May 2-8, 31, June 1-2: measurements of the winter balance, setup of AWSs.

June 21-22: installation of melt wires and maintenance of the lower AWS on Breiðamerkurjökull.

September 12, October 22- 27: summer balance measurements, take down of AWSs;

In all expeditions the locations of mass balance stakes were measured with Kinematic GPS (or fast static GPS) for surface velocity calculation.

The following members of staff of the Institute of Earth Sciences, University of Iceland, carried out the fieldwork on Vatnajökull: Finnur Pálsson, Sveinbjörn Steinþórsson, Eyjólfur Magnússon, Þorsteinn Sæmundsson with Andri Gunnarsson and Steinunn Helgadóttir (National Power Company), Hlynur Skagfjörð (Reykjavík Rescue Team) and Andri Björnsson.

Volunteers in the Iceland Glaciological Society Spring expedition to Vatnajökull helped in the field work in June.

### **3. MASS BALANCE MEASUREMENTS**

The purpose of the mass balance measurements is to describe the temporal and spatial distribution of the components of the mass balance. The mean annual values of the components and their variation from year to year are analyzed and related to meteorological conditions and climatic variability. The results are used in studies of changes in the glacier volume, estimates of meltwater contribution to glacial rivers, mass balance modeling, evaluation of altitudinal and regional variations of mass balance in response to climatic variations, and to assess the hydrometeorological and dynamic response of the ice cap to climate change.

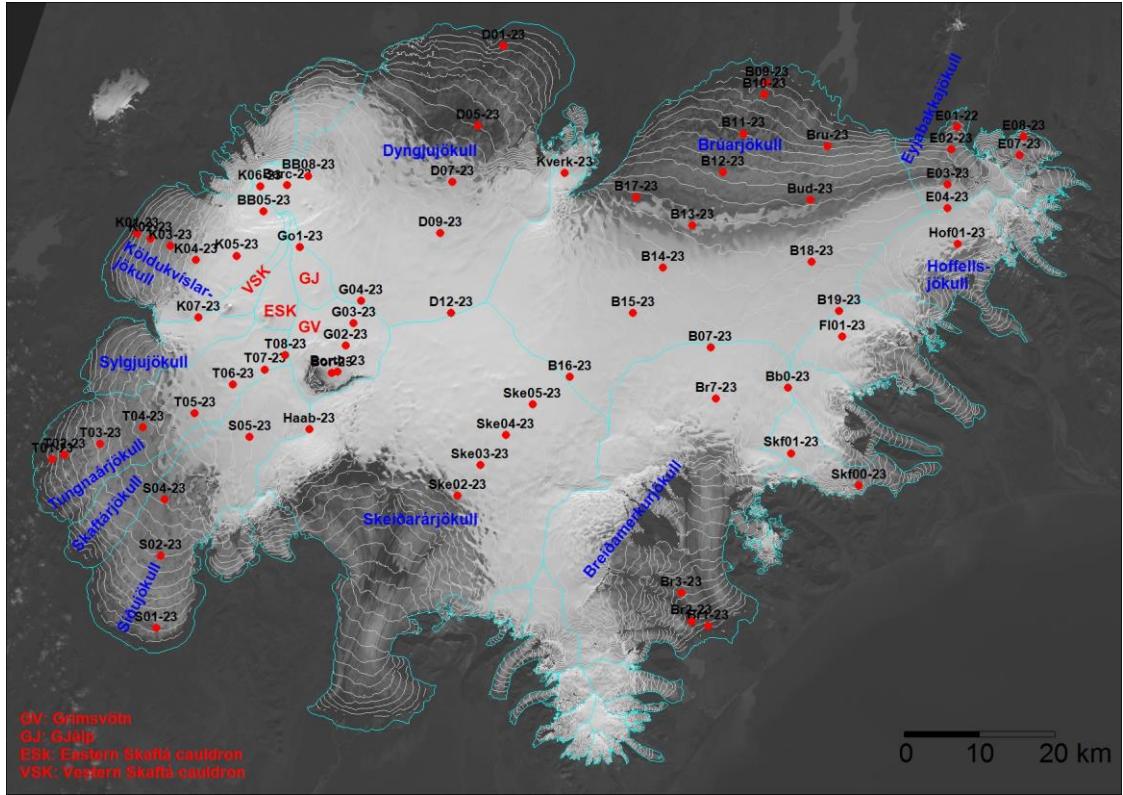
The mass balance was determined by a stratigraphic method, measuring changes in thickness and density relative to the summer surface. The winter balance was estimated by drilling ice cores through the winter layer in the spring. Ablation was monitored from markers; snow stakes were put up on the glacier and wires were drilled down in the ablation area. The summer balance was measured in the autumn.

#### **3.1 Methods**

Measurements of the surface mass balance on a large ice cap like Vatnajökull are impractical in terms of cost with conventional techniques and sampling density that are typically used on small glaciers. The spatial variability of the mass balance may, however, be predictable on the flat large outlets of such an ice cap given data on several profiles extending over the elevation range of the glacier. The precipitation generally increases with elevation and decreases with the distance from the coast, but both the

distribution of snowfall and redistribution of snow by drift depend on the prevailing wind direction during the winter. The summer melting depends mainly on the altitude and the albedo of the glacier surface. Therefore, we have used observations along a limited number of flowlines which span the elevation ranges of the outlets. Each profile describes the variation with elevation, but together they also describe the lateral variation of the mass balance. Recently, modern over-snow vehicles and helicopters have allowed fast traverses to ensure successful fieldwork despite frequently poor weather conditions. The error for individual point measurement is estimated  $\sim 30$  cm<sup>we</sup> for both summer and winter balance. The error for the glacier wide specific mass balance, based on area integral of mass balance, is however considered smaller, since the error for individual survey sites is independent.

The winter mass balance ( $b_w$ ) is defined as the mass of snow accumulated during the winter months, the summer balance ( $b_s$ ) is the mass balance during the summer, and the net balance ( $b_n$ ) is defined as their sum. The specific mass balance is expressed in terms of the equivalent thickness of water. All mass balance components apply to a time interval between given measurement dates, which are not fixed from one year to another. The dates in the autumn are separated by approximately one calendar year, which roughly coincides with the glaciological year defined as October 1st to September 30th. Snow cores are drilled in April-May through the winter layer and profiles of the density are measured. The summer balance is derived in the autumn from measurements of the changes in the snow core density during the summer in the accumulation area and from readings at stakes and wires drilled into the ice in the ablation areas.



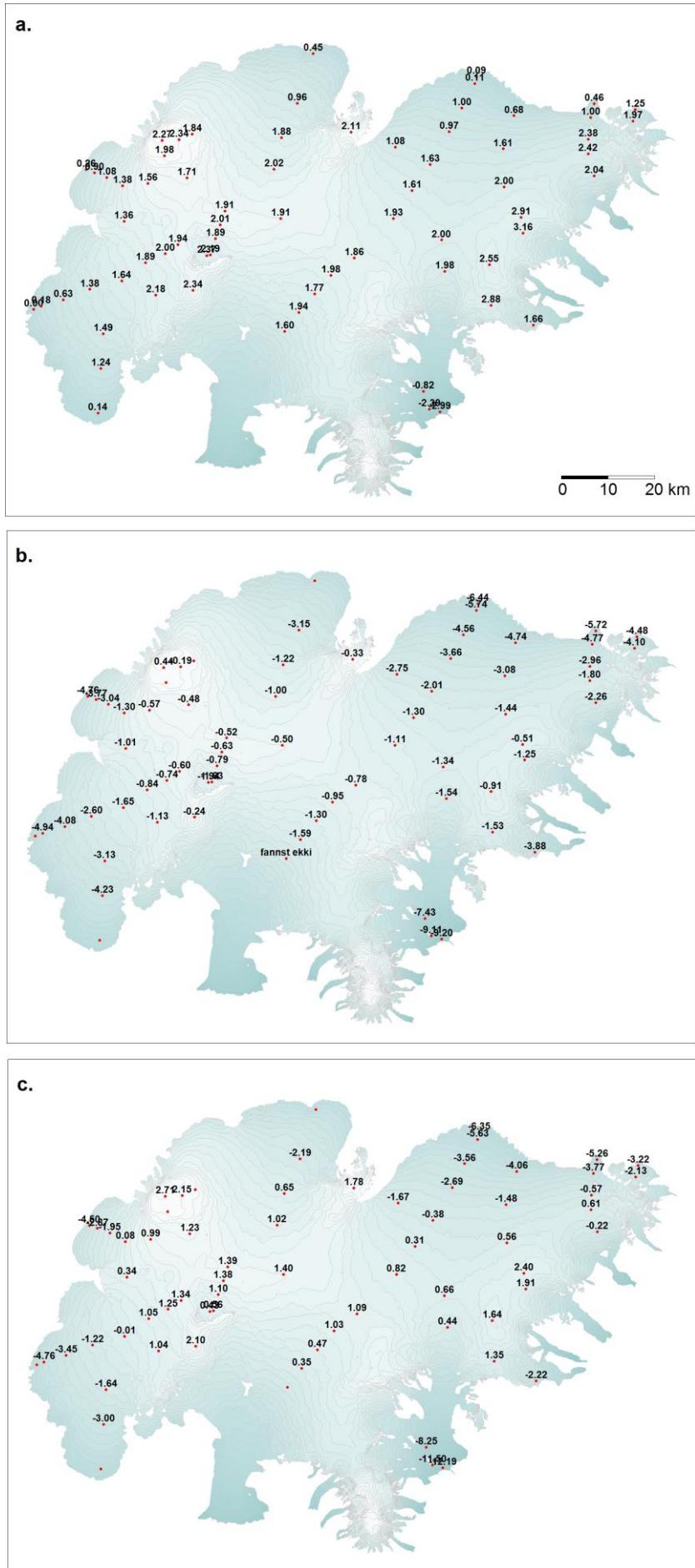
*Figure 1. Outlets of Vatnajökull and location of mass balance survey sites 2022\_23.*

Digital maps are created for winter, summer and net balance for the whole ice cap based on the in-situ measurements. The mass balance is calculated over both the ice and water drainage basins. The summer balance over the water basin is an estimate of meltwater contribution to rivers and groundwater storage. This estimate, however, does not include precipitation that falls as rain on the glacier or snow, which falls and melts during the summer. As conventional for the north hemisphere we define the glaciological year from the start of October to the end of September next year and the period draining meltwater from the glacier during the summer from start of June through September. It would be misleading to include May in the summer period because runoff from the glacier melt in May is delayed due to refreezing during the elimination of the frost in the surface layer.

### 3.2 Results of mass balance measurements.

Winter mass balance measurements were done at 68 sites in spring 2023 (Fig. 1). The specific mass balance at individual sites is shown in Fig. 2. Most survey sites are on approximate central flow lines at individual outlets. The specific mass balance along the flow lines is given in Fig 3. for the glacier outlets: Síðujökull, Tungnaárjökull, Köldukvíslarjökull, Dyngjujökull, Brúarjökull (west and east), Eyjabakkajökull, Breiðamerkurjökull, SE-Vatnajökull, Skeiðarárjökull accumulation zone and the ice catchment of Grímsvötn.

Digital maps for winter, summer and net balance are shown in Figure 4. The mass balance of individual outlet is discussed in the following subsections.



*Figure 2. Maps showing point values of specific surface mass balance in  $m_{we}$ , 2022\_23. a. winter, b. summer, c. net balance.*

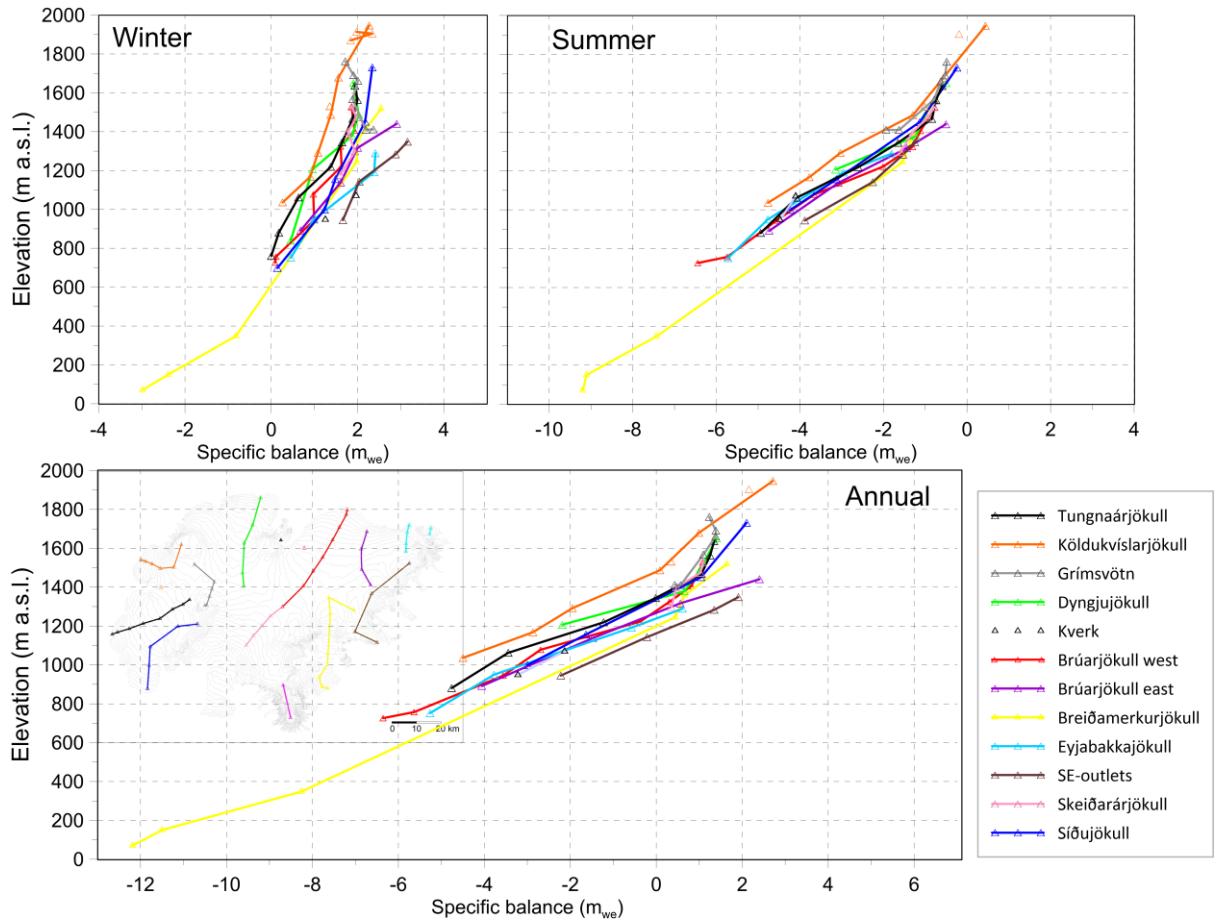


Figure 3. a. Specific mass balance ( $m_{we}$ ), at survey sites along all mass balance profiles 2022\_23.

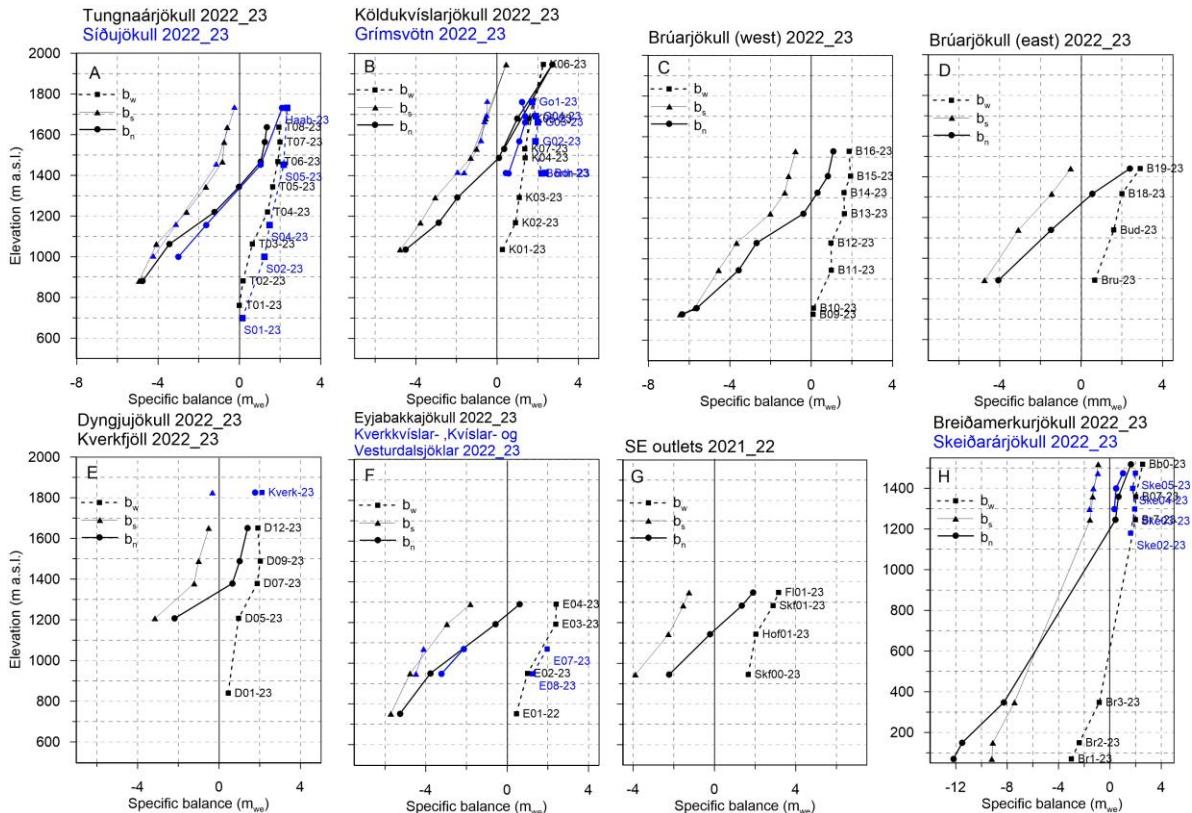


Figure 3. b. Specific point mass balance ( $m_{we}$ ) 2022\_23 as a function of elevation on central flow lines on Vatnajökull outlets.

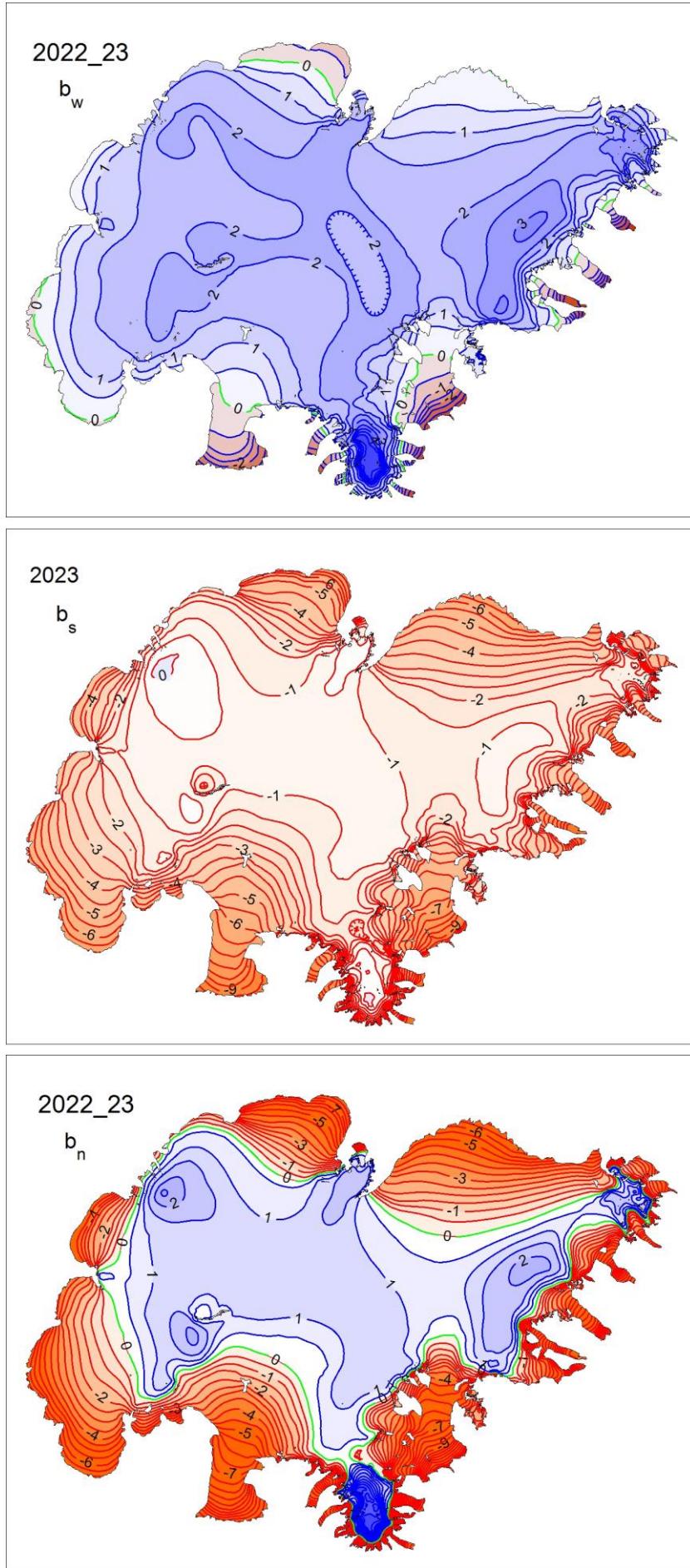
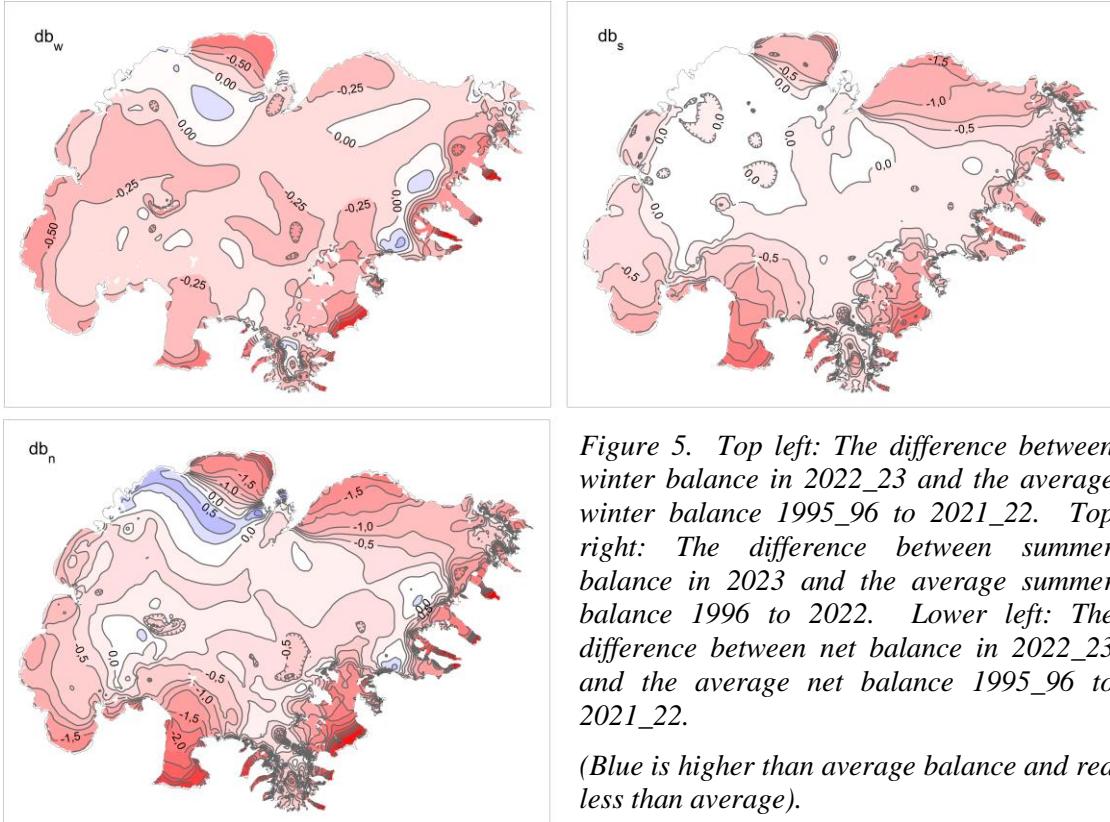


Figure 4. Specific mass balance ( $m_{we}$ ) maps of Vatnajökull 2022\_23.  
Top: winter, Centre: summer, Bottom: net balance.



*Figure 5. Top left: The difference between winter balance in 2022\_23 and the average winter balance 1995\_96 to 2021\_22. Top right: The difference between summer balance in 2023 and the average summer balance 1996 to 2022. Lower left: The difference between net balance in 2022\_23 and the average net balance 1995\_96 to 2021\_22.*

(Blue is higher than average balance and red less than average).

A surface DEM is needed for surface area distribution and delineation of ice divides for individual outlets and catchments. The currently used surface DEM is mostly based on LiDAR survey 2010, -11 and -12 (\*\*Jóhannesson et al. 2013), but the large set of GNSS profiles measured in spring 2023 were used to update the DEM to the 2023 elevation. This DEM was cut to the glacier terminus of autumn 2023, was used in all area distributions; ice and water divides were not reworked. Although of variable accuracy locally the DEM reflects fairly accurate elevation distribution.

The winter of 2022-2023 was rather cold, with winter precipitation less than average in the west (west of Bárðarbunga - Öræfajökull) but closer to average in the east.

Distribution of the winter snow was not typical (see fig. 5). In general, there was by far less snow than average in the lower ablation zones of the icecap, and by far less than average at all elevations in the west and south. Winter melting at the low-lying S-outlets was more than average. The

summer was for most part rather warm, very dry and calm, most of the N-Atlantic low-pressure systems passed far south of Iceland. This resulted in an over average summer melt. The warm autumn contributed markedly to the total melt. The warm summer is partly due to warming of the sea water around Iceland by ~1 °C from recent years, now like the conditions in the period 1995-2010.

\*\*Jóhannesson, T., Björnsson, H., Magnússon, E., Guðmundsson, S., Pálsson, F., Sigurðsson, O., Thorsteinsson, T., and Berthier, E.: Ice-volume changes, bias estimation of mass-balance measurements and changes in subglacial lakes derived by lidar mapping of the surface Icelandic glaciers, Ann. Glaciol., 54, 63–74, doi:10.3189/2013AoG63A422, 2013.

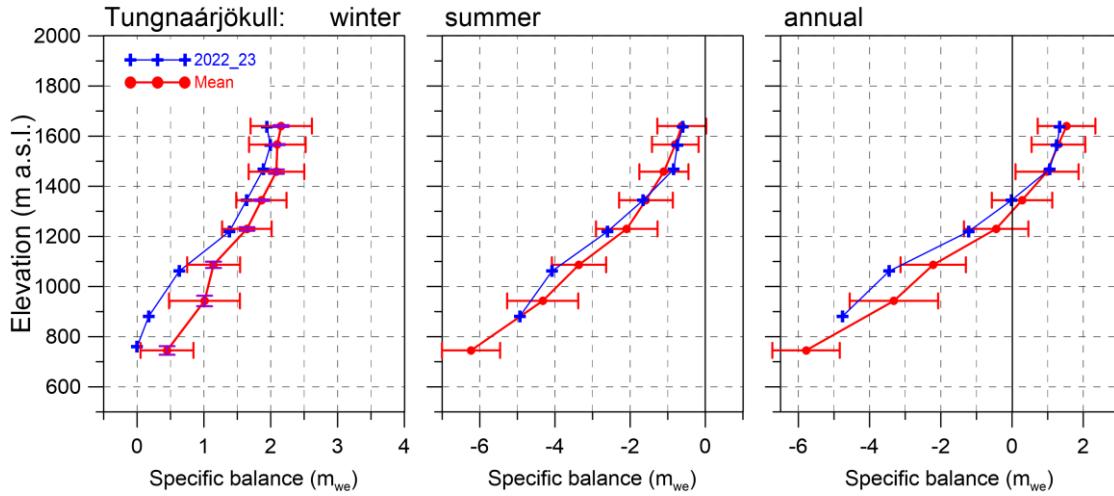


Figure 6. Mass balance at a central flow line of Tungnaárjökull 2022\_23 and average mass balance 1991\_92 to 2021\_22 (the horizontal red lines indicate std. dev of the variability at the survey site during the survey period).

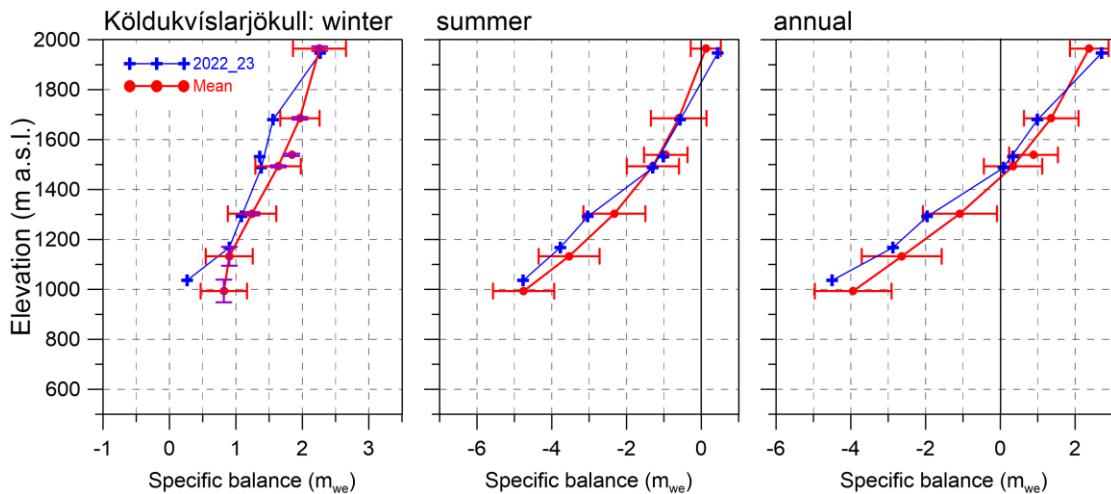


Figure 7. Mass balance at a central flow line of Köldukvíslarjökull 2022\_23 and average mass balance 1991\_92 to 2021\_22.

### 3.2.1 Tungnaárjökull.

$$\text{Area} = 323 \text{ km}^2$$

$$B_w = 0.38 \text{ km}^3 \text{ we}; b_w = 1.16 \text{ m}_\text{we}$$

$$B_s = -0.87 \text{ km}^3 \text{ we}; b_s = -2.69 \text{ m}_\text{we}$$

$$B_n = -0.49 \text{ km}^3 \text{ we}; b_n = -1.53 \text{ m}_\text{we}$$

$$\text{ELA} = 1346 \text{ m a.s.l. (at profile)}$$

$$\text{AAR} = 33 \%$$

(The terms are defined at the foot of this page)

Variation of mass balance along a central flow line on Tungnaárjökull is shown in Fig. 6. The winter accumulation was under average at all survey sites, by far so, in the ablation zone. The total winter balance was only 76% of the average. Summer mass loss was not far from average, in total about 2% over the average. This

For each ice catchment basin,  $B_w$ ,  $B_s$  and  $B_n$  are water equivalent volumes of winter, summer and net balance, ELA the equilibrium line altitude, and AAR is the accumulation area ratio.

year is the 28<sup>th</sup> year out of the 32 surveyed with negative net balance on Tungnaárjökull catchment, this time 35% more mass was lost than at average in the survey period.

### 3.2.2 Köldukvíslarjökull

$$\text{Area} = 284 \text{ km}^2$$

$$B_w = 0.35 \text{ km}^3 \text{ we}; b_w = 1.23 \text{ m}_\text{we}$$

$$B_s = -0.56 \text{ km}^3 \text{ we}; b_s = -1.97 \text{ m}_\text{we}$$

$$B_n = -0.21 \text{ km}^3 \text{ we}; b_n = -0.74 \text{ m}_\text{we}$$

$$\text{ELA} = 1478 \text{ m a.s.l. (at profile)}$$

$$\text{AAR} = 48 \%$$

Variation of mass balance along a central flow line on Köldukvíslarjökull is shown in Fig. 7. The winter accumulation was less than average in the accumulation zone by about 1. Std.

close to average in the mid ablation zone, but almost no snow accumulated below 1000 m elevation. The total winter accumulation was ~83% of the average. Summer mass loss was close to average in the accumulation zone, but by  $\frac{1}{2}$  to 1 std. in the ablation zone. all survey sites. In total summer mass loss was ~1% more than average. This year Köldukvíslarjökull net balance was negative, this is the 26<sup>th</sup> year out of the 32 surveyed with negative net balance; now 58% more mass was lost than in an average year since 1991-92.

### 3.2.3 Dyngjujökull

Area = 1026 km<sup>2</sup>  
 $B_w = 1.53 \text{ km}^3 \text{ we}$ ;  $b_w = 1.50 \text{ m}_\text{we}$   
 $B_s = -1.85 \text{ km}^3 \text{ we}$ ;  $b_s = -1.80 \text{ m}_\text{we}$   
 $B_n = -0.32 \text{ km}^3 \text{ we}$ ;  $b_n = -0.30 \text{ m}_\text{we}$   
ELA = 1336 m a.s.l. (at profile)  
AAR = 67 %

Variation of mass balance along a flow line on Dyngjujökull is shown on Fig. 8. In the high accumulation zone sites snow accumulation was ~1 std. under average, about 1 std. over average in the lower accumulation zone. In the ablation zone snow collection was

close to average. The total winter accumulation is estimated 93% of the average of the survey period.

Summer mass loss was almost at average at all survey sites but by about 1 std. over the average at 1200 m. The lowest site has not been visited yet when the report is written. The net balance was negative by  $-0.30 \text{ m}_\text{we}$  about tenfold the average for Dyngjujökull that is only slightly negative ( $-0.03 \text{ m}_\text{we}$ ).

Dyngjujökull has often had mass balance close to zero, and the net balance has been estimated positive in at least 12 years of the three-decade period of almost continuous mass loss for Vatnajökull as a whole. The inland Dyngjujökull, is the outlet of Vatnajökull closest to mass equilibrium during the survey period.

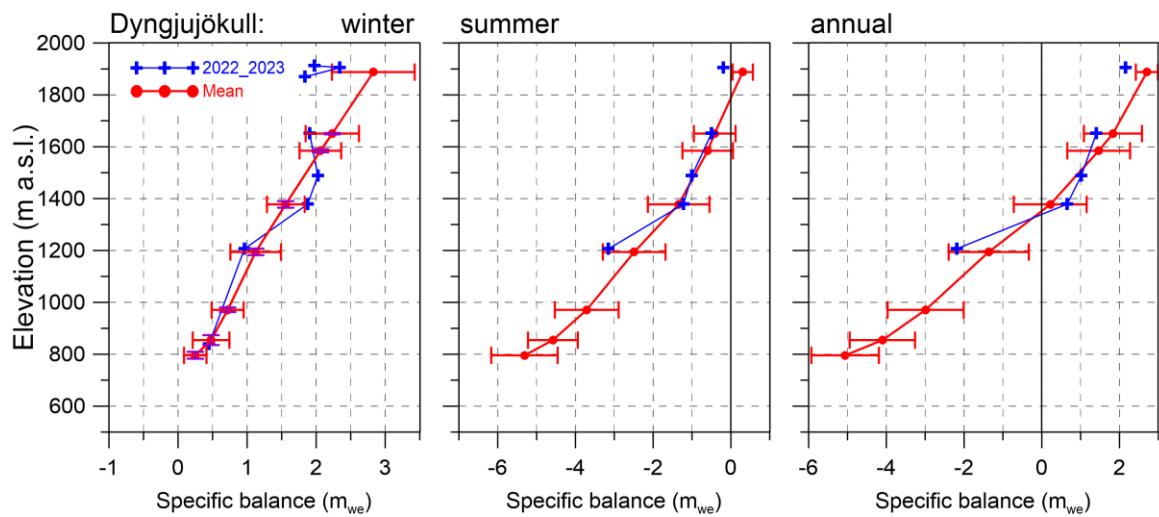
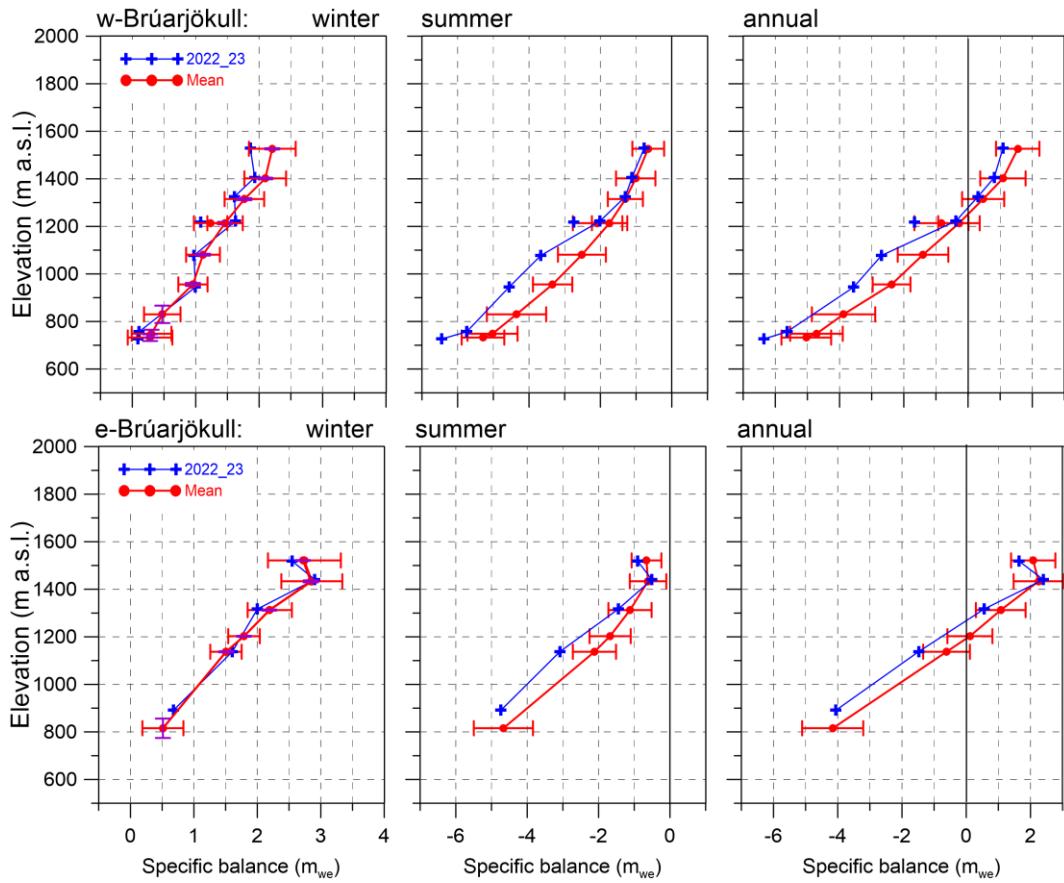


Figure 8. Mass balance at a central flow line on Dyngjujökull 2022\_23 and average mass balance 1991\_92 to 2021\_22 (except 1998\_99 – 2003\_04 at all but the top elevation).



*Figure 9. Mass balance at two flow lines on Brúarjökull 2022\_23 and average mass balance 1992\_93 to 2021\_22.*

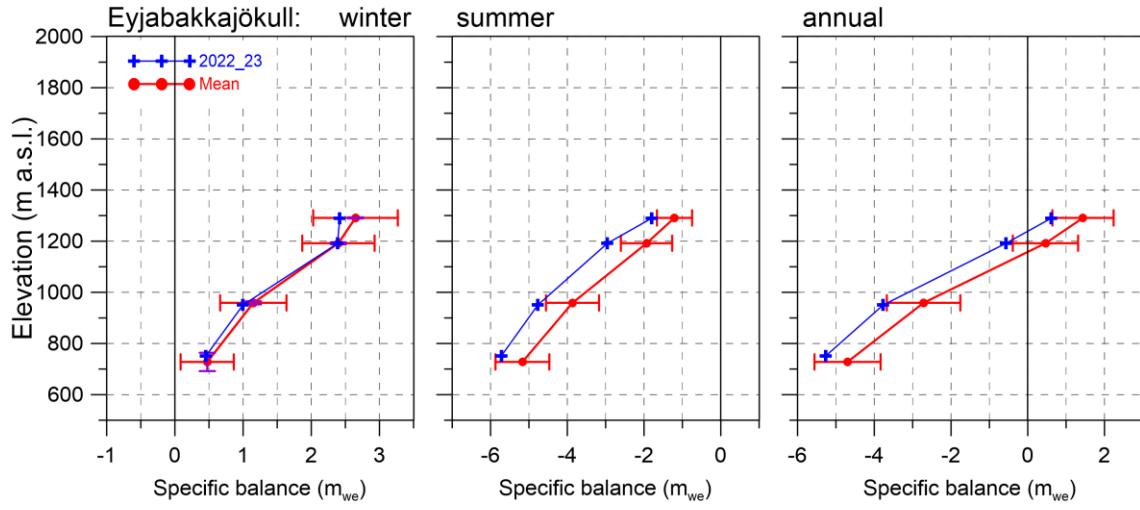
### 3.2.4 Brúarjökull

Area = 1481 km<sup>2</sup>  
 $B_w = 2.30 \text{ km}^3 \text{ we}$ ;  $b_w = 1.55 \text{ m}_\text{we}$   
 $B_s = -3.36 \text{ km}^3 \text{ we}$ ;  $b_s = -2.26 \text{ m}_\text{we}$   
 $B_n = -1.06 \text{ km}^3 \text{ we}$ ;  $b_n = -0.71 \text{ m}_\text{we}$   
ELA = 1280 m a.s.l. (western flow line)  
ELA = 1268 m a.s.l. (eastern flow line)  
AAR = 54 %

Variation of mass balance along the flow lines on Brúarjökull is shown in Fig. 9. On Brúarjökull winter snow collection was not far from average at most survey sites, except in the top western accumulation zone, where it was ~1 std. less than average. The winter accumulation was in total ~96% of the average. Summer mass loss was close to average at most survey sites above 1200 m elevation, but more than 1 std. over than average at all the other

sites. In total the mass loss in summer was 19% more than average.

The net balance was close to average in 1200-1400 m elevation range, but at other sites about 1 std. lower at all the other. In total the net balance was negative by 0.71 m<sub>we</sub>. That amounts to about 25 fold that of an average year. During the survey period, there have been 9 years of positive balance and 22 years with negative net balance.



*Figure 10. Mass balance at a central flow line of Eyjabakkajökull 2022\_23 and average mass balance 1995\_96 to 2021\_22.*

### 3.2.5 Eyjabakkajökull

Area = 104 km<sup>2</sup>

$B_w = 0.19 \text{ km}^3 \text{ we}$ ;  $b_w = 1.81 \text{ m}_\text{we}$

$B_s = -0.33 \text{ km}^3 \text{ we}$ ;  $b_s = -3.23 \text{ m}_\text{we}$

$B_n = -0.14 \text{ km}^3 \text{ we}$ ;  $b_n = -1.42 \text{ m}_\text{we}$

ELA = 1239 m a.s.l. (at profile)

AAR = 38 %

Variation of mass balance along a central flow line on Eyjabakkajökull is shown in Fig. 10. Like Brúarjökull the winter accumulation here was at average at all sites except the highest, where it was less than average. The total winter accumulation is estimated 99% of the survey period average. Summer mass loss was about 1 std more than average at all survey sites.

The total summer mass loss was 20% more than average. The net balance was negative by about 1.7-fold that of the average of the survey period and has been negative for all but 3 years of the 28 years of survey.

### 3.2.6 Breiðamerkurjökull

Area = 875 km<sup>2</sup>

$B_w = 1.10 \text{ km}^3 \text{ we}$ ;  $b_w = 1.26 \text{ m}_\text{we}$

$B_s = -2.55 \text{ km}^3 \text{ we}$ ;  $b_s = -2.92 \text{ m}_\text{we}$

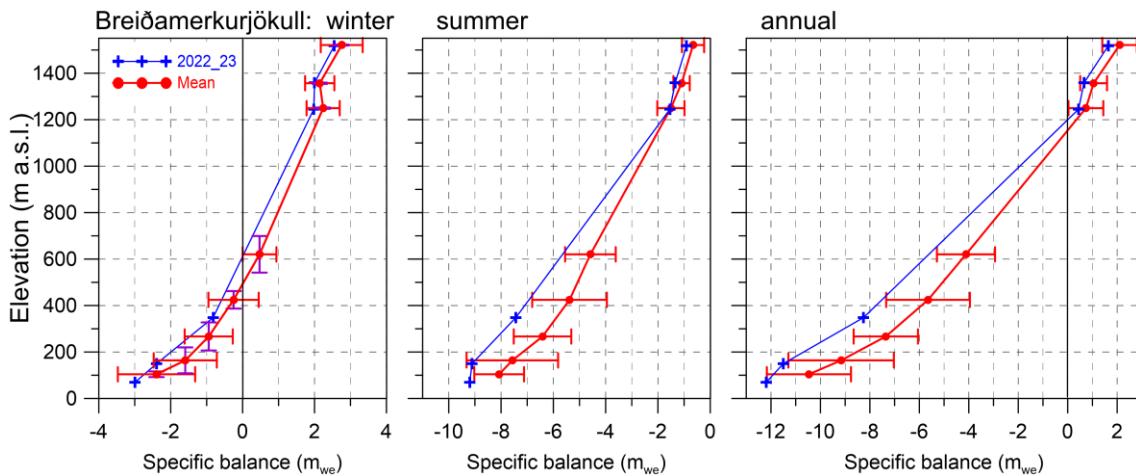
$B_n = -1.45 \text{ km}^3 \text{ we}$ ;  $b_n = -1.66 \text{ m}_\text{we}$

ELA = 1200 m a.s.l. (at profile)

AAR = 51%

Variation of surface mass balance along a central flow line on Breiðamerkurjökull is shown in Fig. 11.

Winter accumulation was less than



*Figure 11. Mass balance at a central flow line of Breiðamerkurjökull 2022\_23 and average mass balance 1995\_96 to 2021\_22.*

average at the survey sites in the accumulation zone, but at the lower sites in the ablation zone mass loss in winter was more than average. The total winter balance was ~84% of the survey period average.

Summer mass loss was not far from the average in the accumulation zone), but more than 1 std. over average in the lower ablation zone. The total summer mass loss is estimated 12% over the average during the survey period. The net surface mass loss this year is estimated about 1.5-fold that of an average year.

In addition to mass loss due to surface melt Breiðamerkurjökull loses in the order of  $0.5 \text{ km}^3$  (~0.6 m) annually via calving into the marginal lake Jökulsárlón; this mass loss is not accounted for here.

### 3.2.7 Skeiðarárjökull

Area =  $1346 \text{ km}^2$

$B_w = 1.87 \text{ km}^3_{\text{we}}$ ;  $b_w = 1.39 \text{ m}_{\text{we}}$

$B_s = -3.58 \text{ km}^3_{\text{we}}$ ;  $b_s = -2.66 \text{ m}_{\text{we}}$

$B_n = -1.71 \text{ km}^3_{\text{we}}$ ;  $b_n = -1.27 \text{ m}_{\text{we}}$

ELA = ~1250 m a.s.l. (at profile)

AAR = 54

The surface mass balance of Skeiðarárjökull is only measured in the accumulation zone due to almost impassable terrain in the ablation zone

both in autumn and spring.

The mb-survey program here was initiated in 2002, although sporadic measurements were conducted in the 1990s. Estimation of mb in the ablation zone for the creation of the mb-maps is based on the survey of the neighboring Breiðamerkurjökull in the east (with similar elevation span) and western neighboring outlet Síðujökull.

Variation of mass balance along the survey profile on Skeiðarárjökull is shown in Fig. 12. Winter snow accumulation was 1 Std. under average at the highest (as was the site B16 located at the ice-divide of Brúarjökull and Skeiðarárjökull in continuation of the Skeiðarárjökull profile). The site at 1300 m however had winter mb close to average; this is likely due redistribution of snow by wind and seen at many other outlets of Vatnajökull this year. The redistribution of snow is more likely in prevailing northly winds and cold temperatures during snow fall.

Summer balance was close to average at the upper sites, and the lowest was not reachable in the autumn due to crevasses. The net balance was about 1 std under average, now due to unusually low winter balance.

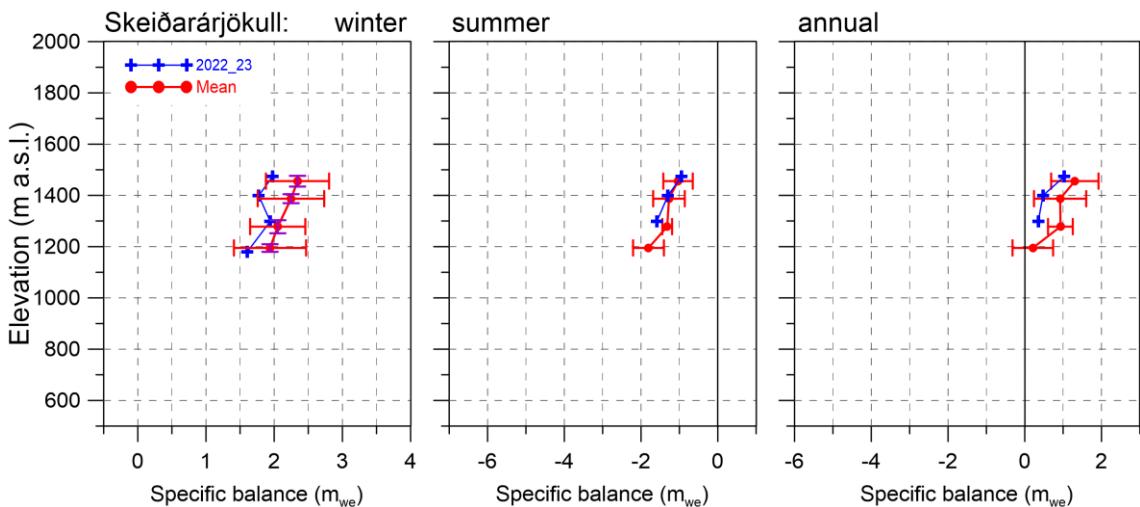


Figure 12. Mass balance at a central flow line of Skeiðarárjökull 2022\_23 and average mass balance 2016\_17 to 2021\_22.

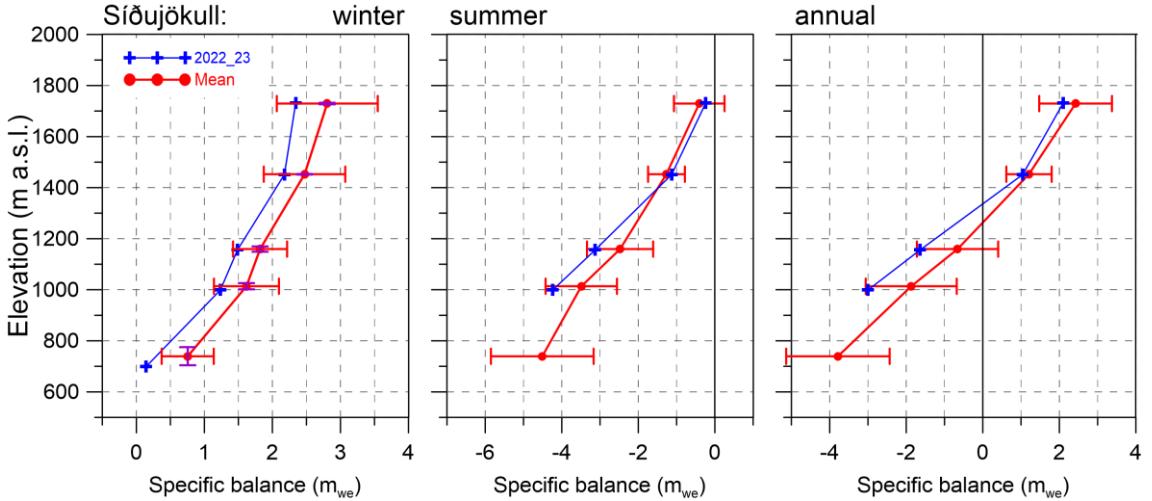


Figure 13. Mass balance at a central flow line of Síðujökull 2022\_23 and average mass balance 2004\_05 to 2021\_22.

### 3.2.8 Síðujökull

Area = 400 km<sup>2</sup>

$B_w = 0.55 \text{ km}^3 \text{ we}$ ;  $b_w = 1.38 \text{ m}_\text{we}$

$B_s = -1.26 \text{ km}^3 \text{ we}$ ;  $b_s = -3.15 \text{ m}_\text{we}$

$B_n = -0.71 \text{ km}^3 \text{ we}$ ;  $b_n = -1.77 \text{ m}_\text{we}$

ELA = 1335 m a.s.l. (at profile)

AAR = 36 %

Variation of mass balance along a central flow line on Síðujökull is shown in Fig. 13.

The winter snow accumulation was well under average at all survey sites. The total winter balance was 86% of the average (since 2004\_05). Summer

mass loss was at average at the highest sites, but far over the at the lower sites (In autumn the route to the lowest sit3 was impassable). The total summer mass loss was 8% over the average of the survey period. Total mass loss was ~35% more than average during the 18-year survey period. At Síðujökull the only year of surveyed positive net balance was 2014\_2015.

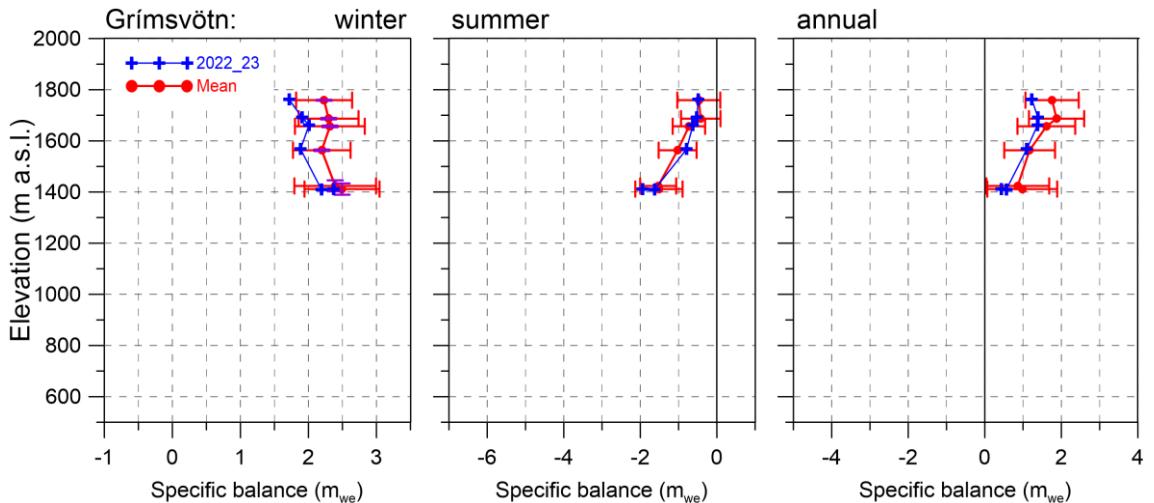


Figure 14. Mass balance at a flow line towards Grímsvötn 2022\_23 and average mass balance 1991\_92 to 2021\_22.

### 3.2.9 Grímsvötn-Gjálp

Area = 174 km<sup>2</sup>

$B_w = 0.34 \text{ km}^3 \text{ we}$ ;  $b_w = 1.99 \text{ m we}$

$B_s = -0.13 \text{ km}^3 \text{ we}$ ;  $b_s = -0.78 \text{ m we}$

$B_n = 0.21 \text{ km}^3 \text{ we}$ ;  $b_n = 1.21 \text{ m we}$

Variation of mass balance at sites close to a flow line from Bárðarbunga towards Grímsvötn center is shown in Fig. 14. Snow accumulation at the survey sites was between  $\frac{1}{2}$  - 1 std. less than average, and total winter accumulation 12% less than average. Summer mass loss was close to average at all survey sites; total summer mass loss was 6% more than average. Net balance was positive as always (except 2010), however, now only 78 % of the average.

In addition to surface mass loss in summer, geothermal melt in the Grímsvötn catchment area is on the order of 0.2 km<sup>3</sup> annually. This mass loss is about 1.21 m evenly distributed over the ice catchment, or approximately equal to this year net surface balance. This means that the total balance for the catchment of Grímsvötn is close to zero this year.

The average surface mass balance in the survey period (since 1991-92) is +1.50 m, so assuming the annual 1.21 m loss due to geothermal melt yields an annual surplus of ~0.3 m (0.052 km<sup>3</sup>) on average, or ~1.6 km<sup>3</sup>. In the Gjálp eruption, within the Grímsvötn ice catchment, over 3.5 km<sup>3</sup> of ice was melted and some, although much less, in the 1998, 2004 and 2011 Grímsvötn eruptions. About half of this has been compensated for by the average total positive surface balance.

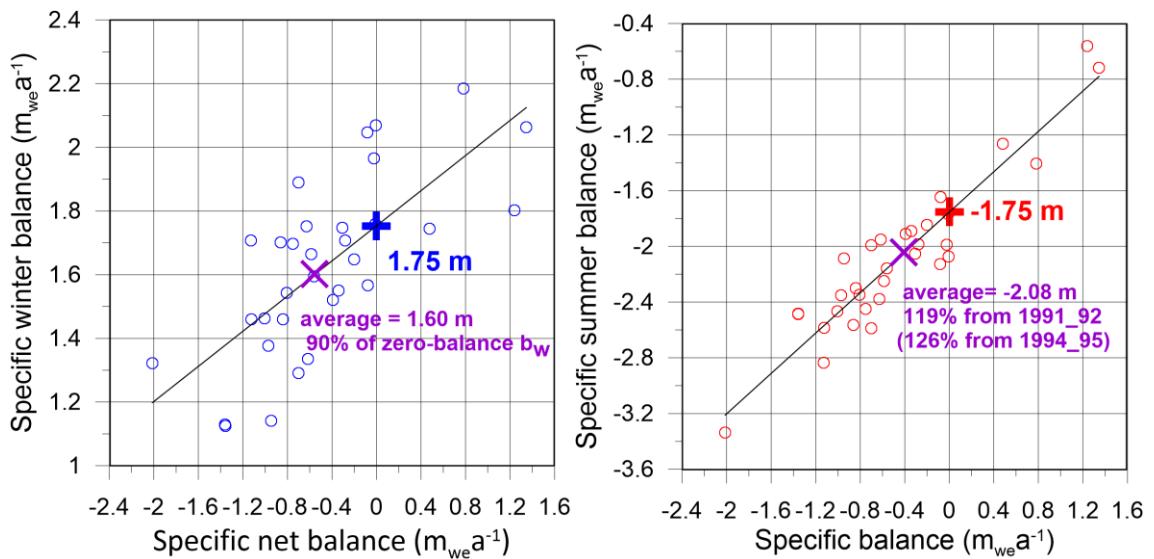


Figure 15. Vatnajökull winter (left) and summer (right) mass balance plotted against net mass balance for the survey period 1991\_92 to 2022\_23. The + and + and the accompanying numbers, mark the zero-mass balance mass turnover for Vatnajökull (current topography) as estimated from the linear trends shown with thin black lines.

### **3.3 Vatnajökull: Surface mass balance record**

From the digital mb maps (Fig. 4) the glacier wide volumes of winter, summer and net balances for Vatnajökull have been calculated by integration and are as follows:

**Area = 7656 km<sup>2</sup>**

**B<sub>w</sub> = 11.10 km<sup>3</sup>we ; b<sub>w</sub> = 1.46 m<sub>we</sub>**

**B<sub>s</sub> = -18.74 km<sup>3</sup>we ; b<sub>s</sub> = -2.47 m<sub>we</sub>**

**B<sub>n</sub> = -7.64 km<sup>3</sup>we ; b<sub>n</sub> = -1.01 m<sub>we</sub>**

**AAR = 53%;**

(balance values as a function of elevation are tabulated in appendix D)

The winter of 2022-2023 was rather cold, with winter precipitation less than average in the west (west of Bárðarbunga - Öræfajökull) but closer to average in the east.

Distribution of the winter snow was not typical (see fig. 5). In general, there was by far less snow than average in the lower ablation zones of the icecap, and by far less average at all elevations in the west and south. In many of the outlets over average winter accumulation was measured in the mid elevation range of the accumulation zone, but less than average at higher elevations. This is at least partly due to wind redistribution, but perhaps also by lesser portion falling as rain in autumn due to the colder than average autumn. Winter melting at the low-lying S-outlets more than average. The summer was for most part rather warm, very dry and calm, most of the N-Atlantic low-pressure systems passed far south of Iceland. This resulted in more than average summer melt. The warm 2023 autumn contributed markedly to the total melt. The warm summer is partly due to warming of the sea water around Iceland by ~1 °C from recent years, now similar to the sea

temperatures in the period 1995-2010. The total winter balance was ~90% of the average (over the observation period from 1991\_92).

The total summer mass loss was almost 20% more than the average of the survey period.

The net balance of 2022\_23 was very negative or 2.25-fold the average (over the observation period from 1991\_92).

The zero-mass balance mass turnover (mbt) for Vatnajökull (current topography) is estimated from the zero net balance crossover of the linear trend of b<sub>w</sub> plotted against b<sub>n</sub> and equivalently b<sub>s</sub> against b<sub>n</sub> (see fig 15.) and found to be close to 1.75 m<sub>we</sub> (13.4 km<sup>3</sup>we). The winter balance 2022\_23 is ~83% of the estimated zero-mass balance turnover (0-mbt), while the average b<sub>w</sub> of the survey period is ~90% of the 0-mbt.

The summer balance of 2023 is -0.72 m (or 42%) more negative than 0-mbt. On average the summer mass loss has been 19% (average of summers 1992-2022) higher than 0-mbt, (26% for the period of 1995-2022).

This clearly shows that the high mass loss of the past 3 decades is governed by too much mass loss during summer rather than too little snow accumulation during winter.

Since 2010, after the 15-year period of high mass loss, the summer and net balance have been highly variable (figure 16.), one year with definite positive mass balance, 2014\_15, and a few close to zero or slightly positive: 2010\_11, 2016\_17, 2017\_18 and 2021\_22.

The variability of the winter balance is by far more prominent for the outlets closest to sea. That section of the glacier receives precipitation in all south and east wind directions, and thus has high snow accumulation in winters when prevailing paths of the North Atlantic low-pressure systems are just south and east of Iceland.

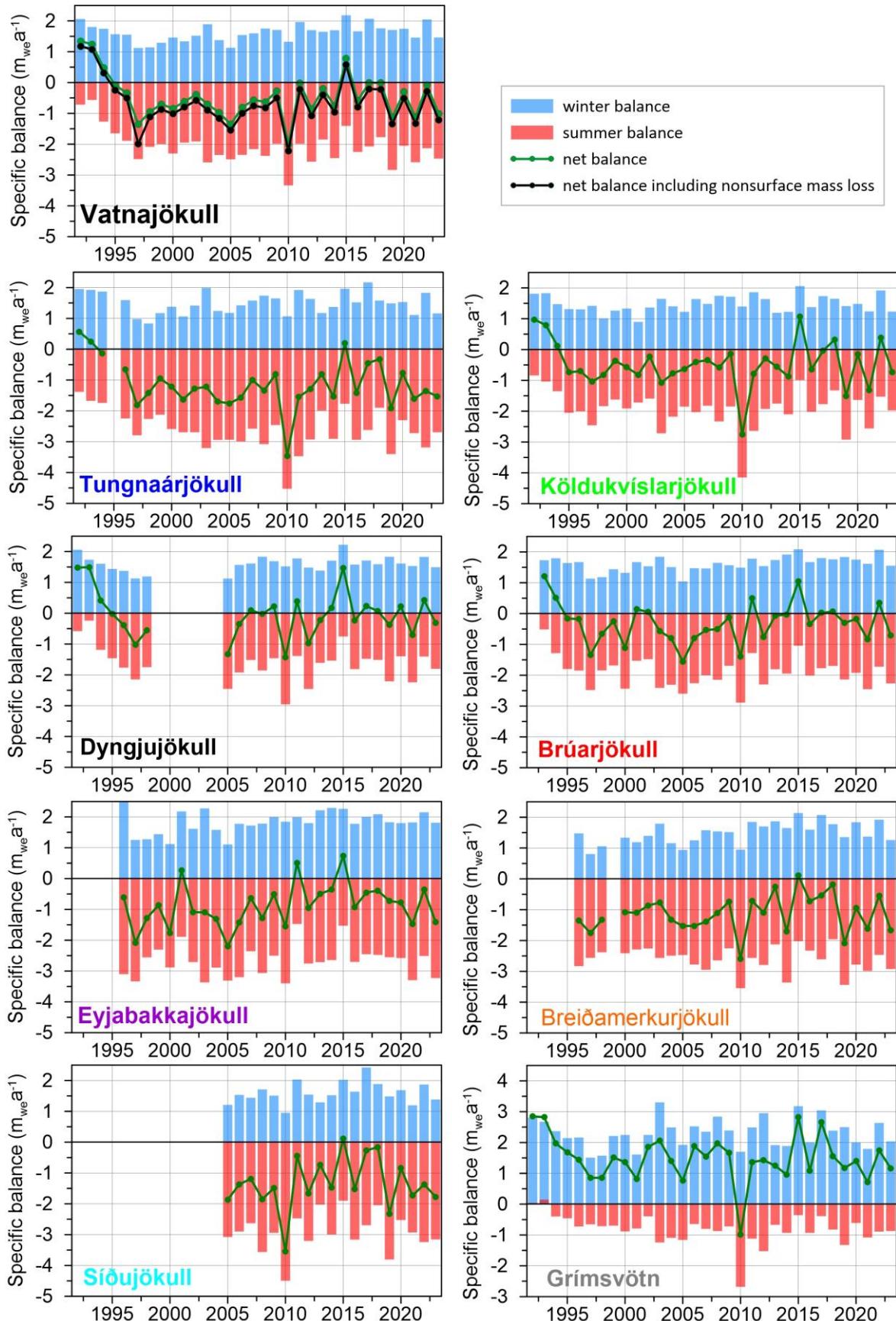
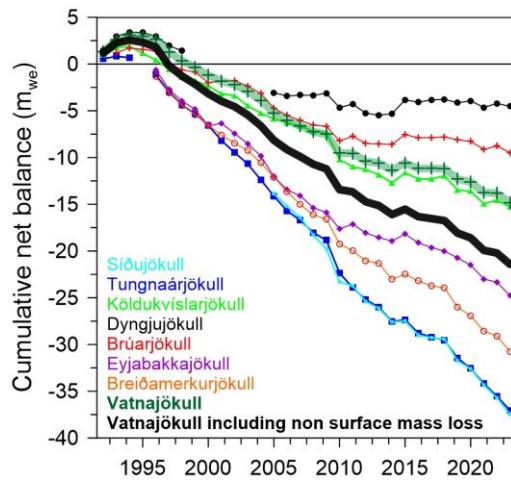


Figure 16. Specific mass balance record for Vatnajökull (top), and selected Vatnajökull outlets 1991\_92-2022\_23.



*Figure 17. Cumulative specific surface mass balance Vatnajökull and selected Vatnajökull outlets 1991\_92 – 2022\_23.*

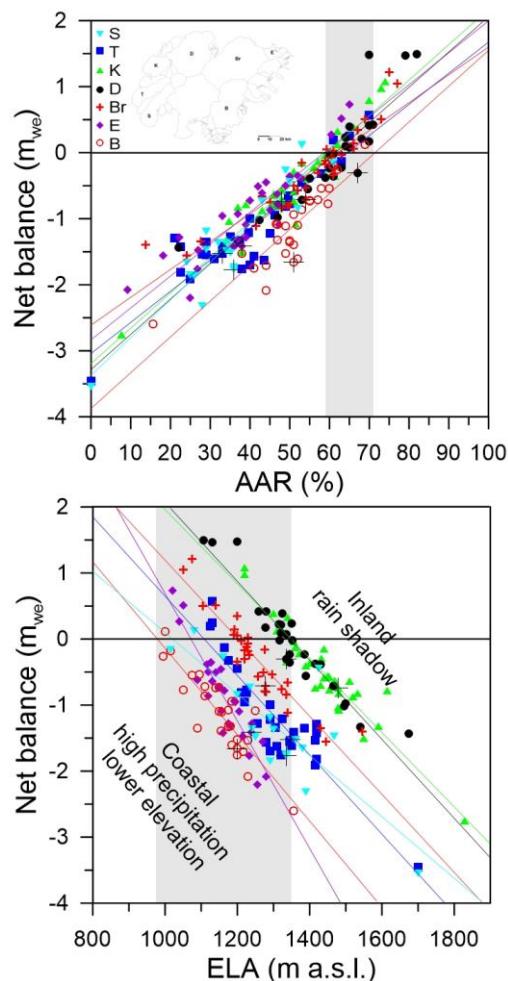
The cumulative net balance curves for the outlets of Vatnajökull in Fig. 17 show that all outlets have been losing mass since in most years since 1994\_95. In the period of high mass loss, the loss rate is about  $-0.5$  to  $-0.6$   $m_{wea}^{-1}$  for the northern outlets but  $-1.1$  to  $-1.5$   $m_{wea}^{-1}$  for the south and western outlets. After 2010 there is a distinct difference between the north inland (Dyngjujökull and Brúarjökull) and the south and west coastal outlets (Breiðamerkurjökull, Tungnaárjökull and Síðujökull) in that there is a sudden change in the mass balance trend for the northern. The trend changes from  $-0.5$   $m_{wea}^{-1}$  to about zero for the northern while there is little change for the others. The east outlet Eyjabakkajökull behaves like the coastal and is in fact close to sea, while Köldukvíslarjökull in the NV is more like the northern.

The cumulative mb for Vatnajökull is very similar to Köldukvíslarjökull, with a slope of  $-0.75$   $m_{wea}^{-1}$  in the period of high mass loss, but  $-0.35$   $m_{wea}^{-1}$  after 2010.

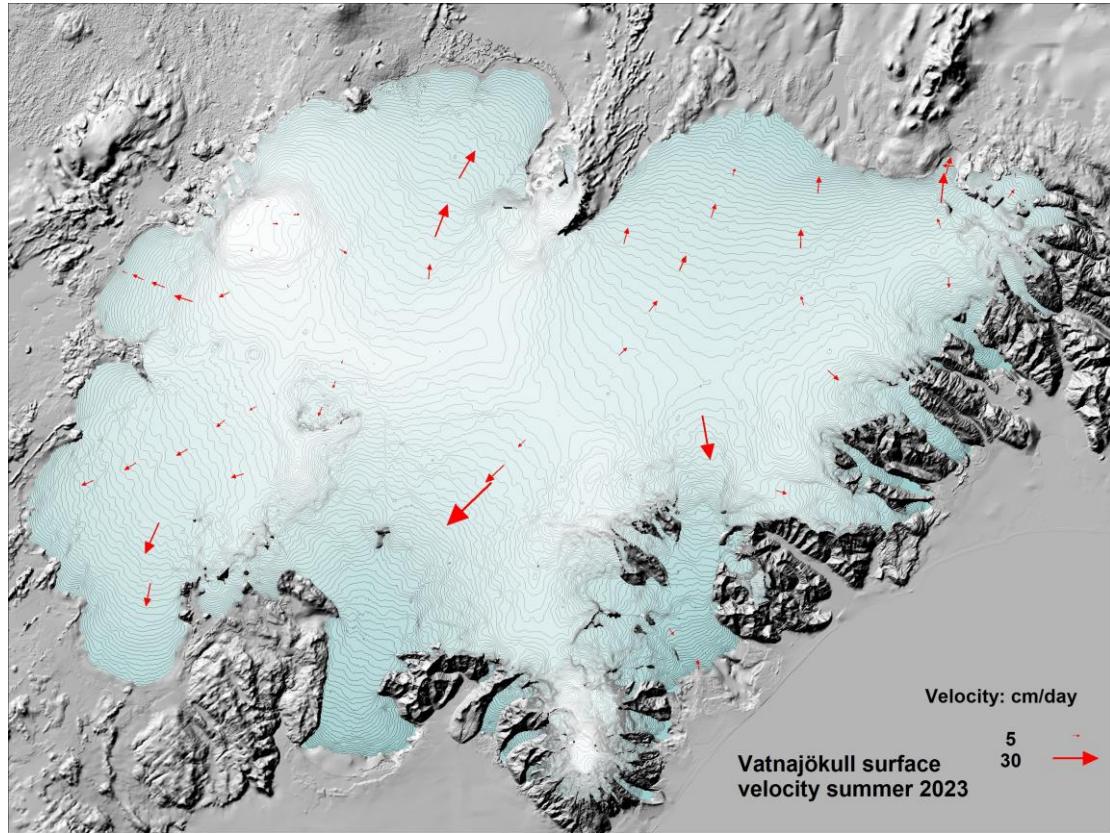
During the survey period starting in 1991\_92 Vatnajökull lost  $\sim 131$   $km^3$  of ice or thinned  $\sim 15$  m due to surface

mass loss (summing from the start of high mass loss in 1994\_95 yields  $159$   $km^3$  or  $19$  m thinning).

In addition, non-surface mass loss is estimated (calving, geothermal melt, internal friction, eruptions)  $\sim 0.21$   $m_{we}$  for Vatnajökull in a paper by Tómas Jóhannesson and others (Jóhannesson, T., Pálmarsson, B., Hjartarson, Á., Jarosch, A., Magnússon, E., Belart, J., et al. (2020). Non-surface mass balance of glaciers in Iceland. *J. Glaciol.* 66, 685–697. doi:10.1017/jog.2020.37) which amounts to an ice loss of  $\sim 59$   $km^3$  or  $7.7$  m average thinning since 1994\_95.



*Figure 18. The relation between net annual balance ( $b_n$ ) and accumulation area ratio (AAR) (upper) and  $b_n$  and equilibrium line altitude (ELA), for Vatnajökull outlets during the survey period. (This year's points are marked with a black +).*



*Figure 19. Average summer velocity at survey sites in 2023.*

In Fig. 17 the relation of the annual net balance to the accumulation area ratio (AAR) and equilibrium line altitude (ELA) is shown for different outlets over the survey period. The bn-AAR gradient is similar for all outlets, about  $0.5 \text{ m}_{\text{we}}$  for 10% change in AAR. The zero-balance AAR varies for different outlets in the range 60–65%, similar for all outlets except for the southern outlet Breiðamerkurjökull. Breiðamerkurjökull is far from equilibrium, the ablation area is too large. A large part of the outlet has carved 200–300 m deep valley into the former sediment bed, and the surface and bed elevation has lowered accordingly. Similarly, the zero-balance ELA varies from about 1000–1100 m a.s.l. for the southern outlets to 1400 m a.s.l. for the NW outlets. The bn-ELA slope is similar for all outlets  $-0.6 \text{ m}_{\text{we}}$  per 100 m, except Eyjabakkajökull with a slope of  $-1.0 \text{ m}_{\text{we}}$  per 100 m and Síðujökull with a slope of  $-0.45 \text{ m}_{\text{we}}$  per 100 m (for Síðujökull possibly due to outliers in the data set).

#### 4. SURFACE VELOCITY MEASUREMENTS

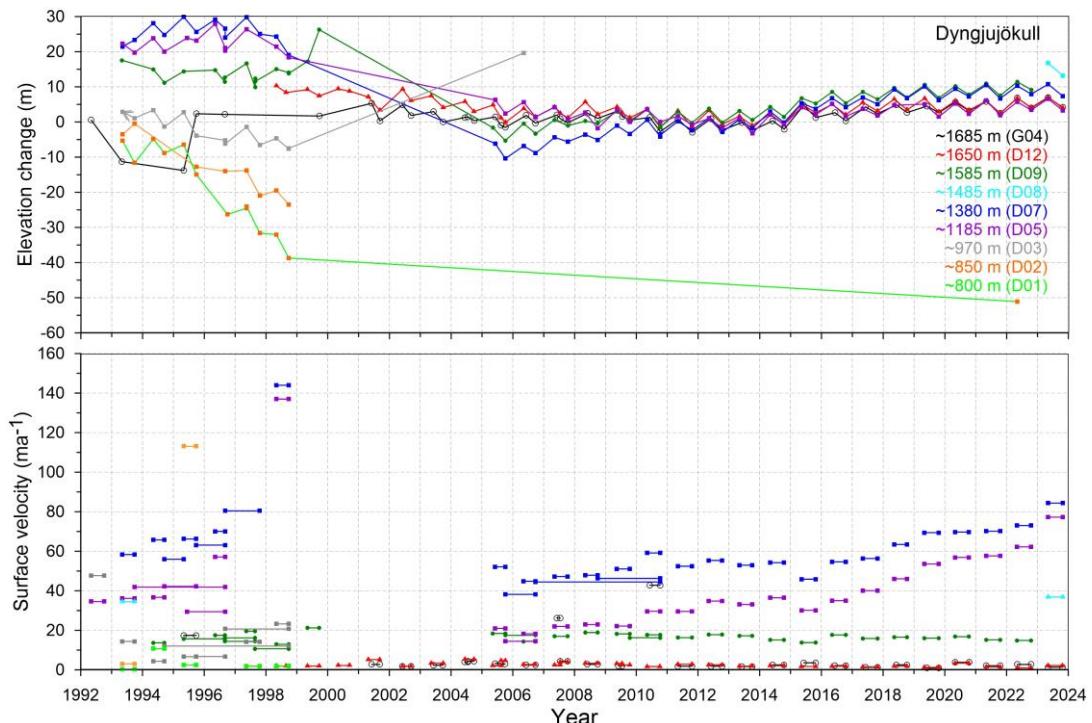
The average summer surface velocity of the glacier surface at the survey sites was calculated from fast static or kinematic GNSS positioning of the ablation stakes/wires (accuracy about  $\sim 10 \text{ cm}$ ). In 2023 all sites were surveyed in spring and autumn and many in June. At a few sites, stakes from previous years were found and resurveyed, making it possible to calculate surface velocity over a year or longer time span. The average summer surface velocity is shown in Figure 19.

At sites close to the glacier terminus very small lateral movement is generally measured. This indicates that the glacier snouts are almost stagnant. In the centre areas of some of the outlets especially close to the equilibrium line, there is an increase in velocity during summer compared to winter. The summer velocity is

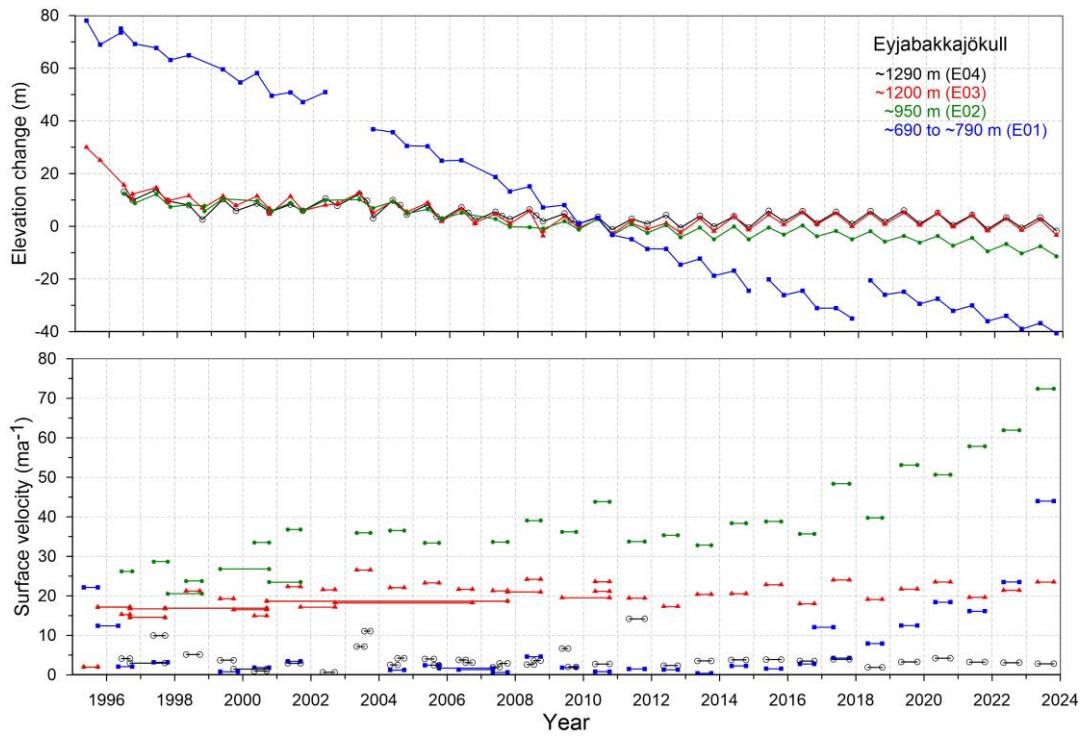
typically in the order of two-fold the winter velocity. This suggests that basal sliding is increased in the melting season and is often at the same magnitude as the deformation velocity. To better understand the variable velocity continuous GNSS has been run during summer at several sites. From previous velocity measurements, surging of outlets has been predicted. Currently the increase in velocity at sites D05 and D07 (Fig. 20.) persists and suggests that Dyngjujökull may surge within a few years. The velocity at sites D07 and D05 is now similar to that in 1997 prior to the surge in 1998–2000 and the accumulation zone has thickened. To monitor velocity changes leading up to a surge GNSS instruments were set up in spring to continuously monitor movement at sites D05 and D07.

The data collected allows for post-processing to acquire more accuracy ( $\sim$ dm instead of  $\sim$ m), but the processing has not been finished when this report is written.

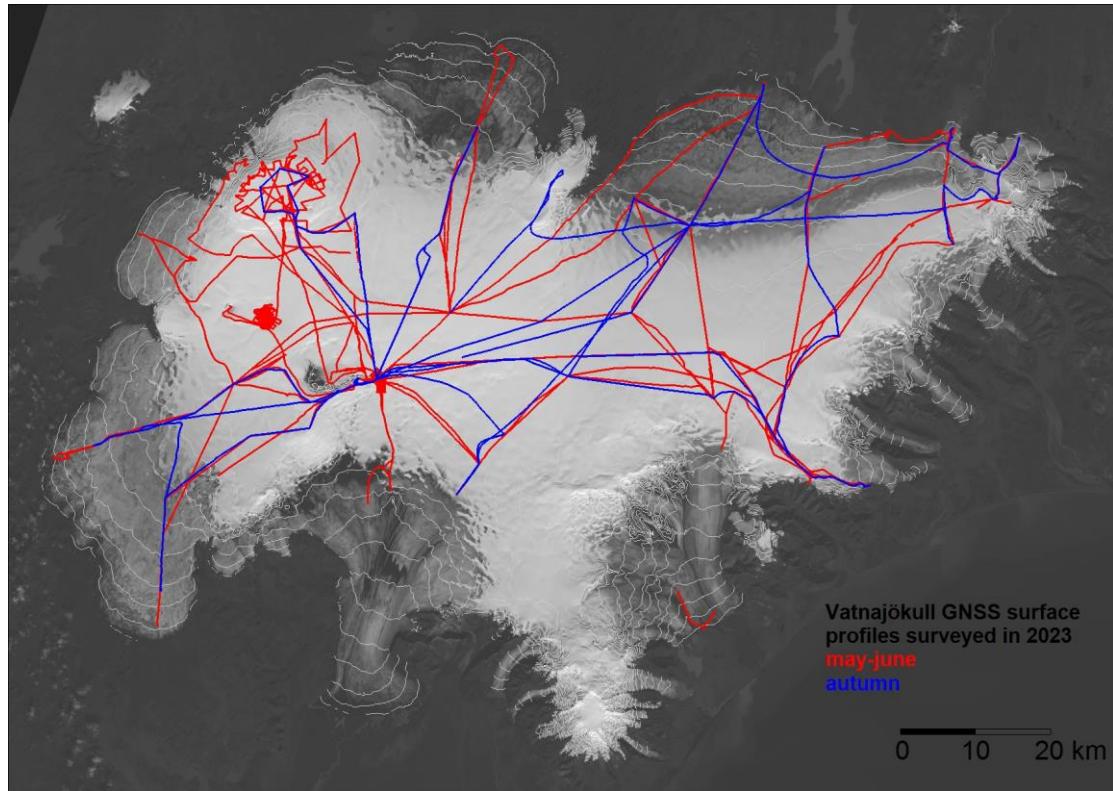
Figure 21. shows the average summer velocity and elevation change record at the survey sites on Eyjabakkajökull. There is a steady increase in velocity at sites E01 and E02 since about 2018. This may be caused by the rapid recession of the glacier snout, and thus steeper surface slopes, formation of a frontal lake and the floating of the ice front. This might be signs of a starting surge, but then speed up at E03 would be expected, which is not the case. Images of velocity and elevation records for other mb survey sites are displayed in Appendix F. Most vehicles used in the survey expeditions are equipped with survey type GNSS instruments that collect data while driving. These are post-processed, to yield surface profiles with an accuracy of  $\sim$ dm in horizontal and vertical. Location of all profiles surveyed in 2023 is shown in figure 22. The profiles have proved of high importance to increase accuracy of remote sensing-based surface DEMs.



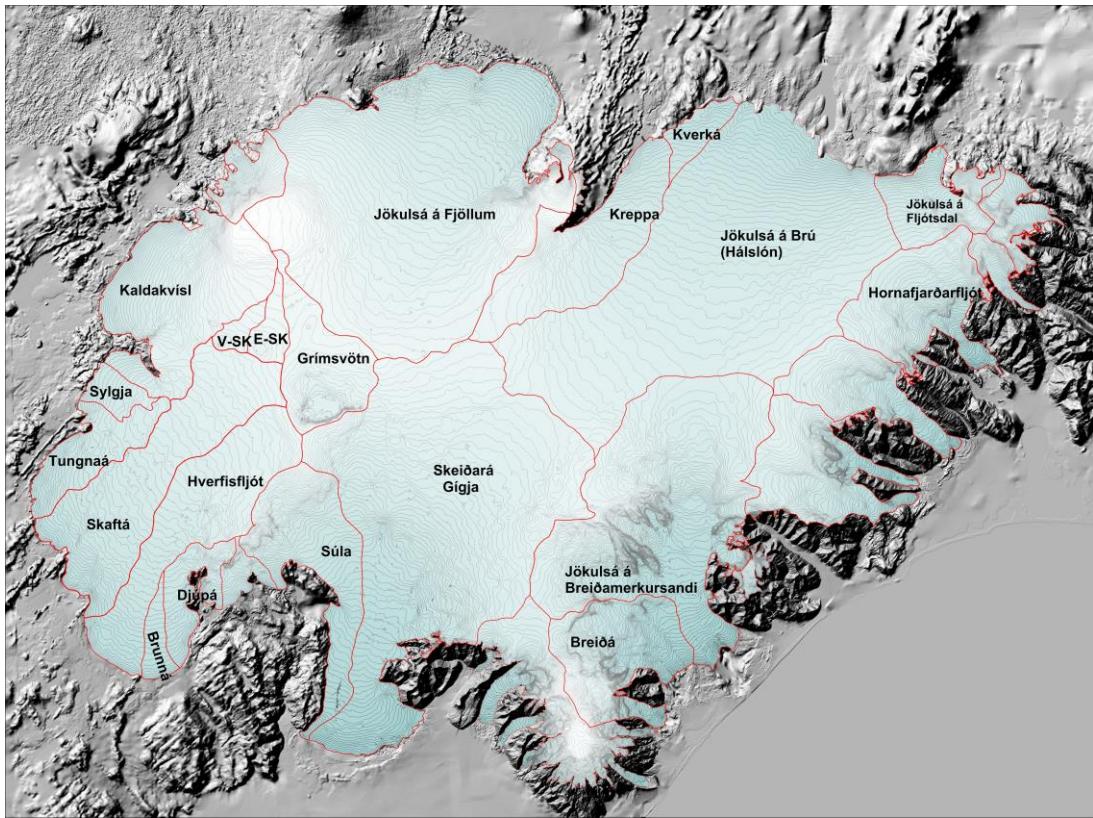
*Figure 20. Surface elevation change relative to summer 2011 (upper panel) and average surface velocity (lower panel) at mb sites on Dyngjujökull in 1992 to 2023.*



*Figure 21. Surface elevation change relative to summer 2010 (upper panel) and average surface velocity (lower panel) at mb sites on Eyjabakkajökull in 1995 to 2023.*



*Figure 22. Location of surface elevation profiles surveyed in field trips on Vatnajökull in 2023. Survey in spring is shown in red and autumn survey in blue.*



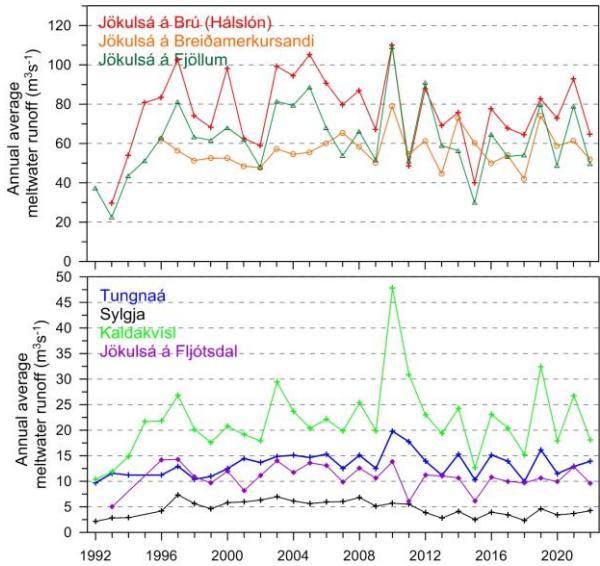
*Figure 23. Water divides and drainage basins of selected rivers draining water from Vatnajökull, Súla is since summer 2016 diverted to Gígja.*

## 5. Melt water runoff.

Water divides and drainage basins for rivers draining water from Vatnajökull have been defined from water pressure potential maps. The potential maps were produced from surface (year 2010) and bedrock DEMs.

Figure 23. shows the water divides and drainage areas for selected rivers draining melt water from Vatnajökull. The summer balance over the water basin is an estimate of meltwater contribution to rivers and groundwater storage. This estimate, however, does not include precipitation that falls as rain on the glacier, or snow that falls and melts during the summer. The meltwater contribution can be compared with river runoff at stream flow gauges closest to the glacier. For this comparison, we define the glaciological year from the start of October to the end of September and the period draining meltwater from the

glacier during the summer from June through September. It would be misleading to include May in the summer period because runoff from the glacier melt in May is delayed due



*Figure 24. The temporal variation of average annual meltwater runoff to selected river catchments.*

**Table I. Melt water drainage to selected rivers in summer 2023.**

| Water Catchment:            | Area<br>(km <sup>2</sup> ) | $\Sigma Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $Q_s$<br>(m <sup>3</sup> s <sup>-1</sup> ) | $Q_a$<br>(m <sup>3</sup> s <sup>-1</sup> ) | $q_s$<br>(ls <sup>-1</sup> km <sup>-2</sup> ) |
|-----------------------------|----------------------------|---|--|--|---|
| Vatnajökull                 | 7570                       | 18747   | 1778,5                                     | 594,5                                      | 78,5  |
| Tungnaá                     | 104                        | 388   | 36,8                                       | 12,3                                       | 117,7   |
| Sylgja                      | 38                         | 122   | 11,5                                       | 3,9  | 102,1   |
| Kaldakvísl                  | 328                        | 656   | 62,2                                       | 20,8                                       | 63,5  |
| Jökulsá á Fjöllum           | 1109                       | 1959  | 185,8                                      | 62,1                                       | 56,0  |
| Kreppa                      | 287                        | 522   | 49,5                                       | 16,5                                       | 57,6  |
| Kverka                      | 34                         | 177   | 16,8                                       | 5,6  | 164,9   |
| Háslón                      | 1186                       | 2681  | 254,3                                      | 85,0                                       | 71,7  |
| Jökulsá á Fljótsdal         | 121                        | 386   | 36,6                                       | 12,2                                       | 101,6   |
| Jökulsá í Lóni              | 92                         | 289   | 27,4                                       | 9,2  | 99,4  |
| Hornafjarðarfjlót           | 227                        | 631   | 59,9                                       | 20,0                                       | 88,0  |
| Jökulsá á Breiðamerkursandi | 686                        | 1783  | 169,1                                      | 56,5                                       | 82,4  |
| Breiðá-Fjallsá              | 220                        | 955   | 90,6                                       | 30,3                                       | 137,6   |
| Gígia                       | 1383                       | 3707  | 351,7                                      | 117,6                                      | 85,0  |
| Brunná                      | 30                         | 166   | 15,8                                       | 5,3  | 176,7   |
| Djúpá                       | 70                         | 296   | 28,1                                       | 9,4  | 133,9   |
| Hverfisfljót                | 306                        | 765   | 72,6                                       | 24,3                                       | 79,3  |
| Skaftá                      | 380                        | 1047  | 99,3                                       | 33,2                                       | 87,3  |
| Grímsvötn                   | 171                        | 133   | 12,6                                       | 4,2  | 24,6  |
| Eystri Skaftárketill        | 39                         | 20  | 1,9  | 0,6  | 16,1  |
| Vestari Skaftárketill       | 25                         | 15  | 1,4  | 0,5  | 19,0  |
| Hólmsá                      | 157                        | 463   | 43,9                                       | 14,7                                       | 93,7  |
| Heinabergsvötn              | 214                        | 649   | 61,6                                       | 20,6                                       | 96,4  |
| Skjálfandafljót             | 89                         | 88  | 8,3  | 2,8  | 31,2  |

$\Sigma Q_s$ : total summer melt water;  $Q_s$ : average runoff (averaged over summer, 4 months, June – September)  
 $Q_a$ : average runoff (averaged over a whole year);  $q_s$ : average runoff per km<sup>2</sup> (averaged over a whole year)

to refreezing during elimination of the cold wave and because of the contribution of the spring snow melt from the highlands to the runoff. Some melting also occurs during winter, especially in the terminus regions of the southern outlets.

Average melt water runoff to different rivers is given in Table I, and temporal variation of the average meltwater runoff in Fig. 24. The average specific runoff ( $q_s$ ) differs from basin to basin from ~31 to ~176 ls<sup>-1</sup>km<sup>-2</sup>. This is mainly due to different elevation distributions, for example, the water drainage basins for Tungnaá, Brunná and Kverká are within the ablation zone, while that of Grímsvötn and Skaftárkatlar are high in the accumulation zone.

Runoff as function of elevation, estimated from summer balance, is tabulated for individual water catchments in Appendix E.

## 6. Conclusions

In the glaciological year 2022\_23 the winter balance for Vatnajökull was ~90% of the average in the observation period from 1991\_92. Only 7 winters of the survey period have had lower winter balance, but 9 out the 12 recent years have had higher than average winter balance. The average winter balance is 1.63 m<sub>we</sub> and standard variability is 0.28 m<sub>we</sub>.

The total summer surface mass loss was 12% over the average since 1995 (19% more than average since 1991\_92). During the survey period, only five summers had more surface mass loss. The average summer balance is -2.09 m<sub>we</sub>, and the standard variability 0.56 m<sub>we</sub>.

The net balance was negative by 2.25-fold that of the average, and only 7 years have had more surface mass loss. The average net balance is -0.46 m<sub>we</sub>, and the standard variability 0.56 m<sub>we</sub>. Since 2010, after the 15-year period of high mass loss, the summer and net balance have been highly variable, even one year with positive mass balance in 2014\_15 and close to zero in 2010\_11, 2016\_17, 2017\_18 and 2021\_22. In contrast 2018\_19 and 2020\_21 are both among years with highest surface mass loss of the survey period. It is also noteworthy that 5 years out of the last decade have had more mass loss than the average of the whole survey period.

The cumulative mb for Vatnajökull is very similar to Köldukvíslarjökull, with a slope of -0.75 m<sub>wea</sub><sup>-1</sup> in the period of high mass loss, but -0.35 m<sub>wea</sub><sup>-1</sup> in the period after 2010.

During the survey period starting in 1991\_92 Vatnajökull has lost ~131 km<sup>3</sup> of ice or thinned ~15 m due to surface mass loss (summing from the start of high mass loss in 1994\_95

yields 159 km<sup>3</sup> or 19 m thinning).

In addition, non-surface mass loss is estimated (calving, geothermal melt, internal friction, eruptions) ~0.21 m<sub>we</sub> for Vatnajökull in a paper by Tómas Jóhannesson and others (Jóhannesson, T., Pálmarsson, B., Hjartarson, Á., Jarosch, A., Magnússon, E., Belart,J., et al. (2020). Non-surface mass balance of glaciers in Iceland. *J. Glaciol.* 66,685–697. doi:10.1017/jog.2020.37) which amounts to an ice loss of ~59 km<sup>3</sup> or 7.7 m average thinning since 1994\_95.

Glacier surface meltwater runoff in summer 2023 (estimated from summer surface balance only, summer rain and snow that falls and melts during summer, calving and geothermal and internal melting, is not included): to Tungnaá 97% of the average, 103% of the average to Kaldakvísl, 105% of the average to Jökulsá á Fjöllum, 120% of the average to Háslón, 122% to Jökulsá í Fljótsdal and 108% to Jökulsá á Breiðamerkursandi. (Averages refer to the survey period of each outlet.)

Surface velocity measurements suggest that Dyngjujökull is in the first phase of a surge and may complete a surge cycle within the next few years.

## Surface mass balance summary 2022\_23:

$$B_w = 11.10 \text{ km}^3 \text{we}$$

$$B_s = -18.74 \text{ km}^3 \text{we}$$

$$B_n = -7.64 \text{ km}^3 \text{we}$$

$$AAR = 53\%$$

## Specific Values:

$$b_w = 1.46 \text{ mwe}$$

$$b_s = -2.47 \text{ mwe}$$

$$b_n = -1.01 \text{ mwe}$$

$$b_{n(including other mass loss)} = -1.22 \text{ mwe}$$

## Appendix A: Surface mass balance at measurement sites 2022\_23.

**b<sub>w</sub>**: specific winter balance, **b<sub>s</sub>**: specific summer balance, **b<sub>n</sub>**: specific net balance,  
**l<sub>a</sub>**: new snow in autumn (all in water equivalent).

| Site    | Position |           | Elévation  | Date      | Date      | b <sub>w</sub> | b <sub>s</sub> | b <sub>n</sub> | l <sub>a</sub> |        |      |
|---------|----------|-----------|------------|-----------|-----------|----------------|----------------|----------------|----------------|--------|------|
|         | Latitude | Longitude | (m a.s.l.) | in spring | in autumn | (m)            | (m)            | (m)            | (m)            |        |      |
| B09-23  | 64       | 44,483    | 16         | 6,1882    | 726,3     | 20230505       | 20231024       | 0,09           | -6,444         | -6,354 | 0,02 |
| B10-23  | 64       | 43,682    | 16         | 6,7041    | 757,2     | 20230505       | 20231024       | 0,11           | -5,744         | -5,634 | 0,04 |
| B11-23  | 64       | 40,939    | 16         | 10,484    | 944,6     | 20230505       | 20231024       | 0,995          | -4,559         | -3,564 | 0,16 |
| B12-23  | 64       | 38,262    | 16         | 14,149    | 1078      | 20230505       | 20231024       | 0,974          | -3,665         | -2,691 | 0,25 |
| B13-23  | 64       | 34,578    | 16         | 19,637    | 1222      | 20230504       | 20231026       | 1,63           | -2,008         | -0,378 | 0,35 |
| B14-23  | 64       | 31,65     | 16         | 24,772    | 1324      | 20230504       | 20231023       | 1,609          | -1,303         | 0,306  | 0,35 |
| B15-23  | 64       | 28,513    | 16         | 30,032    | 1406      | 20230504       | 20231024       | 1,93           | -1,114         | 0,816  | 0,35 |
| B16-23  | 64       | 24,123    | 16         | 40,92     | 1529      | 20230508       | 20231023       | 1,862          | -0,776         | 1,086  | 0,38 |
| B17-23  | 64       | 36,733    | 16         | 28,797    | 1217      | 20230504       | 20231023       | 1,082          | -2,747         | -1,665 | 0,39 |
| Br1-23  | 64       | 5,9586    | 16         | 19,82     | 70,04     | 20230501       | 20231022       | -2,99          | -9,198         | -12,19 | 0    |
| Br2-23  | 64       | 6,354     | 16         | 22,523    | 150       | 20230501       | 20231022       | -2,39          | -9,108         | -11,5  | 0    |
| Br3-23  | 64       | 8,4131    | 16         | 23,971    | 348,4     | 20230501       | 20231022       | -0,82          | -7,434         | -8,254 | 0    |
| Br7-23  | 64       | 22,143    | 16         | 16,939    | 1245      | 20230504       | 20231023       | 1,98           | -1,542         | 0,438  | 0,21 |
| B07-23  | 64       | 25,797    | 16         | 17,481    | 1359      | 20230504       | 20231027       | 2,001          | -1,341         | 0,66   | 0,34 |
| Bb0-23  | 64       | 22,707    | 16         | 5,0412    | 1519      | 20230504       | 20231023       | 2,55           | -0,906         | 1,644  | 0,46 |
| Bru-23  | 64       | 39,753    | 15         | 56,535    | 891,4     | 20230503       | 20231023       | 0,679          | -4,738         | -4,059 | 0,12 |
| Bud-23  | 64       | 35,99     | 15         | 59,887    | 1138      | 20230503       | 20231023       | 1,608          | -3,084         | -1,476 | 0,37 |
| B18-23  | 64       | 31,577    | 16         | 0,1205    | 1317      | 20230503       | 20231023       | 2,002          | -1,444         | 0,558  | 0,4  |
| B19-23  | 64       | 27,978    | 15         | 56,008    | 1441      | 20230503       | 20231023       | 2,906          | -0,506         | 2,4    | 0,37 |
| D01-23  | 64       | 47,868    | 16         | 49,975    | 839,5     | 20230505       |                | 0,45           |                |        | 0    |
| D05-23  | 64       | 42,225    | 16         | 54,689    | 1207      | 20230505       | 20231026       | 0,96           | -3,147         | -2,187 | 0,35 |
| D07-23  | 64       | 38,289    | 16         | 59,258    | 1379      | 20230505       | 20231026       | 1,876          | -1,222         | 0,654  | 0,36 |
| D09-23  | 64       | 34,682    | 17         | 1,5194    | 1489      | 20230505       | 20231026       | 2,025          | -1,005         | 1,02   | 0,32 |
| D12-23  | 64       | 28,975    | 17         | 0,1844    | 1652      | 20230505       | 20231024       | 1,905          | -0,501         | 1,404  | 0,29 |
| E01-22  | 64       | 40,65     | 15         | 34,843    | 751,7     | 20230503       | 20231024       | 0,455          | -5,72          | -5,265 | 0,02 |
| E02-23  | 64       | 39,108    | 15         | 35,996    | 950,1     | 20230503       | 20231024       | 0,999          | -4,77          | -3,771 | 0,11 |
| E03-23  | 64       | 36,603    | 15         | 36,902    | 1192      | 20230503       | 20231024       | 2,385          | -2,959         | -0,574 | 0,35 |
| E04-23  | 64       | 34,938    | 15         | 37,179    | 1289      | 20230503       | 20231024       | 2,415          | -1,803         | 0,612  | 0,32 |
| K01-23  | 64       | 35,177    | 17         | 51,88     | 1036      | 20230506       | 20231025       | 0,265          | -4,765         | -4,5   | 0,04 |
| K02-23  | 64       | 34,804    | 17         | 49,677    | 1168      | 20230506       | 20231025       | 0,902          | -3,773         | -2,871 | 0,16 |
| K03-23  | 64       | 34,234    | 17         | 46,393    | 1292      | 20230506       | 20231025       | 1,083          | -3,036         | -1,953 | 0,2  |
| K04-23  | 64       | 33,211    | 17         | 42,246    | 1487      | 20230506       | 20231025       | 1,38           | -1,296         | 0,084  | 0,13 |
| K05-23  | 64       | 33,446    | 17         | 35,458    | 1679      | 20230506       | 20231025       | 1,558          | -0,568         | 0,99   | 0,28 |
| K06-23  | 64       | 38,354    | 17         | 31,313    | 1946      | 20230506       | 20231024       | 2,27           | 0,442          | 2,712  | 0,42 |
| K07-23  | 64       | 29,115    | 17         | 42,036    | 1531      | 20230506       | 20231025       | 1,357          | -1,015         | 0,342  | 0,27 |
| S01-23  | 64       | 7,0163    | 17         | 49,974    | 698,6     | 20230506       |                | 0,143          |                |        |      |
| S02-23  | 64       | 12,165    | 17         | 48,986    | 999,4     | 20230506       | 20231025       | 1,236          | -4,233         | -2,997 | 0,08 |
| S04-23  | 64       | 16,181    | 17         | 48,192    | 1156      | 20230506       | 20231025       | 1,487          | -3,125         | -1,638 | 0,14 |
| S05-23  | 64       | 20,515    | 17         | 33,993    | 1451      | 20230506       | 20231025       | 2,176          | -1,132         | 1,044  | 0,27 |
| Haab-23 | 64       | 20,966    | 17         | 24,11     | 1731      | 20230506       | 20231025       | 2,342          | -0,242         | 2,1    | 0,27 |

|          |    |         |    |         |       |          |          |       |             |        |       |  |
|----------|----|---------|----|---------|-------|----------|----------|-------|-------------|--------|-------|--|
| T01-23   | 64 | 19,155  | 18 | 6,5245  | 761   | 20230507 |          | 0     |             |        |       |  |
| T02-23   | 64 | 19,479  | 18 | 4,5473  | 880,8 | 20230507 | 20231025 | 0,176 | -4,937      | -4,761 | 0     |  |
| T03-23   | 64 | 20,199  | 17 | 58,611  | 1062  | 20230507 | 20231025 | 0,633 | -4,08       | -3,447 | 0,02  |  |
| T04-23   | 64 | 21,336  | 17 | 51,529  | 1219  | 20230507 | 20231025 | 1,38  | -2,604      | -1,224 | 0,12  |  |
| T05-23   | 64 | 22,263  | 17 | 43,003  | 1344  | 20230507 | 20231025 | 1,638 | -1,652      | -0,014 | 0,18  |  |
| T06-23   | 64 | 24,271  | 17 | 36,527  | 1468  | 20230506 | 20231025 | 1,889 | -0,839      | 1,05   | 0,2   |  |
| T07-23   | 64 | 25,293  | 17 | 31,215  | 1564  | 20230506 | 20231025 | 1,997 | -0,743      | 1,254  | 0,21  |  |
| T08-23   | 64 | 26,298  | 17 | 27,756  | 1637  | 20230506 | 20231025 | 1,94  | -0,596      | 1,344  | 0,26  |  |
| Bor-23   | 64 | 24,938  | 17 | 20,154  | 1412  | 20230602 | 20231027 | 2,37  | -1,938      | 0,432  | 0,27  |  |
| Borth-23 | 64 | 24,991  | 17 | 19,202  | 1410  | 20230507 | 20231027 | 2,19  | -1,626      | 0,564  | 0,27  |  |
| G02-23   | 64 | 26,847  | 17 | 17,718  | 1568  | 20230507 | 20231024 | 1,885 | -0,787      | 1,098  | 0,15  |  |
| G03-23   | 64 | 28,442  | 17 | 16,335  | 1662  | 20230507 | 20231024 | 2,008 | -0,628      | 1,38   | 0,26  |  |
| G04-23   | 64 | 30,025  | 17 | 15,027  | 1691  | 20230506 | 20231024 | 1,909 | -0,523      | 1,386  | 0,35  |  |
| Go1-23   | 64 | 33,967  | 17 | 24,927  | 1762  | 20230506 | 20231024 | 1,715 | -0,485      | 1,23   | 0,37  |  |
| Skf00-23 | 64 | 15,481  | 15 | 54,096  | 945   | 20230502 | 20231023 | 1,66  | -3,883      | -2,223 | 0,09  |  |
| Hof01-23 | 64 | 32,349  | 15 | 35,83   | 1143  | 20230503 | 20231024 | 2,04  | -2,257      | -0,217 | 0,18  |  |
| Skf01-23 | 64 | 18,017  | 16 | 5,0229  | 1283  | 20230503 | 20231023 | 2,88  | -1,532      | 1,348  | 1,13  |  |
| Fl01-23  | 64 | 26,164  | 15 | 55,632  | 1349  | 20230503 | 20231023 | 3,16  | -1,252      | 1,908  | 0,27  |  |
| Ske02-23 | 64 | 15,912  | 17 | 0,0657  | 1179  | 20230508 |          | 1,603 | fannst ekki |        |       |  |
| Ske03-23 | 64 | 18,053  | 16 | 56,162  | 1298  | 20230508 | 20231026 | 1,94  | -1,586      | 0,354  | 0,35  |  |
| Ske04-23 | 64 | 20,146  | 16 | 51,806  | 1400  | 20230508 | 20231026 | 1,773 | -1,299      | 0,474  | 0,25  |  |
| Ske05-23 | 64 | 22,234  | 16 | 47,234  | 1473  | 20230508 | 20231026 | 1,975 | -0,949      | 1,026  | 0,34  |  |
| E07-23   | 64 | 38,412  | 15 | 24,703  | 1070  | 20230503 | 20231024 | 1,966 | -4,099      | -2,133 | 0,26  |  |
| E08-23   | 64 | 39,72   | 15 | 23,848  | 948,4 | 20230503 | 20231024 | 1,254 | -4,476      | -3,222 | 0,07  |  |
| Kverk-23 | 64 | 38,659  | 16 | 40,535  | 1826  | 20230601 | 20231024 | 2,111 | -0,329      | 1,782  | 0,49  |  |
| Barc-23  | 64 | 38,407  | 17 | 26,762  | 1905  | 20230531 | 20231024 | 2,342 | -0,188      | 2,154  | 0,47  |  |
| BB08-23  | 64 | 39,023  | 17 | 23,218  | 1870  | 20230531 | 20231024 | 1,84  |             |        | 0,37  |  |
| BB05-23  | 64 | 36,5909 | 17 | 30,7886 | 1913  | 20230531 | 20231024 | 1,975 |             |        | 0,315 |  |

## Appendix B: Surface mass balance distribution by elevation in 2022\_23.

$\Delta S$  : area in elevation range,  $\sum \Delta S$ : cumulative area above given elevation,  $b_w$ : specific winter balance,  $b_s$ : specific summer balance,  $b_n$ : specific net annual balance,  $\Delta B_w$ : winter balance at a given elevation range,  $\sum \Delta B_w$ : cumulative winter balance above given elevation,  $\Delta B_s$  summer balance at a given elevation range,  $\sum \Delta B_s$ : cumulative summer balance above given elevation,  $\Delta B_n$ : net annual balance in a given elevation range,  $\sum B_n$ : cumulative net annual balance above given elevation.

### Vatnajökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | $b_w$<br>(mm) | $b_s$<br>(mm) | $b_n$<br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|-------------------------|----------------------------------|---------------------------------------|---------------|---------------|---------------|---|--|---|--|---|---|
|-------------------------|----------------------------------|---------------------------------------|---------------|---------------|---------------|---|--|---|--|---|---|

|      |      |      |       |        |       |        |        |        |         |         |          |        |         |
|------|------|------|-------|--------|-------|--------|--------|--------|---------|---------|----------|--------|---------|
| 2000 | 2050 | 2025 | 0,3   | 0,3    | 5251  | -265   | 4986   | 1,8    | 1,8     | -0,1    | -0,1     | 1,7    | 1,7     |
| 1950 | 2000 | 1975 | 6,9   | 7,3    | 2766  | -20    | 2745   | 19,1   | 21,0    | -0,1    | -0,2     | 19,0   | 20,7    |
| 1900 | 1950 | 1925 | 41,3  | 48,6   | 2281  | -25    | 2255   | 94,3   | 115,3   | -1,0    | -1,3     | 93,2   | 114,0   |
| 1850 | 1900 | 1875 | 44,3  | 92,9   | 2457  | -213   | 2243   | 109,0  | 224,2   | -9,5    | -10,8    | 99,5   | 213,5   |
| 1800 | 1850 | 1825 | 45,6  | 138,6  | 2739  | -230   | 2508   | 125,0  | 349,3   | -10,5   | -21,3    | 114,5  | 328,0   |
| 1750 | 1800 | 1775 | 54,8  | 193,4  | 2334  | -325   | 2008   | 128,0  | 477,3   | -17,9   | -39,2    | 110,1  | 438,1   |
| 1700 | 1750 | 1725 | 114,4 | 307,8  | 2011  | -428   | 1582   | 230,1  | 707,4   | -49,0   | -88,2    | 181,1  | 619,2   |
| 1650 | 1700 | 1675 | 217,3 | 525,1  | 2000  | -530   | 1469   | 434,7  | 1142,1  | -115,3  | -203,5   | 319,4  | 938,5   |
| 1600 | 1650 | 1625 | 373,6 | 898,7  | 2009  | -617   | 1392   | 750,7  | 1892,8  | -230,6  | -434,1   | 520,1  | 1458,6  |
| 1550 | 1600 | 1575 | 357,9 | 1256,6 | 2003  | -721   | 1281   | 717,0  | 2609,8  | -258,3  | -692,4   | 458,8  | 1917,4  |
| 1500 | 1550 | 1525 | 421,2 | 1677,8 | 1979  | -842   | 1137   | 834,0  | 3443,8  | -354,9  | -1047,3  | 479,1  | 2396,5  |
| 1450 | 1500 | 1475 | 452,5 | 2130,4 | 2018  | -983   | 1034   | 913,3  | 4357,1  | -445,2  | -1492,5  | 468,1  | 2864,6  |
| 1400 | 1450 | 1425 | 502,9 | 2633,3 | 2086  | -1100  | 986    | 1049,3 | 5406,4  | -553,3  | -2045,8  | 496,0  | 3360,6  |
| 1350 | 1400 | 1375 | 540,3 | 3173,6 | 2044  | -1256  | 787    | 1104,6 | 6511,0  | -678,9  | -2724,7  | 425,7  | 3786,3  |
| 1300 | 1350 | 1325 | 531,3 | 3704,8 | 1959  | -1503  | 456    | 1041,0 | 7552,1  | -798,7  | -3523,5  | 242,3  | 4028,6  |
| 1250 | 1300 | 1275 | 496,7 | 4201,6 | 1875  | -1806  | 69     | 931,6  | 8483,7  | -897,2  | -4420,6  | 34,4   | 4063,0  |
| 1200 | 1250 | 1225 | 435,5 | 4637,1 | 1693  | -2214  | -521   | 737,7  | 9221,4  | -964,7  | -5385,3  | -227,0 | 3836,0  |
| 1150 | 1200 | 1175 | 387,9 | 5025   | 1497  | -2683  | -1186  | 580,7  | 9802,1  | -1041,2 | -6426,5  | -460,4 | 3375,6  |
| 1100 | 1150 | 1125 | 344,1 | 5369,1 | 1323  | -3091  | -1767  | 455,5  | 10257,6 | -1063,5 | -7490,0  | -608,0 | 2767,6  |
| 1050 | 1100 | 1075 | 296,5 | 5665,6 | 1165  | -3459  | -2293  | 345,7  | 10603,3 | -1025,9 | -8515,9  | -680,2 | 2087,4  |
| 1000 | 1050 | 1025 | 276,5 | 5942,1 | 996   | -3809  | -2813  | 275,5  | 10878,7 | -1053,3 | -9569,2  | -777,8 | 1309,6  |
| 950  | 1000 | 975  | 247,4 | 6189,5 | 855   | -4121  | -3265  | 211,6  | 11090,4 | -1019,6 | -10588,8 | -808,0 | 501,5   |
| 900  | 950  | 925  | 214   | 6403,6 | 714   | -4397  | -3682  | 153,0  | 11243,3 | -941,1  | -11529,9 | -788,1 | -286,6  |
| 850  | 900  | 875  | 184,3 | 6587,9 | 566   | -4708  | -4141  | 104,5  | 11347,8 | -867,8  | -12397,7 | -763,3 | -1049,9 |
| 800  | 850  | 825  | 166,7 | 6754,6 | 440   | -5018  | -4577  | 73,4   | 11421,2 | -836,4  | -13234,1 | -763,0 | -1812,9 |
| 750  | 800  | 775  | 145,4 | 6899,9 | 356   | -5299  | -4942  | 51,8   | 11473,1 | -770,3  | -14004,4 | -718,5 | -2531,4 |
| 700  | 750  | 725  | 114,8 | 7014,8 | 280   | -5562  | -5281  | 32,2   | 11505,2 | -638,8  | -14643,2 | -606,6 | -3138,0 |
| 650  | 700  | 675  | 95,1  | 7109,9 | 188   | -5746  | -5558  | 17,9   | 11523,2 | -546,6  | -15189,8 | -528,7 | -3666,6 |
| 600  | 650  | 625  | 64,3  | 7174,2 | 115   | -5818  | -5702  | 7,5    | 11530,6 | -374,3  | -15564,1 | -366,9 | -4033,5 |
| 550  | 600  | 575  | 52,7  | 7226,9 | 2     | -6004  | -6002  | 0,1    | 11530,7 | -316,6  | -15880,7 | -316,5 | -4350,0 |
| 500  | 550  | 525  | 53,6  | 7280,5 | -142  | -6307  | -6449  | -7,6   | 11523,1 | -338,0  | -16218,7 | -345,6 | -4695,6 |
| 450  | 500  | 475  | 37,9  | 7318,4 | -289  | -6623  | -6912  | -11,0  | 11512,1 | -250,9  | -16469,6 | -261,9 | -4957,5 |
| 400  | 450  | 425  | 34,7  | 7353,2 | -453  | -6895  | -7348  | -15,7  | 11496,4 | -239,5  | -16709,2 | -255,3 | -5212,8 |
| 350  | 400  | 375  | 38,9  | 7392   | -652  | -7218  | -7871  | -25,4  | 11471,0 | -280,6  | -16989,7 | -305,9 | -5518,7 |
| 300  | 350  | 325  | 35,2  | 7427,2 | -870  | -7640  | -8511  | -30,6  | 11440,4 | -268,7  | -17258,4 | -299,3 | -5818,0 |
| 250  | 300  | 275  | 31,9  | 7459,1 | -1147 | -8030  | -9177  | -36,6  | 11403,8 | -256,2  | -17514,7 | -292,8 | -6110,9 |
| 200  | 250  | 225  | 30,7  | 7489,8 | -1526 | -8406  | -9933  | -46,8  | 11357,0 | -257,8  | -17772,5 | -304,7 | -6415,5 |
| 150  | 200  | 175  | 29,6  | 7519,4 | -1900 | -8769  | -10670 | -56,3  | 11300,7 | -259,9  | -18032,4 | -316,2 | -6731,7 |
| 100  | 150  | 125  | 28,2  | 7547,6 | -2288 | -9124  | -11413 | -64,5  | 11236,1 | -257,3  | -18289,6 | -321,8 | -7053,5 |
| 50   | 100  | 75   | 22,2  | 7569,8 | -2626 | -9484  | -12111 | -58,3  | 11177,8 | -210,5  | -18500,1 | -268,8 | -7322,3 |
| 0    | 50   | 25   | 24,1  | 7593,9 | -3074 | -10150 | -13224 | -74,0  | 11103,8 | -244,4  | -18744,5 | -318,4 | -7640,7 |

### Tungnaárjökull

| Elevation<br>( m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |       |        |
|--------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|-------|--------|
| 1650                     | 1700                             | 1675                                  | 1,7                    | 1,7                    | 1923                   | -579  | 1343   | 3,3   | 3,3  | -1,0  | -1,0  | 2,3   | 2,3    |
| 1600                     | 1650                             | 1625                                  | 12,3                   | 14                     | 1901                   | -603  | 1297   | 23,4  | 26,7   | -7,4  | -8,4  | 16,0  | 18,3   |
| 1550                     | 1600                             | 1575                                  | 16,3                   | 30,4                   | 1856                   | -679  | 1176   | 30,3  | 57,0   | -11,1   | -19,5   | 19,2  | 37,5   |
| 1500                     | 1550                             | 1525                                  | 16,1                   | 46,4                   | 1826                   | -775  | 1050   | 29,3  | 86,3   | -12,5   | -32,0   | 16,9  | 54,4   |
| 1450                     | 1500                             | 1475                                  | 18,3                   | 64,7                   | 1775                   | -867  | 908  | 32,5  | 118,9  | -15,9   | -47,9   | 16,6  | 71,0   |
| 1400                     | 1450                             | 1425                                  | 23                     | 87,8                   | 1754                   | -1116   | 638  | 40,4  | 159,3  | -25,7   | -73,6   | 14,7  | 85,7   |
| 1350                     | 1400                             | 1375                                  | 21                     | 108,8                  | 1675                   | -1483   | 192  | 35,2  | 194,5  | -31,2   | -104,7  | 4,0   | 89,7   |
| 1300                     | 1350                             | 1325                                  | 27,1                   | 135,9                  | 1585                   | -1861   | -275   | 43,0  | 237,4  | -50,4   | -155,2  | -7,5  | 82,3   |
| 1250                     | 1300                             | 1275                                  | 20,3                   | 156,2                  | 1502                   | -2214   | -711   | 30,5  | 268,0  | -45,0   | -200,2  | -14,5 | 67,8   |
| 1200                     | 1250                             | 1225                                  | 22,2                   | 178,4                  | 1368                   | -2576   | -1207  | 30,4  | 298,4  | -57,2   | -257,4  | -26,8 | 41,0   |
| 1150                     | 1200                             | 1175                                  | 21                     | 199,4                  | 1175                   | -2935   | -1759  | 24,7  | 323,0  | -61,6   | -319,0  | -36,9 | 4,1    |
| 1100                     | 1150                             | 1125                                  | 17,6                   | 217                    | 935                    | -3266   | -2331  | 16,5  | 339,6  | -57,6   | -376,6  | -41,1 | -37,1  |
| 1050                     | 1100                             | 1075                                  | 16,4                   | 233,4                  | 730                    | -3614   | -2884  | 12,0  | 351,6  | -59,4   | -436,0  | -47,4 | -84,5  |
| 1000                     | 1050                             | 1025                                  | 16,7                   | 250,2                  | 579                    | -4001   | -3421  | 9,7   | 361,3  | -66,9   | -503,0  | -57,2 | -141,7 |
| 950                      | 1000                             | 975                                   | 15,6                   | 265,8                  | 445                    | -4362   | -3917  | 7,0   | 368,2  | -68,2   | -571,1  | -61,2 | -202,9 |
| 900                      | 950                              | 925                                   | 16                     | 281,8                  | 315                    | -4694   | -4378  | 5,1   | 373,3  | -75,3   | -646,4  | -70,2 | -273,1 |
| 850                      | 900                              | 875                                   | 12,4                   | 294,3                  | 205                    | -5020   | -4814  | 2,5   | 375,8  | -62,4   | -708,7  | -59,8 | -332,9 |
| 800                      | 850                              | 825                                   | 12,1                   | 306,3                  | 105                    | -5327   | -5222  | 1,3   | 377,1  | -64,2   | -773,0  | -63,0 | -395,9 |
| 750                      | 800                              | 775                                   | 9,7                    | 316                    | -8                     | -5632   | -5640  | -0,1  | 377,0  | -54,4   | -827,4  | -54,5 | -450,4 |
| 700                      | 750                              | 725                                   | 6,1                    | 322                    | -123                   | -5904   | -6027  | -0,7  | 376,3  | -35,8   | -863,1  | -36,5 | -486,9 |
| 650                      | 700                              | 675                                   | 1,2                    | 323,2                  | -199                   | -6191   | -6391  | -0,2  | 376,0  | -7,2  | -870,3  | -7,4  | -494,3 |

### Sylgjujökull

| Elevation<br>( m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |       |        |
|--------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|-------|--------|
| 1600                     | 1650                             | 1625                                  | 1,4                    | 1,4                    | 1700                   | -626  | 1074   | 2,3   | 2,3  | -0,9  | -0,9  | 1,5   | 1,5    |
| 1550                     | 1600                             | 1575                                  | 5,1                    | 6,5                    | 1661                   | -702  | 959  | 8,5   | 10,8   | -3,6  | -4,4  | 4,9   | 6,4    |
| 1500                     | 1550                             | 1525                                  | 18,8                   | 25,3                   | 1530                   | -880  | 649  | 28,8  | 39,6   | -16,6   | -21,0   | 12,2  | 18,6   |
| 1450                     | 1500                             | 1475                                  | 13,4                   | 38,7                   | 1497                   | -1047   | 450  | 20,1  | 59,8   | -14,1   | -35,1   | 6,0   | 24,7   |
| 1400                     | 1450                             | 1425                                  | 8,3                    | 47,1                   | 1499                   | -1281   | 217  | 12,5  | 72,2   | -10,7   | -45,8   | 1,8   | 26,5   |
| 1350                     | 1400                             | 1375                                  | 5,6                    | 52,6                   | 1492                   | -1491   | 1  | 8,3   | 80,6   | -8,3  | -54,1   | 0,0   | 26,5   |
| 1300                     | 1350                             | 1325                                  | 5,1                    | 57,7                   | 1442                   | -1932   | -489   | 7,3   | 87,9   | -9,8  | -63,9   | -2,5  | 24,0   |
| 1250                     | 1300                             | 1275                                  | 9,6                    | 67,3                   | 1322                   | -2355   | -1033  | 12,7  | 100,6  | -22,7   | -86,6   | -9,9  | 14,0   |
| 1200                     | 1250                             | 1225                                  | 11,4                   | 78,7                   | 1165                   | -2685   | -1519  | 13,3  | 113,9  | -30,6   | -117,2  | -17,3 | -3,3   |
| 1150                     | 1200                             | 1175                                  | 12,8                   | 91,5                   | 1000                   | -2966   | -1965  | 12,8  | 126,7  | -38,0   | -155,2  | -25,2 | -28,4  |
| 1100                     | 1150                             | 1125                                  | 12,1                   | 103,6                  | 824                    | -3279   | -2455  | 10,0  | 136,7  | -39,7   | -194,8  | -29,7 | -58,1  |
| 1050                     | 1100                             | 1075                                  | 11,2                   | 114,8                  | 658                    | -3587   | -2928  | 7,3   | 144,0  | -40,0   | -234,8  | -32,7 | -90,8  |
| 1000                     | 1050                             | 1025                                  | 9,9                    | 124,7                  | 464                    | -3888   | -3423  | 4,6   | 148,7  | -38,6   | -273,5  | -34,0 | -124,8 |
| 950                      | 1000                             | 975                                   | 3,1                    | 127,8                  | 410                    | -4184   | -3774  | 1,3   | 149,9  | -13,0   | -286,4  | -11,7 | -136,5 |
| 900                      | 950                              | 925                                   | 1,2                    | 129,1                  | 357                    | -4371   | -4014  | 0,4   | 150,4  | -5,4  | -291,8  | -4,9  | -141,4 |

### Köldukvíslarjökul

| Elevation<br>( m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|--------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|
| 1950                     | 2000                             | 1975                                  | 0,6                    | 0,6                    | 2094                   | 221   | 2315   | 1,4   | 1,4  | 0,1   | 0,1   |
| 1900                     | 1950                             | 1925                                  | 13,7                   | 14,4                   | 1975                   | 23  | 1999   | 27,1  | 28,5   | 0,3   | 0,5   |
| 1850                     | 1900                             | 1875                                  | 6,6                    | 20,9                   | 1830                   | -193  | 1637   | 12,1  | 40,5   | -1,3  | -0,8  |
| 1800                     | 1850                             | 1825                                  | 6,2                    | 27,1                   | 1769                   | -287  | 1482   | 10,9  | 51,5   | -1,8  | -2,6  |
| 1750                     | 1800                             | 1775                                  | 10,1                   | 37,3                   | 1752                   | -349  | 1402   | 17,8  | 69,2   | -3,5  | -6,1  |
| 1700                     | 1750                             | 1725                                  | 17,3                   | 54,6                   | 1660                   | -442  | 1217   | 28,7  | 97,9   | -7,6  | -13,8   |
| 1650                     | 1700                             | 1675                                  | 16                     | 70,5                   | 1571                   | -562  | 1008   | 25,1  | 123,0  | -9,0  | -22,7   |
| 1600                     | 1650                             | 1625                                  | 14,3                   | 84,8                   | 1514                   | -688  | 826  | 21,7  | 144,7  | -9,9  | -32,6   |
| 1550                     | 1600                             | 1575                                  | 18,4                   | 103,3                  | 1463                   | -868  | 594  | 27,0  | 171,7  | -16,0   | -48,6   |
| 1500                     | 1550                             | 1525                                  | 19,9                   | 123,2                  | 1420                   | -1070   | 350  | 28,3  | 200,0  | -21,3   | -69,9   |
| 1450                     | 1500                             | 1475                                  | 19,2                   | 142,4                  | 1388                   | -1298   | 90   | 26,7  | 226,7  | -25,0   | -94,9   |
| 1400                     | 1450                             | 1425                                  | 14,8                   | 157,2                  | 1329                   | -1577   | -248   | 19,7  | 246,4  | -23,4   | -118,3  |
| 1350                     | 1400                             | 1375                                  | 14,7                   | 172                    | 1247                   | -1982   | -735   | 18,4  | 264,7  | -29,2   | -147,5  |
| 1300                     | 1350                             | 1325                                  | 16,3                   | 188,3                  | 1174                   | -2489   | -1315  | 19,1  | 283,9  | -40,5   | -188,1  |
| 1250                     | 1300                             | 1275                                  | 17,3                   | 205,6                  | 1090                   | -2965   | -1875  | 18,9  | 302,8  | -51,4   | -239,4  |
| 1200                     | 1250                             | 1225                                  | 16,5                   | 222,1                  | 963                    | -3320   | -2356  | 15,9  | 318,7  | -54,9   | -294,3  |
| 1150                     | 1200                             | 1175                                  | 15,9                   | 238                    | 776                    | -3633   | -2857  | 12,4  | 331,1  | -57,8   | -352,1  |
| 1100                     | 1150                             | 1125                                  | 14,1                   | 252,1                  | 579                    | -4079   | -3499  | 8,2   | 339,2  | -57,5   | -409,6  |
| 1050                     | 1100                             | 1075                                  | 12,7                   | 264,8                  | 408                    | -4545   | -4137  | 5,2   | 344,4  | -57,5   | -467,1  |
| 1000                     | 1050                             | 1025                                  | 10,2                   | 275                    | 277                    | -4836   | -4559  | 2,8   | 347,2  | -49,4   | -516,5  |
| 950                      | 1000                             | 975                                   | 7,2                    | 282,2                  | 192                    | -4961   | -4769  | 1,4   | 348,6  | -35,9   | -552,5  |
| 900                      | 950                              | 925                                   | 1,2                    | 283,5                  | 139                    | -5024   | -4884  | 0,2   | 348,8  | -6,1  | -558,6  |
|                          |                                  |                                       |                        |                        |                        |   |  |   |  |   | -5,9  |
|                          |                                  |                                       |                        |                        |                        |   |  |   |  |   | -209,8  |

## Dyngjujökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|
| 1950                    | 2000                             | 1975                                  | 2,4                    | 2,4                    | 2081                   | 79  | 2161   | 4,9   | 4,9  | 0,2   | 0,2   |
| 1900                    | 1950                             | 1925                                  | 17,7                   | 20,1                   | 2205                   | 11  | 2216   | 39,0  | 44,0   | 0,2   | 0,4   |
| 1850                    | 1900                             | 1875                                  | 21,7                   | 41,8                   | 2066                   | -192  | 1873   | 44,9  | 88,9   | -4,2  | -3,8  |
| 1800                    | 1850                             | 1825                                  | 13,2                   | 55                     | 1964                   | -278  | 1685   | 25,9  | 114,8  | -3,7  | -7,5  |
| 1750                    | 1800                             | 1775                                  | 15,6                   | 70,7                   | 1916                   | -353  | 1562   | 30,0  | 144,8  | -5,5  | -13,0   |
| 1700                    | 1750                             | 1725                                  | 32,7                   | 103,3                  | 1918                   | -413  | 1504   | 62,7  | 207,5  | -13,5   | -26,5   |
| 1650                    | 1700                             | 1675                                  | 74,5                   | 177,8                  | 1951                   | -507  | 1444   | 145,4   | 352,9  | -37,8   | -64,3   |
| 1600                    | 1650                             | 1625                                  | 120,5                  | 298,3                  | 1987                   | -606  | 1380   | 239,5   | 592,4  | -73,1   | -137,5  |
| 1550                    | 1600                             | 1575                                  | 96,3                   | 394,6                  | 2013                   | -737  | 1275   | 193,9   | 786,3  | -71,1   | -208,5  |
| 1500                    | 1550                             | 1525                                  | 86,8                   | 481,4                  | 2023                   | -889  | 1134   | 175,7   | 962,0  | -77,2   | -285,8  |
| 1450                    | 1500                             | 1475                                  | 72,6                   | 554                    | 2001                   | -1053   | 947  | 145,3   | 1107,2   | -76,5   | -362,2  |
| 1400                    | 1450                             | 1425                                  | 60,3                   | 614,3                  | 1945                   | -1121   | 823  | 117,2   | 1224,4   | -67,6   | -429,8  |
| 1350                    | 1400                             | 1375                                  | 47,7                   | 661,9                  | 1834                   | -1225   | 609  | 87,5  | 1311,9   | -58,4   | -488,2  |
| 1300                    | 1350                             | 1325                                  | 36,1                   | 698                    | 1673                   | -1536   | 137  | 60,4  | 1372,3   | -55,5   | -543,7  |
| 1250                    | 1300                             | 1275                                  | 39,2                   | 737,2                  | 1477                   | -1982   | -505   | 57,9  | 1430,2   | -77,7   | -621,4  |
| 1200                    | 1250                             | 1225                                  | 43,5                   | 780,7                  | 1215                   | -2535   | -1319  | 52,9  | 1483,0   | -110,3  | -731,6  |
| 1150                    | 1200                             | 1175                                  | 43,3                   | 824                    | 914                    | -3209   | -2295  | 39,6  | 1522,6   | -139,0  | -870,6  |
| 1100                    | 1150                             | 1125                                  | 42,3                   | 866,3                  | 667                    | -3809   | -3141  | 28,3  | 1550,9   | -161,3  | -1031,9   |
| 1050                    | 1100                             | 1075                                  | 30,2                   | 896,6                  | 390                    | -4370   | -3979  | 11,8  | 1562,7   | -132,2  | -1164,1   |
| 1000                    | 1050                             | 1025                                  | 30,6                   | 927,2                  | 113                    | -4591   | -4477  | 3,5   | 1566,2   | -140,5  | -1304,6   |
| 950                     | 1000                             | 975                                   | 28,4                   | 955,6                  | -123                   | -4900   | -5024  | -3,5  | 1562,7   | -139,4  | -1444,0   |
| 900                     | 950                              | 925                                   | 24,3                   | 979,9                  | -287                   | -5247   | -5534  | -7,0  | 1555,7   | -127,5  | -1571,5   |
| 850                     | 900                              | 875                                   | 20,4                   | 1000,4                 | -397                   | -5621   | -6018  | -8,1  | 1547,6   | -114,8  | -1686,4   |
| 800                     | 850                              | 825                                   | 16,5                   | 1016,9                 | -476                   | -6237   | -6714  | -7,9  | 1539,7   | -103,0  | -1789,4   |
| 750                     | 800                              | 775                                   | 8,5                    | 1025,4                 | -557                   | -6892   | -7449  | -4,7  | 1535,0   | -58,6   | -1848,0   |
| 700                     | 750                              | 725                                   | 0,3                    | 1025,7                 | -612                   | -7356   | -7968  | -0,2  | 1534,8   | -2,5  | -1850,5   |

## Brúarjökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|
| 1900                    | 1950                             | 1925                                  | 0                      | 0                      | 1971                   | -514  | 1457   | 0,1   | 0,1  | 0,0   | 0,1   |
| 1850                    | 1900                             | 1875                                  | 1,2                    | 1,3                    | 2068                   | -441  | 1627   | 2,5   | 2,6  | -0,5  | -0,6  |
| 1800                    | 1850                             | 1825                                  | 4,4                    | 5,6                    | 2080                   | -344  | 1735   | 9,1   | 11,7   | -1,5  | -2,1  |
| 1750                    | 1800                             | 1775                                  | 2,8                    | 8,5                    | 2048                   | -378  | 1669   | 5,8   | 17,5   | -1,1  | -3,1  |
| 1700                    | 1750                             | 1725                                  | 4                      | 12,5                   | 2040                   | -427  | 1612   | 8,1   | 25,7   | -1,7  | -4,9  |
| 1650                    | 1700                             | 1675                                  | 5,6                    | 18,1                   | 2038                   | -490  | 1547   | 11,4  | 37,1   | -2,8  | -7,6  |
| 1600                    | 1650                             | 1625                                  | 51,6                   | 69,6                   | 2037                   | -632  | 1405   | 105,0   | 142,1  | -32,6   | -40,2   |
| 1550                    | 1600                             | 1575                                  | 47,7                   | 117,3                  | 1992                   | -702  | 1289   | 95,0  | 237,1  | -33,5   | -73,7   |
| 1500                    | 1550                             | 1525                                  | 73,6                   | 190,9                  | 1927                   | -784  | 1143   | 141,8   | 378,9  | -57,7   | -131,4  |
| 1450                    | 1500                             | 1475                                  | 80,1                   | 271                    | 2012                   | -897  | 1115   | 161,3   | 540,2  | -71,9   | -203,3  |
| 1400                    | 1450                             | 1425                                  | 114                    | 385                    | 2166                   | -970  | 1196   | 247,0   | 787,2  | -110,6  | -313,9  |
| 1350                    | 1400                             | 1375                                  | 157,5                  | 542,4                  | 2056                   | -1117   | 939  | 323,9   | 1111,0   | -175,9  | -489,8  |
| 1300                    | 1350                             | 1325                                  | 147,2                  | 689,7                  | 1897                   | -1330   | 567  | 279,4   | 1390,5   | -195,9  | -685,7  |
| 1250                    | 1300                             | 1275                                  | 137,9                  | 827,6                  | 1801                   | -1671   | 130  | 248,5   | 1638,9   | -230,5  | -916,2  |
| 1200                    | 1250                             | 1225                                  | 115,8                  | 943,4                  | 1641                   | -2152   | -510   | 190,1   | 1829,0   | -249,2  | -1165,5   |
| 1150                    | 1200                             | 1175                                  | 99,5                   | 1042,9                 | 1468                   | -2739   | -1270  | 146,1   | 1975,1   | -272,5  | -1438,0   |
| 1100                    | 1150                             | 1125                                  | 80,2                   | 1123,1                 | 1289                   | -3230   | -1940  | 103,4   | 2078,6   | -259,0  | -1697,0   |
| 1050                    | 1100                             | 1075                                  | 64,9                   | 1188                   | 1106                   | -3628   | -2521  | 71,8  | 2150,4   | -235,6  | -1932,5   |
| 1000                    | 1050                             | 1025                                  | 57,2                   | 1245,2                 | 900                    | -3979   | -3079  | 51,4  | 2201,8   | -227,5  | -2160,0   |
| 950                     | 1000                             | 975                                   | 51,6                   | 1296,8                 | 698                    | -4301   | -3602  | 36,1  | 2237,9   | -222,1  | -2382,1   |
| 900                     | 950                              | 925                                   | 44,6                   | 1341,4                 | 542                    | -4607   | -4065  | 24,2  | 2262,1   | -205,5  | -2587,6   |
| 850                     | 900                              | 875                                   | 38,4                   | 1379,8                 | 415                    | -4922   | -4506  | 15,9  | 2278,0   | -188,8  | -2776,5   |
| 800                     | 850                              | 825                                   | 34,2                   | 1414                   | 317                    | -5259   | -4941  | 10,9  | 2288,9   | -180,1  | -2956,6   |
| 750                     | 800                              | 775                                   | 30,9                   | 1444,9                 | 229                    | -5655   | -5426  | 7,1   | 2296,0   | -175,0  | -3131,5   |
| 700                     | 750                              | 725                                   | 26,1                   | 1471                   | 157                    | -6132   | -5974  | 4,1   | 2300,1   | -160,0  | -3291,6   |
| 650                     | 700                              | 675                                   | 9,5                    | 1480,6                 | 92                     | -6494   | -6401  | 0,9   | 2301,0   | -62,0   | -3353,6   |
| 600                     | 650                              | 625                                   | 0,5                    | 1481,1                 | 38                     | -6836   | -6797  | 0,0   | 2301,0   | -3,3  | -3356,9   |
|                         |                                  |                                       |                        |                        |                        |   |  |   |  | -3,3  | -1055,8   |

## Eyjabakkajökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|
| 1550                    | 1600                             | 1575                                  | 0                      | 0                      | 2799                   | -751  | 2047   | 0,0   | 0,0  | 0,0   | 0,0   |
| 1500                    | 1550                             | 1525                                  | 0,1                    | 0,1                    | 2795                   | -808  | 1986   | 0,2   | 0,3  | -0,1  | -0,1  |
| 1450                    | 1500                             | 1475                                  | 1,1                    | 1,2                    | 2719                   | -1033   | 1685   | 3,0   | 3,3  | -1,2  | -1,2  |
| 1400                    | 1450                             | 1425                                  | 2                      | 3,3                    | 2690                   | -1094   | 1595   | 5,5   | 8,8  | -2,2  | -3,5  |
| 1350                    | 1400                             | 1375                                  | 2,6                    | 5,9                    | 2632                   | -1201   | 1430   | 6,9   | 15,7   | -3,1  | -6,6  |
| 1300                    | 1350                             | 1325                                  | 4,2                    | 10,1                   | 2549                   | -1384   | 1165   | 10,7  | 26,4   | -5,8  | -12,4   |
| 1250                    | 1300                             | 1275                                  | 13,4                   | 23,5                   | 2420                   | -1833   | 586  | 32,4  | 58,8   | -24,5   | -37,0   |
| 1200                    | 1250                             | 1225                                  | 12,4                   | 35,9                   | 2318                   | -2384   | -65  | 28,9  | 87,7   | -29,7   | -66,6   |
| 1150                    | 1200                             | 1175                                  | 13,9                   | 49,8                   | 2108                   | -2978   | -870   | 29,3  | 116,9  | -41,3   | -108,0  |
| 1100                    | 1150                             | 1125                                  | 11,4                   | 61,2                   | 1872                   | -3414   | -1541  | 21,4  | 138,3  | -39,1   | -147,1  |
| 1050                    | 1100                             | 1075                                  | 9,8                    | 71,1                   | 1627                   | -3733   | -2105  | 16,0  | 154,3  | -36,7   | -183,7  |
| 1000                    | 1050                             | 1025                                  | 9,1                    | 80,2                   | 1384                   | -4038   | -2654  | 12,7  | 167,0  | -36,9   | -220,7  |
| 950                     | 1000                             | 975                                   | 7,6                    | 87,8                   | 1139                   | -4387   | -3248  | 8,7   | 175,7  | -33,3   | -254,0  |
| 900                     | 950                              | 925                                   | 5                      | 92,8                   | 930                    | -4710   | -3780  | 4,7   | 180,3  | -23,7   | -277,7  |
| 850                     | 900                              | 875                                   | 3,9                    | 96,7                   | 811                    | -4916   | -4105  | 3,2   | 183,5  | -19,2   | -297,0  |
| 800                     | 850                              | 825                                   | 2,9                    | 99,6                   | 731                    | -5142   | -4410  | 2,1   | 185,6  | -14,7   | -311,7  |
| 750                     | 800                              | 775                                   | 1,8                    | 101,4                  | 626                    | -5483   | -4856  | 1,1   | 186,7  | -9,6  | -321,3  |
| 700                     | 750                              | 725                                   | 1,6                    | 103                    | 514                    | -5752   | -5237  | 0,8   | 187,6  | -9,4  | -330,7  |
| 650                     | 700                              | 675                                   | 0,6                    | 103,6                  | 370                    | -6105   | -5734  | 0,2   | 187,8  | -3,9  | -334,6  |
|                         |                                  |                                       |                        |                        |                        |   |  |   |  | -3,7  | -146,8  |

## Hoffellsjökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\Sigma \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |        |
|-------------------------|----------------------------------|---|------------------------|------------------------|------------------------|---|--|---|--|---|---|--------|
| 1450                    | 1500                             | 1475                                    | 1,2                    | 1,2                    | 2755                   | -1041   | 1714   | 3,2   | 3,2  | -1,2  | -1,2  | 2,0    |
| 1400                    | 1450                             | 1425                                    | 7,3                    | 8,4                    | 2853                   | -954  | 1899   | 20,8  | 24,0   | -6,9  | -8,2  | 13,8   |
| 1350                    | 1400                             | 1375                                    | 9,8                    | 18,3                   | 2781                   | -1073   | 1707   | 27,4  | 51,4   | -10,6   | -18,7   | 16,8   |
| 1300                    | 1350                             | 1325                                    | 16,1                   | 34,4                   | 2696                   | -1287   | 1409   | 43,4  | 94,8   | -20,7   | -39,4   | 22,7   |
| 1250                    | 1300                             | 1275                                    | 34,4                   | 68,7                   | 2418                   | -1632   | 786  | 83,1  | 177,9  | -56,1   | -95,5   | 27,0   |
| 1200                    | 1250                             | 1225                                    | 25,5                   | 94,3                   | 2257                   | -1800   | 457  | 57,6  | 235,5  | -46,0   | -141,5  | 11,7   |
| 1150                    | 1200                             | 1175                                    | 17,6                   | 111,9                  | 2041                   | -2083   | -42  | 35,9  | 271,4  | -36,6   | -178,1  | -0,8   |
| 1100                    | 1150                             | 1125                                    | 16,6                   | 128,4                  | 1752                   | -2379   | -627   | 29,0  | 300,4  | -39,4   | -217,5  | -10,4  |
| 1050                    | 1100                             | 1075                                    | 12,4                   | 140,8                  | 1454                   | -2792   | -1338  | 18,1  | 318,5  | -34,7   | -252,2  | -16,6  |
| 1000                    | 1050                             | 1025                                    | 9,4                    | 150,3                  | 1270                   | -3204   | -1933  | 12,0  | 330,5  | -30,2   | -282,4  | -18,2  |
| 950                     | 1000                             | 975                                     | 8,6                    | 158,9                  | 1131                   | -3545   | -2414  | 9,8   | 340,2  | -30,6   | -313,1  | -20,8  |
| 900                     | 950                              | 925                                     | 6,7                    | 165,6                  | 976                    | -3821   | -2844  | 6,5   | 346,7  | -25,4   | -338,5  | -18,9  |
| 850                     | 900                              | 875                                     | 4,2                    | 169,7                  | 806                    | -4089   | -3282  | 3,4   | 350,1  | -17,1   | -355,6  | -13,7  |
| 800                     | 850                              | 825                                     | 3,4                    | 173,2                  | 686                    | -4313   | -3627  | 2,4   | 352,5  | -14,8   | -370,4  | -12,5  |
| 750                     | 800                              | 775                                     | 2,9                    | 176,1                  | 616                    | -4458   | -3841  | 1,8   | 354,3  | -13,0   | -383,4  | -11,2  |
| 700                     | 750                              | 725                                     | 2,9                    | 179                    | 416                    | -4883   | -4467  | 1,2   | 355,5  | -14,3   | -397,7  | -13,1  |
| 650                     | 700                              | 675                                     | 3,2                    | 182,2                  | 223                    | -5349   | -5126  | 0,7   | 356,2  | -16,9   | -414,6  | -16,2  |
| 600                     | 650                              | 625                                     | 2,5                    | 184,7                  | 92                     | -5651   | -5558  | 0,2   | 356,4  | -14,1   | -428,8  | -13,9  |
| 550                     | 600                              | 575                                     | 1,8                    | 186,5                  | -14                    | -5836   | -5851  | 0,0   | 356,4  | -10,5   | -439,3  | -10,5  |
| 500                     | 550                              | 525                                     | 1,5                    | 188                    | -134                   | -6014   | -6149  | -0,2  | 356,2  | -9,1  | -448,3  | -9,3   |
| 450                     | 500                              | 475                                     | 1,1                    | 189                    | -335                   | -6327   | -6663  | -0,4  | 355,8  | -6,7  | -455,0  | -7,1   |
| 400                     | 450                              | 425                                     | 0,7                    | 189,8                  | -539                   | -6691   | -7230  | -0,4  | 355,4  | -4,8  | -459,8  | -5,2   |
| 350                     | 400                              | 375                                     | 0,7                    | 190,5                  | -787                   | -7120   | -7908  | -0,6  | 354,9  | -5,1  | -464,9  | -5,7   |
| 300                     | 350                              | 325                                     | 0,5                    | 191                    | -1005                  | -7509   | -8514  | -0,5  | 354,4  | -3,8  | -468,7  | -4,3   |
| 250                     | 300                              | 275                                     | 0,6                    | 191,6                  | -1226                  | -7860   | -9086  | -0,7  | 353,6  | -4,8  | -473,5  | -5,5   |
| 200                     | 250                              | 225                                     | 0,9                    | 192,4                  | -1571                  | -8246   | -9817  | -1,3  | 352,3  | -7,0  | -480,5  | -8,4   |
| 150                     | 200                              | 175                                     | 1,8                    | 194,2                  | -2020                  | -8671   | -10692   | -3,6  | 348,7  | -15,5   | -496,0  | -19,1  |
| 100                     | 150                              | 125                                     | 2,4                    | 196,6                  | -2529                  | -9140   | -11669   | -6,0  | 342,7  | -21,6   | -517,7  | -27,6  |
| 50                      | 100                              | 75                                      | 2,2                    | 198,8                  | -2972                  | -9559   | -12531   | -6,5  | 336,2  | -20,9   | -538,6  | -27,4  |
| 0                       | 50                               | 25                                      | 2,9                    | 201,7                  | -3518                  | -10086  | -13604   | -10,2   | 326,0  | -29,1   | -567,7  | -39,3  |
|                         |                                  |   |                        |                        |                        |   |  |   |  |   |   | -241,7 |

## Breiðamerkurjökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\Sigma \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|-------------------------|----------------------------------|---|------------------------|------------------------|------------------------|---|--|---|--|---|---|
| 1900                    | 1950                             | 1925                                    | 0                      | 0                      | 5158                   | -242  | 4916   | 0,2   | 0,2  | 0,0   | 0,0   |
| 1850                    | 1900                             | 1875                                    | 0,4                    | 0,4                    | 5166                   | -129  | 5036   | 1,9   | 2,2  | 0,0   | -0,1  |
| 1800                    | 1850                             | 1825                                    | 0,5                    | 0,9                    | 5066                   | -38   | 5027   | 2,4   | 4,6  | 0,0   | -0,1  |
| 1750                    | 1800                             | 1775                                    | 0,9                    | 1,8                    | 4769                   | -60   | 4709   | 4,3   | 9,0  | -0,1  | -0,1  |
| 1700                    | 1750                             | 1725                                    | 2,6                    | 4,4                    | 3406                   | -360  | 3046   | 8,8   | 17,7   | -0,9  | -1,1  |
| 1650                    | 1700                             | 1675                                    | 6                      | 10,4                   | 2555                   | -550  | 2004   | 15,3  | 33,0   | -3,3  | -4,4  |
| 1600                    | 1650                             | 1625                                    | 18                     | 28,3                   | 2179                   | -615  | 1564   | 39,1  | 72,2   | -11,0   | -15,4   |
| 1550                    | 1600                             | 1575                                    | 26,4                   | 54,7                   | 2105                   | -698  | 1406   | 55,5  | 127,7  | -18,4   | -33,8   |
| 1500                    | 1550                             | 1525                                    | 31,8                   | 86,5                   | 2138                   | -826  | 1312   | 68,1  | 195,7  | -26,3   | -60,1   |
| 1450                    | 1500                             | 1475                                    | 46,6                   | 133,1                  | 2183                   | -934  | 1248   | 101,6   | 297,4  | -43,5   | -103,6  |
| 1400                    | 1450                             | 1425                                    | 57,5                   | 190,6                  | 2153                   | -1045   | 1107   | 123,8   | 421,2  | -60,1   | -163,7  |
| 1350                    | 1400                             | 1375                                    | 88,2                   | 278,8                  | 2111                   | -1225   | 886  | 186,4   | 607,6  | -108,1  | -271,9  |
| 1300                    | 1350                             | 1325                                    | 94,3                   | 373,1                  | 2058                   | -1438   | 620  | 194,1   | 801,6  | -135,6  | -407,4  |
| 1250                    | 1300                             | 1275                                    | 56,9                   | 430                    | 1968                   | -1571   | 396  | 111,9   | 913,6  | -89,4   | -496,8  |
| 1200                    | 1250                             | 1225                                    | 38,2                   | 468,2                  | 1855                   | -1741   | 113  | 71,0  | 984,6  | -66,6   | -563,4  |
| 1150                    | 1200                             | 1175                                    | 30,7                   | 498,9                  | 1716                   | -1978   | -261   | 52,7  | 1037,3   | -60,8   | -624,2  |
| 1100                    | 1150                             | 1125                                    | 25,1                   | 524,1                  | 1573                   | -2287   | -713   | 39,5  | 1076,8   | -57,5   | -681,7  |
| 1050                    | 1100                             | 1075                                    | 21,6                   | 545,7                  | 1448                   | -2574   | -1126  | 31,4  | 1108,2   | -55,7   | -737,4  |
| 1000                    | 1050                             | 1025                                    | 18,7                   | 564,4                  | 1350                   | -2842   | -1491  | 25,3  | 1133,5   | -53,2   | -790,6  |
| 950                     | 1000                             | 975                                     | 20,3                   | 584,7                  | 1256                   | -3225   | -1969  | 25,5  | 1158,9   | -65,4   | -856,0  |
| 900                     | 950                              | 925                                     | 21,9                   | 606,6                  | 1107                   | -3526   | -2419  | 24,2  | 1183,2   | -77,2   | -933,2  |
| 850                     | 900                              | 875                                     | 17,9                   | 624,5                  | 886                    | -3864   | -2978  | 15,9  | 1199,1   | -69,3   | -1002,6   |
| 800                     | 850                              | 825                                     | 20,8                   | 645,4                  | 703                    | -4202   | -3499  | 14,7  | 1213,7   | -87,6   | -1090,1   |
| 750                     | 800                              | 775                                     | 21,8                   | 667,2                  | 535                    | -4559   | -4024  | 11,7  | 1225,4   | -99,4   | -1189,5   |
| 700                     | 750                              | 725                                     | 16,7                   | 683,8                  | 385                    | -4893   | -4508  | 6,4   | 1231,8   | -81,5   | -1271,0   |
| 650                     | 700                              | 675                                     | 22,4                   | 706,3                  | 264                    | -5215   | -4950  | 5,9   | 1237,8   | -117,0  | -1388,0   |
| 600                     | 650                              | 625                                     | 25,4                   | 731,6                  | 141                    | -5510   | -5368  | 3,6   | 1241,4   | -139,8  | -1527,8   |
| 550                     | 600                              | 575                                     | 22,5                   | 754,2                  | -18                    | -5823   | -5841  | -0,4  | 1240,9   | -131,3  | -1659,1   |
| 500                     | 550                              | 525                                     | 21,2                   | 775,4                  | -192                   | -6092   | -6285  | -4,1  | 1236,8   | -129,2  | -1788,3   |
| 450                     | 500                              | 475                                     | 12,1                   | 787,5                  | -369                   | -6418   | -6788  | -4,5  | 1232,4   | -77,8   | -1866,1   |
| 400                     | 450                              | 425                                     | 13,3                   | 800,8                  | -526                   | -6701   | -7228  | -7,0  | 1225,4   | -89,0   | -1955,1   |
| 350                     | 400                              | 375                                     | 14,7                   | 815,5                  | -708                   | -7033   | -7741  | -10,4   | 1215,0   | -103,3  | -2058,4   |
| 300                     | 350                              | 325                                     | 11,6                   | 827,1                  | -925                   | -7413   | -8339  | -10,8   | 1204,2   | -86,2   | -2144,6   |
| 250                     | 300                              | 275                                     | 9,8                    | 836,9                  | -1218                  | -7780   | -8999  | -12,0   | 1192,2   | -76,5   | -2221,1   |
| 200                     | 250                              | 225                                     | 9,9                    | 846,8                  | -1673                  | -8206   | -9879  | -16,6   | 1175,6   | -81,4   | -2302,5   |
| 150                     | 200                              | 175                                     | 8,9                    | 855,7                  | -2167                  | -8619   | -10786   | -19,2   | 1156,4   | -76,4   | -2378,9   |
| 100                     | 150                              | 125                                     | 9,1                    | 864,8                  | -2600                  | -8978   | -11578   | -23,6   | 1132,8   | -81,6   | -2460,5   |
| 50                      | 100                              | 75                                      | 7                      | 871,8                  | -2936                  | -9387   | -12324   | -20,6   | 1112,1   | -66,0   | -2526,5   |
| 0                       | 50                               | 25                                      | 3                      | 874,8                  | -3130                  | -10168  | -13299   | -9,3  | 1102,9   | -30,1   | -2556,6   |
|                         |                                  |   |                        |                        |                        |   |  |   |  |   | -39,4   |
|                         |                                  |   |                        |                        |                        |   |  |   |  |   | -1453,8   |

## Síðujökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\Sigma \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |        |        |
|-------------------------|----------------------------------|---|------------------------|------------------------|------------------------|---|--|---|--|---|---|--------|--------|
| 1700                    | 1750                             | 1725                                    | 0,9                    | 0,9                    | 2356                   | -310  | 2046   | 2,2   | 2,2  | -0,3  | -0,3  | 1,9    | 1,9    |
| 1650                    | 1700                             | 1675                                    | 5,9                    | 6,9                    | 2377                   | -398  | 1979   | 14,1  | 16,3   | -2,4  | -2,7  | 11,8   | 13,7   |
| 1600                    | 1650                             | 1625                                    | 11,3                   | 18,1                   | 2215                   | -514  | 1700   | 24,9  | 41,2   | -5,8  | -8,5  | 19,1   | 32,8   |
| 1550                    | 1600                             | 1575                                    | 11,7                   | 29,8                   | 2220                   | -566  | 1654   | 25,9  | 67,1   | -6,6  | -15,1   | 19,3   | 52,1   |
| 1500                    | 1550                             | 1525                                    | 21,4                   | 51,2                   | 2196                   | -704  | 1491   | 47,1  | 114,2  | -15,1   | -30,2   | 32,0   | 84,1   |
| 1450                    | 1500                             | 1475                                    | 38                     | 89,2                   | 2129                   | -969  | 1159   | 80,9  | 195,1  | -36,9   | -67,0   | 44,1   | 128,1  |
| 1400                    | 1450                             | 1425                                    | 24,8                   | 114                    | 2037                   | -1166   | 870  | 50,5  | 245,6  | -28,9   | -95,9   | 21,6   | 149,7  |
| 1350                    | 1400                             | 1375                                    | 21                     | 135                    | 1928                   | -1468   | 460  | 40,5  | 286,1  | -30,8   | -126,7  | 9,7    | 159,3  |
| 1300                    | 1350                             | 1325                                    | 17,1                   | 152                    | 1833                   | -1826   | 6  | 31,3  | 317,4  | -31,2   | -157,9  | 0,1    | 159,5  |
| 1250                    | 1300                             | 1275                                    | 15,1                   | 167,2                  | 1760                   | -2176   | -416   | 26,6  | 344,0  | -32,9   | -190,8  | -6,3   | 153,2  |
| 1200                    | 1250                             | 1225                                    | 21,1                   | 188,3                  | 1687                   | -2527   | -840   | 35,6  | 379,6  | -53,4   | -244,2  | -17,7  | 135,4  |
| 1150                    | 1200                             | 1175                                    | 17,5                   | 205,8                  | 1552                   | -2953   | -1401  | 27,2  | 406,9  | -51,8   | -296,0  | -24,6  | 110,8  |
| 1100                    | 1150                             | 1125                                    | 16,6                   | 222,5                  | 1458                   | -3257   | -1798  | 24,3  | 431,1  | -54,2   | -350,2  | -29,9  | 80,9   |
| 1050                    | 1100                             | 1075                                    | 15                     | 237,5                  | 1379                   | -3594   | -2215  | 20,8  | 451,9  | -54,1   | -404,3  | -33,3  | 47,6   |
| 1000                    | 1050                             | 1025                                    | 18,5                   | 256                    | 1288                   | -3991   | -2703  | 23,8  | 475,7  | -73,7   | -478,0  | -49,9  | -2,3   |
| 950                     | 1000                             | 975                                     | 19,4                   | 275,4                  | 1159                   | -4364   | -3205  | 22,5  | 498,1  | -84,5   | -562,5  | -62,1  | -64,4  |
| 900                     | 950                              | 925                                     | 19,6                   | 294,9                  | 963                    | -4684   | -3720  | 18,8  | 517,0  | -91,6   | -654,1  | -72,8  | -137,2 |
| 850                     | 900                              | 875                                     | 18,8                   | 313,7                  | 725                    | -5018   | -4293  | 13,6  | 530,6  | -94,2   | -748,4  | -80,6  | -217,8 |
| 800                     | 850                              | 825                                     | 17,7                   | 331,4                  | 531                    | -5366   | -4835  | 9,4   | 540,0  | -94,8   | -843,2  | -85,5  | -303,2 |
| 750                     | 800                              | 775                                     | 20,1                   | 351,5                  | 361                    | -5688   | -5327  | 7,3   | 547,2  | -114,4  | -957,6  | -107,1 | -410,4 |
| 700                     | 750                              | 725                                     | 20                     | 371,5                  | 221                    | -5977   | -5755  | 4,4   | 551,7  | -119,9  | -1077,5   | -115,4 | -525,8 |
| 650                     | 700                              | 675                                     | 19,9                   | 391,4                  | 100                    | -6341   | -6240  | 2,0   | 553,7  | -126,3  | -1203,7   | -124,2 | -650,0 |
| 600                     | 650                              | 625                                     | 8,9                    | 400,3                  | 13                     | -6689   | -6676  | 0,1   | 553,8  | -59,6   | -1263,3   | -59,4  | -709,5 |
| 550                     | 600                              | 575                                     | 0                      | 400,4                  | -39                    | -6915   | -6954  | 0,0   | 553,8  | -0,3  | -1263,6   | -0,3   | -709,8 |

## Skaftárjökull

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\Sigma \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |       |        |
|-------------------------|----------------------------------|---|------------------------|------------------------|------------------------|---|--|---|--|---|---|-------|--------|
| 1400                    | 1450                             | 1425                                    | 0                      | 0                      | 1871                   | -1289   | 581  | 0   | 0  | -0  | -0  | 0     | 0      |
| 1350                    | 1400                             | 1375                                    | 2,5                    | 2,5                    | 1798                   | -1510   | 287  | 4,4   | 4,4  | -3,7  | -3,7  | 0,7   | 0,7    |
| 1300                    | 1350                             | 1325                                    | 5,2                    | 7,7                    | 1720                   | -1812   | -91  | 9   | 13,4   | -9,5  | -13,2   | -0,5  | 0,2    |
| 1250                    | 1300                             | 1275                                    | 4                      | 11,7                   | 1647                   | -2204   | -556   | 6,5   | 20   | -8,7  | -21,9   | -2,2  | -2     |
| 1200                    | 1250                             | 1225                                    | 6,3                    | 17,9                   | 1561                   | -2631   | -1069  | 9,8   | 29,8   | -16,5   | -38,5   | -6,7  | -8,7   |
| 1150                    | 1200                             | 1175                                    | 7,4                    | 25,3                   | 1468                   | -2978   | -1510  | 10,8  | 40,6   | -21,9   | -60,4   | -11,1 | -19,8  |
| 1100                    | 1150                             | 1125                                    | 10,6                   | 35,9                   | 1344                   | -3293   | -1948  | 14,3  | 54,9   | -35   | -95,4   | -20,7 | -40,5  |
| 1050                    | 1100                             | 1075                                    | 11,7                   | 47,6                   | 1215                   | -3649   | -2434  | 14,2  | 69,1   | -42,7   | -138,1  | -28,5 | -69    |
| 1000                    | 1050                             | 1025                                    | 12,7                   | 60,4                   | 1051                   | -4037   | -2985  | 13,4  | 82,5   | -51,4   | -189,5  | -38   | -107   |
| 950                     | 1000                             | 975                                     | 8,8                    | 69,2                   | 856                    | -4450   | -3594  | 7,6   | 90   | -39,3   | -228,8  | -31,7 | -138,7 |
| 900                     | 950                              | 925                                     | 5,8                    | 75                     | 712                    | -4776   | -4064  | 4,1   | 94,2   | -27,7   | -256,5  | -23,5 | -162,3 |
| 850                     | 900                              | 875                                     | 4,7                    | 79,7                   | 558                    | -5074   | -4516  | 2,6   | 96,8   | -23,9   | -280,4  | -21,3 | -183,6 |
| 800                     | 850                              | 825                                     | 4,8                    | 84,5                   | 413                    | -5373   | -4959  | 2   | 98,8   | -25,7   | -306,1  | -23,7 | -207,3 |
| 750                     | 800                              | 775                                     | 4,5                    | 88,9                   | 289                    | -5657   | -5367  | 1,3   | 100,1  | -25,3   | -331,4  | -24   | -231,3 |
| 700                     | 750                              | 725                                     | 3,9                    | 92,9                   | 155                    | -5899   | -5743  | 0,6   | 100,7  | -23,1   | -354,4  | -22,5 | -253,8 |
| 650                     | 700                              | 675                                     | 2,8                    | 95,7                   | 21                     | -6173   | -6152  | 0,1   | 100,7  | -17,3   | -371,7  | -17,2 | -271   |
| 600                     | 650                              | 625                                     | 0,5                    | 96,2                   | 10                     | -6342   | -6332  | 0   | 100,8  | -3,3  | -375  | -3,3  | -274,2 |

### Vestari Skaftárketill

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |      |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|------|
| 1900                    | 1950                             | 1925                                  | 0,5                    | 0,5                    | 2003                   | -165  | 1837   | 1,1   | 1,1  | -0,1  | -0,1  | 1,0  |
| 1850                    | 1900                             | 1875                                  | 0,7                    | 1,2                    | 1957                   | -204  | 1753   | 1,3   | 2,3  | -0,1  | -0,2  | 1,1  |
| 1800                    | 1850                             | 1825                                  | 0,8                    | 2                      | 1893                   | -255  | 1637   | 1,5   | 3,8  | -0,2  | -0,4  | 1,3  |
| 1750                    | 1800                             | 1775                                  | 2,5                    | 4,4                    | 1775                   | -376  | 1399   | 4,4   | 8,2  | -0,9  | -1,3  | 3,4  |
| 1700                    | 1750                             | 1725                                  | 5,4                    | 9,9                    | 1699                   | -452  | 1247   | 9,2   | 17,4   | -2,5  | -3,8  | 6,8  |
| 1650                    | 1700                             | 1675                                  | 6,5                    | 16,3                   | 1652                   | -526  | 1126   | 10,7  | 28,1   | -3,4  | -7,2  | 7,3  |
| 1600                    | 1650                             | 1625                                  | 7,3                    | 23,6                   | 1632                   | -604  | 1027   | 11,9  | 40,0   | -4,4  | -11,6   | 7,5  |
| 1550                    | 1600                             | 1575                                  | 5                      | 28,6                   | 1587                   | -690  | 896  | 7,9   | 47,9   | -3,4  | -15,0   | 4,5  |
| 1500                    | 1550                             | 1525                                  | 2,7                    | 31,2                   | 1550                   | -746  | 804  | 4,1   | 52,0   | -2,0  | -17,0   | 2,1  |
|                         |                                  |                                       |                        |                        |                        |   |  |   |  |   |   | 35,0 |

### Eystri Skaftárketill

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |      |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|------|
| 1750                    | 1800                             | 1775                                  | 1,1                    | 1,1                    | 1742                   | -427  | 1315   | 1,9   | 1,9  | -0,5  | -0,5  | 1,5  |
| 1700                    | 1750                             | 1725                                  | 10                     | 11,1                   | 1734                   | -471  | 1262   | 17,3  | 19,2   | -4,7  | -5,2  | 12,6 |
| 1650                    | 1700                             | 1675                                  | 15,5                   | 26,6                   | 1798                   | -510  | 1287   | 27,8  | 47,1   | -7,9  | -13,1   | 19,9 |
| 1600                    | 1650                             | 1625                                  | 9,2                    | 35,8                   | 1783                   | -548  | 1235   | 16,4  | 63,5   | -5,1  | -18,1   | 11,4 |
| 1550                    | 1600                             | 1575                                  | 4,2                    | 39,9                   | 1773                   | -568  | 1205   | 7,4   | 70,9   | -2,4  | -20,5   | 5,0  |
|                         |                                  |                                       |                        |                        |                        |   |  |   |  |   |   | 50,4 |

### Gjálp

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |        |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|--------|
| 1900                    | 1950                             | 1925                                  | 0,4                    | 0,4                    | 2031                   | -158  | 1873   | 0,7   | 0,700  | -0,100  | -0,100  | 0,700  |
| 1850                    | 1900                             | 1875                                  | 0,8                    | 1,1                    | 1961                   | -210  | 1750   | 1,5   | 2,200  | -0,200  | -0,200  | 1,300  |
| 1800                    | 1850                             | 1825                                  | 1,2                    | 2,3                    | 1871                   | -279  | 1592   | 2,2   | 4,400  | -0,300  | -0,500  | 1,900  |
| 1750                    | 1800                             | 1775                                  | 5,5                    | 7,8                    | 1753                   | -431  | 1322   | 9,7   | 14,100   | -2,400  | -2,900  | 7,300  |
| 1700                    | 1750                             | 1725                                  | 23,7                   | 31,5                   | 1806                   | -474  | 1331   | 42,9  | 57,000   | -11,300   | -14,200   | 31,600 |
| 1650                    | 1700                             | 1675                                  | 7,8                    | 39,4                   | 1884                   | -489  | 1394   | 14,8  | 71,800   | -3,800  | -18,000   | 10,900 |
|                         |                                  |                                       |                        |                        |                        |   |  |   |  |   |   | 53,700 |

### Grímsvötn

| Elevation<br>(m a.s.l.) | $\Delta S$<br>(km <sup>2</sup> ) | $\sum \Delta S$<br>(km <sup>2</sup> ) | b <sub>w</sub><br>(mm) | b <sub>s</sub><br>(mm) | b <sub>n</sub><br>(mm) | $\Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_w$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum \Delta B_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Delta B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\sum B_n$<br>(10 <sup>6</sup> m <sup>3</sup> ) |       |
|-------------------------|----------------------------------|---------------------------------------|------------------------|------------------------|------------------------|---|--|---|--|---|---|-------|
| 1700                    | 1750                             | 1725                                  | 1,3                    | 1,3                    | 1927                   | -512  | 1415   | 2,6   | 2,6  | -0,7  | -0,7  | 1,9   |
| 1650                    | 1700                             | 1675                                  | 40,7                   | 42,1                   | 1973                   | -588  | 1384   | 80,4  | 83,0   | -24,0   | -24,7   | 56,4  |
| 1600                    | 1650                             | 1625                                  | 30,7                   | 72,8                   | 1985                   | -682  | 1303   | 60,9  | 143,9  | -20,9   | -45,6   | 40,0  |
| 1550                    | 1600                             | 1575                                  | 19,6                   | 92,4                   | 2021                   | -820  | 1201   | 39,6  | 183,5  | -16,1   | -61,7   | 23,5  |
| 1500                    | 1550                             | 1525                                  | 16,3                   | 108,7                  | 2064                   | -1001   | 1063   | 33,7  | 217,2  | -16,3   | -78,0   | 17,3  |
| 1450                    | 1500                             | 1475                                  | 9,5                    | 118,2                  | 2131                   | -1312   | 818  | 20,2  | 237,4  | -12,5   | -90,5   | 7,8   |
| 1400                    | 1450                             | 1425                                  | 13,7                   | 131,9                  | 2250                   | -1709   | 541  | 30,9  | 268,3  | -23,5   | -113,9  | 7,4   |
| 1350                    | 1400                             | 1375                                  | 1,2                    | 133,1                  | 2016                   | -1683   | 333  | 2,5   | 270,8  | -2,1  | -116,0  | 0,4   |
|                         |                                  |                                       |                        |                        |                        |   |  |   |  |   |   | 154,8 |

## Appendix C: Coordinates of the velocity measurement stakes in 2023.

Position of the velocity measurement stakes determined by GPS sub-metre differential (I), fast static (FS) and kinematic (K). (Accuracy of horizontal position 0.5 – 1.0 m, and vertical accuracy 1-2 m for DGPS, about 1cm for fast static, and 3 cm for kinematic).

The station Hofn in Höfn í Hornafirði is used as a stationary reference for all measurements, ÍSN93 datum,  $h_l$  is elevation above ellipsoid, dL antenna height, N estimated difference between ellipsoid and sea-level, H elevation in metres above sea level ( $H = h_l + N + dL$ ). X and Y are ÍSN93 Lambert conformal conic projected coordinates. M is a quality marker.

| Site     | Calender |      |    |     |      |             |             |                    |           |                   |          | X         | Y         | M |
|----------|----------|------|----|-----|------|-------------|-------------|--------------------|-----------|-------------------|----------|-----------|-----------|---|
|          | time     | Date | #  | Day | Year | Latitude    | Longitude   | $h_l$<br>(m a. e.) | dL<br>(m) | N<br>(m a. s. l.) | H<br>(m) |           |           |   |
| B07-23   | 11,72    | 4    | 5  | 124 | 2023 | 64 25,79652 | 16 17,48091 | 1425,86            | 0,00      | -67,05            | 1358,81  | 630454,15 | 439244,78 | K |
| B07-23   | 14,66    | 27   | 10 | 300 | 2023 | 64 25,79558 | 16 17,47997 | 1422,01            | 0,00      | -67,05            | 1354,96  | 630454,97 | 439243,07 | K |
| B09-23   | 12,52    | 5    | 5  | 125 | 2023 | 64 44,48331 | 16 6,18820  | 792,97             | 0,00      | -66,68            | 726,28   | 637922,21 | 474330,23 | K |
| B09-23   | 18,34    | 24   | 10 | 297 | 2023 | 64 44,48316 | 16 6,18824  | 785,91             | 0,00      | -66,68            | 719,23   | 637922,20 | 474329,95 | K |
| B10-23   | 12,87    | 5    | 5  | 125 | 2023 | 64 43,68247 | 16 6,70405  | 823,90             | 0,00      | -66,71            | 757,19   | 637581,12 | 472825,09 | K |
| B10-23   | 19,00    | 24   | 10 | 297 | 2023 | 64 43,68247 | 16 6,70405  | 817,50             | 0,00      | -66,71            | 750,79   | 637581,12 | 472825,09 | K |
| B11-23   | 10,61    | 5    | 5  | 125 | 2023 | 64 40,93875 | 16 10,48385 | 1011,44            | 0,00      | -66,81            | 944,63   | 634810,08 | 467596,73 | K |
| B11-23   | 19,25    | 24   | 10 | 297 | 2023 | 64 40,94359 | 16 10,47997 | 1006,27            | 0,00      | -66,81            | 939,46   | 634812,77 | 467605,85 | K |
| B12-23   | 10,13    | 5    | 5  | 125 | 2023 | 64 38,26171 | 16 14,14876 | 1144,89            | 0,00      | -66,90            | 1077,99  | 632114,81 | 462498,71 | K |
| B12-23   | 19,63    | 24   | 10 | 297 | 2023 | 64 38,26979 | 16 14,14172 | 1140,78            | 0,00      | -66,90            | 1073,88  | 632119,76 | 462513,95 | K |
| B13-23   | 19,71    | 4    | 5  | 124 | 2023 | 64 34,57784 | 16 19,63675 | 1289,43            | 0,00      | -67,01            | 1222,42  | 628035,10 | 455472,21 | K |
| B13-23   | 17,43    | 26   | 10 | 299 | 2023 | 64 34,58619 | 16 19,62759 | 1285,61            | 0,00      | -67,01            | 1218,60  | 628041,75 | 455488,03 | K |
| B13ror15 | 17,75    | 4    | 5  | 124 | 2023 | 64 34,65271 | 16 19,57542 | 1286,54            | 0,00      | -67,01            | 1219,53  | 628078,16 | 455613,27 | K |
| B13ror15 | 16,74    | 26   | 10 | 299 | 2023 | 64 34,66130 | 16 19,56503 | 1285,09            | 0,00      | -67,01            | 1218,08  | 628085,77 | 455629,55 | K |
| B14-23   | 16,36    | 4    | 5  | 124 | 2023 | 64 31,65039 | 16 24,77175 | 1391,49            | 0,00      | -67,11            | 1324,38  | 624160,14 | 449867,02 | K |
| B14-23   | 18,65    | 23   | 10 | 296 | 2023 | 64 31,65696 | 16 24,75936 | 1389,30            | 0,00      | -67,11            | 1322,20  | 624169,55 | 449879,61 | K |
| B15-23   | 15,49    | 4    | 5  | 124 | 2023 | 64 28,51272 | 16 30,03180 | 1472,91            | 0,00      | -67,21            | 1405,70  | 620185,53 | 443872,53 | K |
| B15-23   | 20,66    | 24   | 10 | 297 | 2023 | 64 28,51716 | 16 30,02018 | 1469,11            | 0,00      | -67,21            | 1401,90  | 620194,51 | 443881,14 | K |
| B16-23   | 15,49    | 8    | 5  | 128 | 2023 | 64 24,12250 | 16 40,92038 | 1596,01            | 0,00      | -67,33            | 1528,68  | 611762,44 | 435388,49 | K |
| B16-23   | 19,63    | 23   | 10 | 296 | 2023 | 64 24,12277 | 16 40,91989 | 1594,65            | -1,08     | -67,33            | 1526,24  | 611762,81 | 435389,00 | K |
| B17-23   | 17,15    | 4    | 5  | 124 | 2023 | 64 36,73298 | 16 28,79729 | 1284,46            | 0,00      | -67,12            | 1217,34  | 620565,67 | 459172,88 | K |
| B17-23   | 18,85    | 23   | 10 | 296 | 2023 | 64 36,74267 | 16 28,79082 | 1280,36            | 0,00      | -67,12            | 1213,24  | 620570,11 | 459191,07 | K |
| B18-23   | 21,19    | 3    | 5  | 123 | 2023 | 64 31,57695 | 16 0,12051  | 1383,79            | 0,00      | -66,92            | 1316,87  | 643870,26 | 450601,67 | K |
| B18-23   | 16,02    | 23   | 10 | 296 | 2023 | 64 31,58259 | 16 0,12373  | 1379,62            | 0,00      | -66,92            | 1312,70  | 643867,20 | 450612,02 | K |
| B19-23   | 13,20    | 3    | 5  | 123 | 2023 | 64 27,97835 | 15 56,00763 | 1507,47            | 0,00      | -66,89            | 1440,58  | 647481,46 | 444081,14 | K |
| B19-23   | 15,54    | 23   | 10 | 296 | 2023 | 64 27,97867 | 15 56,00814 | 1502,79            | 0,00      | -66,89            | 1435,90  | 647481,02 | 444081,72 | K |
| Bb0-23   | 10,73    | 4    | 5  | 124 | 2023 | 64 22,70700 | 16 5,04118  | 1585,41            | 0,00      | -66,85            | 1518,56  | 640697,38 | 433954,77 | K |
| Bb0-23   | 14,20    | 23   | 10 | 296 | 2023 | 64 22,70683 | 16 5,04228  | 1580,97            | 0,00      | -66,85            | 1514,12  | 640696,51 | 433954,41 | K |
| Barc-23  | 14,11    | 31   | 5  | 151 | 2023 | 64 38,40650 | 17 26,76249 | 1974,21            | -1,65     | -67,87            | 1904,69  | 574281,29 | 460791,90 | K |
| Barc-23  | 15,64    | 24   | 10 | 297 | 2023 | 64 38,40626 | 17 26,75635 | 1971,88            | -1,35     | -67,87            | 1902,66  | 574286,20 | 460791,56 | K |
| Bb02-23  | 14,39    | 31   | 5  | 151 | 2023 | 64 38,42457 | 17 26,76060 | 1974,14            | -1,65     | -67,87            | 1904,62  | 574281,97 | 460825,50 | K |
| Bb02-23  | 15,90    | 12   | 9  | 255 | 2023 | 64 38,42440 | 17 26,75629 | 1971,34            | -1,00     | -67,87            | 1902,47  | 574285,41 | 460825,26 | K |
| Bb02-23  | 15,23    | 24   | 10 | 297 | 2023 | 64 38,42435 | 17 26,75470 | 1973,03            | -2,70     | -67,87            | 1902,46  | 574286,68 | 460825,20 | K |
| Bb08-23  | 14,71    | 31   | 5  | 151 | 2023 | 64 39,02326 | 17 23,21833 | 1939,34            | -1,65     | -67,84            | 1869,84  | 577075,05 | 462008,18 | K |
| Bb08-23  | 16,63    | 12   | 9  | 255 | 2023 | 64 39,02357 | 17 23,21351 | 1936,61            | -1,00     | -67,87            | 1867,74  | 577078,87 | 462008,86 | K |
| Bb08-23  | 16,37    | 24   | 10 | 297 | 2023 | 64 39,02348 | 17 23,21185 | 1937,34            | -2,40     | -67,87            | 1867,07  | 577080,20 | 462008,73 | K |
| Bb09-23  | 15,07    | 31   | 5  | 151 | 2023 | 64 39,66595 | 17 28,01689 | 1983,95            | -1,65     | -67,87            | 1914,43  | 573225,38 | 463106,86 | K |
| Bb09-23  | 17,54    | 24   | 10 | 297 | 2023 | 64 39,66574 | 17 28,01388 | 1981,79            | -2,20     | -67,87            | 1911,72  | 573227,79 | 463106,54 | K |
| Bb05-23  | 15,41    | 31   | 5  | 151 | 2023 | 64 36,59093 | 17 30,78860 | 1982,95            | -1,65     | -67,87            | 1913,43  | 571153,67 | 457342,36 | K |
| Bb05-23  | 18,88    | 24   | 10 | 297 | 2023 | 64 36,58916 | 17 30,78989 | 1980,74            | -2,25     | -67,87            | 1910,62  | 571152,72 | 457339,04 | K |
| Bb07-23  | 15,78    | 31   | 5  | 151 | 2023 | 64 36,56588 | 17 25,04511 | 1951,47            | -1,65     | -67,86            | 1881,96  | 575734,83 | 457407,03 | K |
| Bb10-23  | 16,11    | 31   | 5  | 151 | 2023 | 64 36,32061 | 17 15,64637 | 1685,34            | -1,65     | -67,72            | 1615,96  | 583241,88 | 457148,45 | K |
| Bb10-23  | 19,89    | 24   | 10 | 297 | 2023 | 64 36,31825 | 17 15,63749 | 1683,01            | -2,05     | -67,72            | 1613,24  | 583249,08 | 457144,27 | K |
| Bb10-23  | 15,35    | 12   | 9  | 255 | 2023 | 64 36,32077 | 17 15,63689 | 1681,85            | -0,85     | -67,72            | 1613,27  | 583249,43 | 457148,96 | K |
| Bor-23   | 14,12    | 2    | 6  | 153 | 2023 | 64 24,93782 | 17 20,15447 | 1480,56            | -1,26     | -67,70            | 1411,60  | 580203,31 | 435909,79 | K |
| Bor-23   | 12,83    | 27   | 10 | 300 | 2023 | 64 24,93314 | 17 20,15922 | 1496,23            | 0,00      | -67,70            | 1428,53  | 580199,73 | 435901,00 | K |

|          |       |    |    |     |      |    |          |    |          |         |       |        |         |           |           |   |
|----------|-------|----|----|-----|------|----|----------|----|----------|---------|-------|--------|---------|-----------|-----------|---|
| Br1-23   | 12,35 | 22 | 6  | 173 | 2023 | 64 | 5,95858  | 16 | 19,81973 | 137,00  | -1,06 | -65,90 | 70,04   | 630134,01 | 402338,50 | K |
| Br1-23   | 17,97 | 22 | 10 | 295 | 2023 | 64 | 5,96327  | 16 | 19,82096 | 131,57  | -1,55 | -65,90 | 64,12   | 630132,65 | 402347,16 | K |
| Br2-22   | 19,30 | 21 | 6  | 172 | 2023 | 64 | 6,35483  | 16 | 22,52633 | 217,27  | -1,06 | -66,03 | 150,18  | 627905,83 | 402982,04 | K |
| Br2-23   | 19,80 | 21 | 6  | 172 | 2023 | 64 | 6,35398  | 16 | 22,52332 | 217,14  | -1,06 | -66,03 | 150,04  | 627908,33 | 402980,56 | K |
| Br2-23   | 14,54 | 22 | 10 | 295 | 2023 | 64 | 6,35358  | 16 | 22,52295 | 211,42  | -1,55 | -66,03 | 143,84  | 627908,67 | 402979,83 | K |
| Br3-22   | 17,00 | 21 | 6  | 172 | 2023 | 64 | 8,41263  | 16 | 23,96994 | 415,63  | -1,06 | -66,26 | 348,31  | 626576,70 | 406753,83 | K |
| Br3-23   | 17,50 | 21 | 6  | 172 | 2023 | 64 | 8,41308  | 16 | 23,97076 | 415,68  | -1,06 | -66,26 | 348,36  | 626576,00 | 406754,63 | K |
| Br3-23   | 15,56 | 22 | 10 | 295 | 2023 | 64 | 8,41016  | 16 | 23,96632 | 412,03  | -1,55 | -66,26 | 344,22  | 626579,82 | 406749,36 | K |
| Br7-23   | 14,30 | 4  | 5  | 124 | 2023 | 64 | 22,14259 | 16 | 16,93857 | 1312,10 | 0,00  | -67,01 | 1245,10 | 631180,98 | 432480,73 | K |
| Br7-23   | 16,17 | 23 | 10 | 296 | 2023 | 64 | 22,11530 | 16 | 16,93063 | 1308,74 | -1,98 | -67,01 | 1239,75 | 631189,55 | 432430,35 | K |
| Bru-23   | 19,77 | 3  | 5  | 123 | 2023 | 64 | 39,75323 | 15 | 56,53495 | 958,13  | 0,00  | -66,78 | 891,35  | 646001,32 | 465912,77 | K |
| Bru-23   | 17,26 | 23 | 10 | 296 | 2023 | 64 | 39,76363 | 15 | 56,53151 | 953,21  | 0,00  | -66,78 | 886,42  | 646003,12 | 465932,19 | K |
| Bud-23   | 19,86 | 3  | 5  | 123 | 2023 | 64 | 35,98984 | 15 | 59,88663 | 1205,05 | 0,00  | -66,88 | 1138,17 | 643667,99 | 458800,44 | K |
| Bud-23   | 16,86 | 23 | 10 | 296 | 2023 | 64 | 36,00147 | 15 | 59,88466 | 1200,24 | 0,00  | -66,88 | 1133,36 | 643668,53 | 458822,10 | K |
| D01-23   | 17,53 | 5  | 5  | 125 | 2023 | 64 | 47,86795 | 16 | 49,97493 | 906,50  | 0,00  | -67,05 | 839,45  | 602977,18 | 479223,49 | K |
| D05-23   | 16,86 | 5  | 5  | 125 | 2023 | 64 | 42,22496 | 16 | 54,68882 | 1274,11 | 0,00  | -67,35 | 1206,76 | 599591,58 | 468618,84 | K |
| D05-23   | 17,30 | 26 | 10 | 299 | 2023 | 64 | 42,24186 | 16 | 54,66462 | 1272,04 | -2,23 | -67,35 | 1202,46 | 599609,76 | 468650,85 | K |
| D07-23   | 17,89 | 5  | 5  | 125 | 2023 | 64 | 38,28941 | 16 | 59,25843 | 1446,36 | 0,00  | -67,50 | 1378,86 | 596193,84 | 461192,51 | K |
| D07-23   | 15,61 | 26 | 10 | 299 | 2023 | 64 | 38,30935 | 16 | 59,23880 | 1444,16 | -2,44 | -67,50 | 1374,22 | 596208,29 | 461230,03 | K |
| D08-23   | 18,59 | 5  | 5  | 125 | 2023 | 64 | 34,68189 | 17 | 1,51937  | 1556,43 | 0,00  | -67,56 | 1488,87 | 594602,50 | 454436,20 | K |
| D08-23   | 14,86 | 26 | 10 | 299 | 2023 | 64 | 34,69128 | 17 | 1,51695  | 1554,81 | -2,30 | -67,56 | 1484,95 | 594603,88 | 454453,71 | K |
| D09      | 14,86 | 26 | 10 | 299 | 2023 | 64 | 34,69128 | 17 | 1,51695  | 1554,81 | -2,30 | -67,56 | 1484,95 | 594603,88 | 454453,71 | K |
| D12-23   | 19,30 | 5  | 5  | 125 | 2023 | 64 | 28,97478 | 17 | 0,18444  | 1719,13 | 0,00  | -67,55 | 1651,58 | 596002,94 | 443871,20 | K |
| D12-23   | 11,19 | 24 | 10 | 297 | 2023 | 64 | 28,97532 | 17 | 0,18424  | 1716,10 | 0,00  | -67,55 | 1648,55 | 596003,06 | 443872,21 | K |
| E01-22   | 18,53 | 3  | 5  | 123 | 2023 | 64 | 40,65000 | 15 | 34,84254 | 818,43  | 0,00  | -66,72 | 751,72  | 663158,10 | 468460,83 | K |
| E01-23   | 18,53 | 3  | 5  | 123 | 2023 | 64 | 40,65000 | 15 | 34,84254 | 818,43  | 0,00  | -66,72 | 751,72  | 663158,10 | 468460,83 | K |
| E01-23   | 17,03 | 24 | 10 | 297 | 2023 | 64 | 40,66066 | 15 | 34,83391 | 813,37  | 0,00  | -66,72 | 746,66  | 663163,88 | 468480,98 | K |
| E02-23   | 18,19 | 3  | 5  | 123 | 2023 | 64 | 39,10820 | 15 | 35,99632 | 1016,88 | 0,00  | -66,79 | 950,10  | 662395,40 | 465550,82 | K |
| E02-23   | 16,69 | 24 | 10 | 297 | 2023 | 64 | 39,12654 | 15 | 35,98950 | 1011,25 | 0,00  | -66,79 | 944,46  | 662398,99 | 465585,14 | K |
| E03-23   | 16,62 | 3  | 5  | 123 | 2023 | 64 | 36,60342 | 15 | 36,90205 | 1258,54 | 0,00  | -66,85 | 1191,69 | 661924,17 | 460864,92 | K |
| E03-23   | 14,83 | 24 | 10 | 297 | 2023 | 64 | 36,60921 | 15 | 36,90590 | 1252,32 | 0,00  | -66,85 | 1185,47 | 661920,53 | 460875,50 | K |
| E04-23   | 15,68 | 3  | 5  | 123 | 2023 | 64 | 34,93758 | 15 | 37,17934 | 1356,15 | 0,00  | -66,83 | 1289,32 | 661868,72 | 457762,39 | K |
| E04-23   | 13,96 | 24 | 10 | 297 | 2023 | 64 | 34,93827 | 15 | 37,17891 | 1351,03 | 0,00  | -66,83 | 1284,20 | 661869,00 | 457763,70 | K |
| E07-23   | 16,75 | 3  | 5  | 123 | 2023 | 64 | 38,41193 | 15 | 24,70313 | 1136,68 | 0,00  | -66,62 | 1070,07 | 671449,23 | 464756,11 | K |
| E07-23   | 15,71 | 24 | 10 | 297 | 2023 | 64 | 38,41668 | 15 | 24,69403 | 1130,47 | 0,00  | -66,62 | 1063,85 | 671455,97 | 464765,34 | K |
| E08-23   | 17,34 | 3  | 5  | 123 | 2023 | 64 | 39,72010 | 15 | 23,84813 | 1014,92 | 0,00  | -66,55 | 948,37  | 671990,94 | 467221,47 | K |
| E08-23   | 16,15 | 24 | 10 | 297 | 2023 | 64 | 39,72246 | 15 | 23,84788 | 1009,03 | 0,00  | -66,55 | 942,48  | 671990,88 | 467225,86 | K |
| FI01-23  | 12,85 | 3  | 5  | 123 | 2023 | 64 | 26,16388 | 15 | 55,63150 | 1415,44 | 0,00  | -66,82 | 1348,61 | 647946,52 | 440728,47 | K |
| FI01-23  | 14,88 | 23 | 10 | 296 | 2023 | 64 | 26,15738 | 15 | 55,61613 | 1409,86 | 0,00  | -66,82 | 1343,04 | 647959,43 | 440717,01 | K |
| G02-23   | 19,45 | 7  | 5  | 127 | 2023 | 64 | 26,84696 | 17 | 17,71810 | 1635,34 | 0,00  | -67,73 | 1567,61 | 582064,28 | 439507,82 | K |
| G02-23   | 11,15 | 24 | 10 | 297 | 2023 | 64 | 26,84273 | 17 | 17,72185 | 1634,66 | -1,77 | -67,73 | 1565,17 | 582061,48 | 439499,89 | K |
| G03-23   | 18,81 | 7  | 5  | 127 | 2023 | 64 | 28,44152 | 17 | 16,33470 | 1729,51 | 0,00  | -67,74 | 1661,78 | 583092,99 | 442499,54 | K |
| G03-23   | 11,49 | 24 | 10 | 297 | 2023 | 64 | 28,43946 | 17 | 16,33598 | 1728,79 | -2,10 | -67,74 | 1658,95 | 583092,07 | 442495,69 | K |
| G04-23   | 10,38 | 6  | 5  | 126 | 2023 | 64 | 30,02476 | 17 | 15,02675 | 1758,88 | 0,00  | -67,73 | 1691,15 | 584059,71 | 445468,90 | K |
| G04-23   | 12,45 | 24 | 10 | 297 | 2023 | 64 | 30,02508 | 17 | 15,02649 | 1758,43 | -2,35 | -67,72 | 1688,36 | 584059,90 | 445469,50 | K |
| Go1-23   | 11,25 | 6  | 5  | 126 | 2023 | 64 | 33,96748 | 17 | 24,92679 | 1829,56 | 0,00  | -67,84 | 1761,72 | 575950,18 | 452583,10 | K |
| Go1-23   | 13,10 | 24 | 10 | 297 | 2023 | 64 | 33,96599 | 17 | 24,92618 | 1829,43 | -2,40 | -67,86 | 1759,17 | 575950,74 | 452580,34 | K |
| Haab-23  | 10,95 | 6  | 5  | 126 | 2023 | 64 | 20,96631 | 17 | 24,11018 | 1798,70 | 0,00  | -67,54 | 1731,16 | 577213,02 | 428451,08 | K |
| Haab-23  | 10,80 | 25 | 10 | 298 | 2023 | 64 | 20,96676 | 17 | 24,10999 | 1795,33 | 0,00  | -67,54 | 1727,79 | 577213,15 | 428451,92 | K |
| Hof01-23 | 14,33 | 3  | 5  | 123 | 2023 | 64 | 32,34928 | 15 | 35,83025 | 1209,56 | 0,00  | -66,67 | 1142,89 | 663203,11 | 453018,07 | K |
| Hof01-23 | 14,25 | 24 | 10 | 297 | 2023 | 64 | 32,34295 | 15 | 35,83034 | 1204,55 | 0,00  | -66,67 | 1137,87 | 663203,68 | 453006,33 | K |
| K01-23   | 17,91 | 6  | 5  | 126 | 2023 | 64 | 35,17679 | 17 | 51,88038 | 1103,74 | 0,00  | -67,58 | 1036,16 | 554380,46 | 454366,41 | K |
| K01-23   | 15,47 | 25 | 10 | 298 | 2023 | 64 | 35,17796 | 17 | 51,88690 | 1098,61 | 0,00  | -67,58 | 1031,03 | 554375,22 | 454368,50 | K |
| K02-23   | 17,28 | 6  | 5  | 126 | 2023 | 64 | 34,80440 | 17 | 49,67746 | 1235,64 | 0,00  | -67,61 | 1168,02 | 556151,70 | 453706,72 | K |
| K02-23   | 15,00 | 25 | 10 | 298 | 2023 | 64 | 34,80774 | 17 | 49,69254 | 1230,80 | 0,00  | -67,61 | 1163,18 | 556139,55 | 453712,72 | K |
| K03-23   | 16,59 | 6  | 5  | 126 | 2023 | 64 | 34,23421 | 17 | 46,39332 | 1359,51 | 0,00  | -67,67 | 1291,84 | 558794,28 | 452697,27 | K |
| K03-23   | 14,11 | 25 | 10 | 298 | 2023 | 64 | 34,23727 | 17 | 46,41187 | 1355,43 | 0,00  | -67,67 | 1287,76 | 558779,36 | 452702,67 | K |
| K04-23   | 15,57 | 6  | 5  | 126 | 2023 | 64 | 33,21107 | 17 | 42,24640 | 1554,76 | 0,00  | -67,73 | 1487,02 | 562145,20 | 450862,78 | K |
| K04-23   | 13,20 | 25 | 10 | 298 | 2023 | 64 | 33,21487 | 17 | 42,27205 | 1550,11 | 0,00  | -67,73 | 1482,37 | 562124,56 | 450869,41 | K |
| K05-23   | 14,34 | 6  | 5  | 126 | 2023 | 64 | 33,44646 | 17 | 35,45784 | 1746,98 | 0,00  | -67,82 | 1679,16 | 567560,40 | 451416,09 | K |
| K05-23   | 11,91 | 25 | 10 | 298 | 2023 | 64 | 33,44370 | 17 | 35,47278 | 1743,61 | 0,00  | -67,82 | 1675,79 | 567548,58 | 451410,70 | K |
| K06-23   | 12,70 | 6  | 5  | 126 | 2023 | 64 | 38,35357 | 17 | 31,31262 | 2014,24 | 0,00  | -67,88 | 1946,37 | 570659,23 | 460606,65 | K |
| K06-23   | 17,81 | 24 | 10 | 297 | 2023 | 64 | 38,35319 | 17 | 31,31006 | 2014,66 | -2,55 | -67,88 | 1944,23 | 570661,29 | 460605,98 | K |
| K07-23   | 18,78 | 6  | 5  | 126 | 2023 | 64 | 29,11538 | 17 | 42,03620 | 1598,96 | 0,00  | -67,68 | 1531,2  |           |           |   |

|          |       |    |    |     |      |    |          |    |          |         |       |        |         |           |           |   |
|----------|-------|----|----|-----|------|----|----------|----|----------|---------|-------|--------|---------|-----------|-----------|---|
| Kverk-23 | 17,50 | 1  | 6  | 152 | 2023 | 64 | 38,65917 | 16 | 40,53513 | 1893,83 | -0,32 | -67,38 | 1826,13 | 611079,01 | 462390,70 | K |
| Kverk-23 | 12,21 | 24 | 10 | 297 | 2023 | 64 | 38,65941 | 16 | 40,53518 | 1889,29 | 0,00  | -67,38 | 1821,91 | 611078,96 | 462391,14 | K |
| S01-23   | 13,91 | 6  | 5  | 126 | 2023 | 64 | 7,01626  | 17 | 49,97436 | 765,42  | 0,00  | -66,84 | 698,58  | 556867,79 | 402080,46 | K |
| S02-23   | 13,19 | 6  | 5  | 126 | 2023 | 64 | 12,16517 | 17 | 48,98648 | 1066,44 | 0,00  | -67,05 | 999,40  | 557490,85 | 411660,57 | K |
| S02-23   | 12,45 | 25 | 10 | 298 | 2023 | 64 | 12,15120 | 17 | 48,99325 | 1060,88 | 0,00  | -67,04 | 993,84  | 557485,86 | 411634,51 | K |
| S04-23   | 12,49 | 6  | 5  | 126 | 2023 | 64 | 16,18145 | 17 | 48,19226 | 1223,58 | 0,00  | -67,21 | 1156,37 | 557992,49 | 419133,67 | K |
| S04-23   | 11,87 | 25 | 10 | 298 | 2023 | 64 | 16,16264 | 17 | 48,21241 | 1217,98 | 0,00  | -67,21 | 1150,78 | 557976,88 | 419098,43 | K |
| S05-23   | 11,66 | 6  | 5  | 126 | 2023 | 64 | 20,51465 | 17 | 33,99310 | 1518,88 | 0,00  | -67,51 | 1451,36 | 569275,50 | 427421,30 | K |
| S05-23   | 11,19 | 25 | 10 | 298 | 2023 | 64 | 20,51258 | 17 | 34,01067 | 1515,16 | 0,00  | -67,51 | 1447,64 | 569261,43 | 427417,14 | K |
| SkGPS-23 | 13,43 | 2  | 6  | 153 | 2023 | 64 | 15,47584 | 17 | 14,73302 | 1027,39 | -1,30 | -67,01 | 959,08  | 585044,98 | 418453,87 | K |
| Ske02-23 | 11,40 | 8  | 5  | 128 | 2023 | 64 | 15,91232 | 17 | 0,06565  | 1246,20 | 0,00  | -67,07 | 1179,13 | 596865,37 | 419616,22 | K |
| Ske03-23 | 12,80 | 8  | 5  | 128 | 2023 | 64 | 18,05267 | 16 | 56,16229 | 1365,66 | 0,00  | -67,20 | 1298,45 | 599887,02 | 423692,21 | K |
| Ske03-23 | 14,78 | 26 | 10 | 299 | 2023 | 64 | 18,02757 | 16 | 56,22648 | 1358,51 | 0,00  | -67,20 | 1291,31 | 599836,78 | 423643,90 | K |
| Ske04-23 | 13,24 | 8  | 5  | 128 | 2023 | 64 | 20,14603 | 16 | 51,80617 | 1466,85 | 0,00  | -67,30 | 1399,56 | 603267,90 | 427696,21 | K |
| Ske04-23 | 13,58 | 26 | 10 | 299 | 2023 | 64 | 20,13582 | 16 | 51,83282 | 1462,96 | 0,00  | -67,30 | 1395,67 | 603247,08 | 427676,52 | K |
| Ske05-23 | 13,92 | 8  | 5  | 128 | 2023 | 64 | 22,23402 | 16 | 47,23409 | 1540,72 | 0,00  | -67,35 | 1473,37 | 606813,74 | 431700,01 | K |
| Ske05-23 | 15,79 | 26 | 10 | 299 | 2023 | 64 | 22,22984 | 16 | 47,24418 | 1537,26 | 0,00  | -67,35 | 1469,91 | 606805,90 | 431691,97 | K |
| Skf00-23 | 20,99 | 2  | 5  | 122 | 2023 | 64 | 15,48130 | 15 | 54,09593 | 1011,07 | 0,00  | -66,03 | 945,03  | 650150,17 | 420964,14 | K |
| Skf00-23 | 11,58 | 23 | 10 | 296 | 2023 | 64 | 15,48292 | 15 | 54,09271 | 1004,88 | 0,00  | -66,03 | 938,85  | 650152,63 | 420967,28 | K |
| Skf01-23 | 9,95  | 3  | 5  | 123 | 2023 | 64 | 18,01726 | 16 | 5,02291  | 1349,99 | 0,00  | -66,64 | 1283,36 | 641113,89 | 425251,13 | K |
| Skf01-23 | 13,74 | 23 | 10 | 296 | 2023 | 64 | 18,01480 | 16 | 5,00810  | 1344,86 | 0,00  | -66,64 | 1278,23 | 641126,03 | 425247,13 | K |
| T01-23   | 15,29 | 7  | 5  | 127 | 2023 | 64 | 19,15529 | 18 | 6,52452  | 828,29  | 0,00  | -67,25 | 761,04  | 543110,47 | 424414,05 | K |
| T02-23   | 14,32 | 7  | 5  | 127 | 2023 | 64 | 19,47945 | 18 | 4,54734  | 948,08  | 0,00  | -67,27 | 880,82  | 544695,50 | 425039,16 | K |
| T03-23   | 12,54 | 7  | 5  | 127 | 2023 | 64 | 20,19899 | 17 | 58,61111 | 1129,37 | 0,00  | -67,30 | 1062,07 | 549458,13 | 426449,60 | K |
| T03-23   | 14,89 | 25 | 10 | 298 | 2023 | 64 | 20,19630 | 17 | 58,62751 | 1124,63 | 0,00  | -67,30 | 1057,33 | 549445,00 | 426444,39 | K |
| T04-23   | 11,42 | 7  | 5  | 127 | 2023 | 64 | 21,33609 | 17 | 51,52929 | 1286,66 | 0,00  | -67,36 | 1219,30 | 555124,90 | 428659,66 | K |
| T04-23   | 14,46 | 25 | 10 | 298 | 2023 | 64 | 21,33178 | 17 | 51,54574 | 1282,32 | 0,00  | -67,36 | 1214,96 | 555111,81 | 428651,41 | K |
| T05-23   | 10,83 | 7  | 5  | 127 | 2023 | 64 | 22,26332 | 17 | 43,00304 | 1411,86 | 0,00  | -67,47 | 1344,39 | 561953,42 | 430513,72 | K |
| T05-23   | 13,85 | 25 | 10 | 298 | 2023 | 64 | 22,25949 | 17 | 43,01894 | 1409,80 | -1,72 | -67,47 | 1340,62 | 561940,76 | 430506,36 | K |
| T06-23   | 17,91 | 6  | 5  | 126 | 2023 | 64 | 24,27135 | 17 | 36,52699 | 1535,23 | 0,00  | -67,61 | 1467,62 | 567081,28 | 434353,98 | K |
| T06-23   | 12,53 | 25 | 10 | 298 | 2023 | 64 | 24,26702 | 17 | 36,53949 | 1535,15 | -2,90 | -67,61 | 1464,64 | 567071,41 | 434345,70 | K |
| T07-23   | 15,36 | 6  | 5  | 126 | 2023 | 64 | 25,29334 | 17 | 31,21459 | 1631,41 | 0,00  | -67,70 | 1563,71 | 571305,27 | 436349,26 | K |
| T07-23   | 11,60 | 25 | 10 | 298 | 2023 | 64 | 25,29120 | 17 | 31,22372 | 1629,94 | -1,90 | -67,70 | 1560,34 | 571298,03 | 436345,11 | K |
| T08-23   | 16,03 | 6  | 5  | 126 | 2023 | 64 | 26,29828 | 17 | 27,75570 | 1704,46 | 0,00  | -67,75 | 1636,71 | 574037,23 | 438282,17 | K |
| T08-23   | 11,11 | 25 | 10 | 298 | 2023 | 64 | 26,29798 | 17 | 27,75821 | 1701,57 | 0,00  | -67,75 | 1633,82 | 574035,23 | 438281,57 | K |

## Appendix D: Measured surface velocity at marked sites on Vatnajökull in 2023.

| Site     | Calendar |     | Calendar |     | # of days | translation (m) | velocity |        | (cm/day) (m/annum) |
|----------|----------|-----|----------|-----|-----------|-----------------|----------|--------|--------------------|
|          | day date | #   | day date | #   |           |                 | (°)      | (m)    |                    |
| B07-23   | 230504   | 124 | 231027   | 300 | 176       | 1,90            | 157      | 1,08   | 3,93               |
| B09-23   | 230505   | 125 | 231024   | 297 | 172       | 0,28            | 187      | 0,16   | 0,59               |
| B10-23   | 230505   | 125 | 231024   | 297 | 172       | 0,00            | 270      | 0,00   | 0,00               |
| B11-23   | 230505   | 125 | 231024   | 297 | 172       | 9,48            | 19       | 5,51   | 20,12              |
| B12-23   | 230505   | 125 | 231024   | 297 | 172       | 15,98           | 21       | 9,29   | 33,91              |
| B13-23   | 230504   | 124 | 231026   | 299 | 175       | 17,11           | 25       | 9,77   | 35,68              |
| B13ror15 | 221017   | 290 | 230504   | 124 | 199       | 5,65            | 27       | 2,84   | 10,36              |
| B13ror15 | 230504   | 124 | 231026   | 299 | 175       | 17,94           | 28       | 10,25  | 37,42              |
| B14-23   | 230504   | 124 | 231023   | 296 | 172       | 15,69           | 39       | 9,12   | 33,30              |
| B15-23   | 230504   | 124 | 231024   | 297 | 173       | 12,42           | 49       | 7,18   | 26,21              |
| B16-23   | 230508   | 128 | 231023   | 296 | 168       | 0,64            | 38       | 0,38   | 1,38               |
| B17-23   | 230504   | 124 | 231023   | 296 | 172       | 18,67           | 16       | 10,86  | 39,62              |
| B18-23   | 230503   | 123 | 231023   | 296 | 173       | 10,76           | 346      | 6,22   | 22,70              |
| B19-23   | 230503   | 123 | 231023   | 296 | 173       | 0,72            | 325      | 0,42   | 1,52               |
| Bb0-23   | 230504   | 124 | 231023   | 296 | 172       | 0,94            | 250      | 0,55   | 1,99               |
| Barc-23  | 230531   | 151 | 231024   | 297 | 146       | 4,91            | 95       | 3,36   | 12,28              |
| Bb02-23  | 230531   | 151 | 230912   | 255 | 104       | 3,45            | 95       | 3,31   | 12,10              |
| Bb02-23  | 230912   | 255 | 231024   | 297 | 42        | 1,27            | 94       | 3,02   | 11,03              |
| Bb08-23  | 230531   | 151 | 230912   | 255 | 104       | 3,88            | 81       | 3,73   | 13,62              |
| Bb08-23  | 230912   | 255 | 231024   | 297 | 42        | 1,33            | 97       | 3,17   | 11,58              |
| Bb09-23  | 230531   | 151 | 231024   | 297 | 146       | 2,43            | 99       | 1,66   | 6,07               |
| Bb05-23  | 230531   | 151 | 231024   | 297 | 146       | 3,44            | 197      | 2,35   | 8,59               |
| Bb10-23  | 230531   | 151 | 231024   | 297 | 146       | 8,32            | 122      | 5,70   | 20,80              |
| Bb10-23  | 231024   | 297 | 230912   | 255 | -42       | 4,69            | 6        | -11,17 | -40,77             |
| Bor-23   | 230602   | 153 | 231027   | 300 | 147       | 9,47            | 204      | 6,44   | 23,51              |
| Br1-23   | 230622   | 173 | 231022   | 295 | 122       | 8,74            | 353      | 7,17   | 26,16              |
| Br2-22   | 220330   | 89  | 230621   | 172 | 448       | 4,28            | 150      | 0,96   | 3,49               |
| Br2-23   | 230621   | 172 | 231022   | 295 | 123       | 0,80            | 158      | 0,65   | 2,37               |
| Br3-22   | 220330   | 89  | 230621   | 172 | 448       | 24,67           | 149      | 5,51   | 20,10              |
| Br3-23   | 230621   | 172 | 231022   | 295 | 123       | 6,50            | 146      | 5,28   | 19,28              |
| Br7-23   | 230504   | 124 | 231023   | 296 | 172       | 50,94           | 173      | 29,62  | 108,11             |
| Bru-23   | 230503   | 123 | 231023   | 296 | 173       | 19,45           | 8        | 11,25  | 41,05              |
| Bud-23   | 230503   | 123 | 231023   | 296 | 173       | 21,60           | 4        | 12,48  | 45,56              |
| D05-23   | 230505   | 125 | 231026   | 299 | 174       | 36,73           | 32       | 21,11  | 77,06              |
| D07-23   | 230505   | 125 | 231026   | 299 | 174       | 40,10           | 23       | 23,05  | 84,12              |
| D08-23   | 230505   | 125 | 231026   | 299 | 174       | 17,50           | 6        | 10,06  | 36,70              |
| D12-23   | 230505   | 125 | 231024   | 297 | 172       | 1,01            | 9        | 0,59   | 2,15               |
| E01-22   | 221017   | 290 | 230503   | 123 | 198       | 15,05           | 276      | 7,60   | 27,74              |
| E01-23   | 230503   | 123 | 231024   | 297 | 174       | 20,90           | 19       | 12,01  | 43,84              |
| E02-23   | 230503   | 123 | 231024   | 297 | 174       | 34,40           | 9        | 19,77  | 72,15              |
| E03-23   | 230503   | 123 | 231024   | 297 | 174       | 11,15           | 344      | 6,41   | 23,40              |
| E04-23   | 230503   | 123 | 231024   | 297 | 174       | 1,32            | 15       | 0,76   | 2,78               |
| E07-23   | 230503   | 123 | 231024   | 297 | 174       | 11,40           | 39       | 6,55   | 23,91              |
| E08-23   | 230503   | 123 | 231024   | 297 | 174       | 4,38            | 3        | 2,51   | 9,18               |
| Fl01-23  | 230503   | 123 | 231023   | 296 | 173       | 17,23           | 134      | 9,96   | 36,36              |
| G02-23   | 230507   | 127 | 231024   | 297 | 170       | 8,39            | 201      | 4,94   | 18,02              |
| G03-23   | 230507   | 127 | 231024   | 297 | 170       | 3,95            | 195      | 2,32   | 8,48               |
| G04-23   | 230506   | 126 | 231024   | 297 | 171       | 0,63            | 19       | 0,37   | 1,34               |
| Go1-23   | 230506   | 126 | 231024   | 297 | 171       | 2,80            | 170      | 1,64   | 5,98               |
| Haab-23  | 230506   | 126 | 231025   | 298 | 172       | 0,85            | 10       | 0,49   | 1,80               |
| Hof01-23 | 230503   | 123 | 231024   | 297 | 174       | 11,72           | 180      | 6,74   | 24,59              |

|          |        |     |        |     |     |       |     |       |        |
|----------|--------|-----|--------|-----|-----|-------|-----|-------|--------|
| K01-23   | 230506 | 126 | 231025 | 298 | 172 | 5,64  | 293 | 3,28  | 11,96  |
| K02-23   | 230506 | 126 | 231025 | 298 | 172 | 13,53 | 297 | 7,87  | 28,72  |
| K03-23   | 230506 | 126 | 231025 | 298 | 172 | 15,86 | 291 | 9,22  | 33,65  |
| K04-23   | 230506 | 126 | 231025 | 298 | 172 | 21,67 | 289 | 12,60 | 45,98  |
| K05-23   | 230506 | 126 | 231025 | 298 | 172 | 12,98 | 247 | 7,55  | 27,55  |
| K06-23   | 230506 | 126 | 231024 | 297 | 171 | 2,16  | 109 | 1,26  | 4,60   |
| K07-23   | 230506 | 126 | 231025 | 298 | 172 | 1,36  | 284 | 0,79  | 2,89   |
| Kverk-23 | 230601 | 152 | 231024 | 297 | 145 | 0,45  | 355 | 0,31  | 1,12   |
| S02-23   | 230506 | 126 | 231025 | 298 | 172 | 26,45 | 192 | 15,38 | 56,12  |
| S04-23   | 230506 | 126 | 231025 | 298 | 172 | 38,45 | 205 | 22,35 | 81,59  |
| S05-23   | 230506 | 126 | 231025 | 298 | 172 | 14,66 | 255 | 8,52  | 31,10  |
| Ske03-23 | 230508 | 128 | 231026 | 299 | 171 | 69,57 | 228 | 40,69 | 148,50 |
| Ske04-23 | 230508 | 128 | 231026 | 299 | 171 | 28,60 | 229 | 16,73 | 61,06  |
| Ske05-23 | 230508 | 128 | 231026 | 299 | 171 | 11,22 | 226 | 6,56  | 23,94  |
| Skf00-23 | 230502 | 122 | 231023 | 296 | 174 | 3,97  | 41  | 2,28  | 8,33   |
| Skf01-23 | 230503 | 123 | 231023 | 296 | 173 | 12,78 | 111 | 7,39  | 26,97  |
| T03-23   | 230507 | 127 | 231025 | 298 | 171 | 14,12 | 249 | 8,26  | 30,13  |
| T04-23   | 230507 | 127 | 231025 | 298 | 171 | 15,46 | 239 | 9,04  | 33,00  |
| T05-23   | 230507 | 127 | 231025 | 298 | 171 | 14,62 | 241 | 8,55  | 31,22  |
| T06-23   | 230506 | 126 | 231025 | 298 | 172 | 12,85 | 231 | 7,47  | 27,27  |
| T07-23   | 230506 | 126 | 231025 | 298 | 172 | 8,33  | 242 | 4,84  | 17,68  |
| T08-23   | 230506 | 126 | 231025 | 298 | 172 | 2,09  | 255 | 1,21  | 4,43   |

## Appendix E: Melt water runoff to selected rivers in summer 2023, derived from summer surface balance.

$\Delta S$ : area in each elevation range where summer balance is negative,  $\Sigma \Delta S$ : cumulative area above a given elevation,  $\Delta Q_s$ : melt water runoff from a given elevation range,  $\Sigma \Delta Q_s$ : cumulative melt water runoff from an area above given elevation.

### Tungnaá water drainage basin

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |      |       |      |       |
|------|------|------|-------|------|-------|
| 1350 | 1400 | 0,3  | 0,3   | 0,5  | 0,5   |
| 1300 | 1350 | 6    | 6,3   | 11,8 | 12,4  |
| 1250 | 1300 | 9,8  | 16,1  | 22,6 | 35,0  |
| 1200 | 1250 | 10,7 | 26,8  | 27,9 | 62,9  |
| 1150 | 1200 | 9,5  | 36,4  | 28,2 | 91,1  |
| 1100 | 1150 | 11   | 47,4  | 36,0 | 127,1 |
| 1050 | 1100 | 10,3 | 57,7  | 37,4 | 164,5 |
| 1000 | 1050 | 9,5  | 67,2  | 38,1 | 202,6 |
| 950  | 1000 | 8,8  | 76,1  | 38,2 | 240,8 |
| 900  | 950  | 8,5  | 84,6  | 39,6 | 280,4 |
| 850  | 900  | 6,3  | 90,9  | 31,8 | 312,2 |
| 800  | 850  | 6,3  | 97,1  | 33,8 | 346,0 |
| 750  | 800  | 4,6  | 101,8 | 26,2 | 372,2 |
| 700  | 750  | 2,5  | 104,2 | 14,5 | 386,7 |
| 650  | 700  | 0,1  | 104,4 | 0,8  | 387,5 |

### Sylgja water drainage basin

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |     |      |      |       |
|------|------|-----|------|------|-------|
| 1300 | 1350 | 1,1 | 1,1  | 2,3  | 2,3   |
| 1250 | 1300 | 3,4 | 4,5  | 8,2  | 10,5  |
| 1200 | 1250 | 5,3 | 9,7  | 14,2 | 24,7  |
| 1150 | 1200 | 8   | 17,8 | 23,5 | 48,2  |
| 1100 | 1150 | 5,8 | 23,5 | 18,9 | 67,2  |
| 1050 | 1100 | 6   | 29,5 | 21,5 | 88,7  |
| 1000 | 1050 | 5,7 | 35,3 | 22,5 | 111,1 |
| 950  | 1000 | 1,8 | 37,1 | 7,7  | 118,8 |
| 900  | 950  | 0,7 | 37,8 | 2,9  | 121,7 |

### Western Skaftá cauldron water drainage basin

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |     |      |     |      |
|------|------|-----|------|-----|------|
| 1700 | 1750 | 2,3 | 2,3  | 1,1 | 1,1  |
| 1650 | 1700 | 7,1 | 9,4  | 3,7 | 4,8  |
| 1600 | 1650 | 7,9 | 17,4 | 4,8 | 9,6  |
| 1550 | 1600 | 5   | 22,4 | 3,4 | 13,1 |
| 1500 | 1550 | 2,6 | 25,0 | 2,0 | 15,0 |

**Eastern Skaftár cauldron water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |     |      |     |      |
|------|------|-----|------|-----|------|
| 1700 | 1750 | 2,3 | 2,3  | 1,1 | 1,1  |
| 1650 | 1700 | 7,1 | 9,4  | 3,7 | 4,8  |
| 1600 | 1650 | 7,9 | 17,4 | 4,8 | 9,6  |
| 1550 | 1600 | 5   | 22,4 | 3,4 | 13,1 |
| 1500 | 1550 | 2,6 | 25,0 | 2,0 | 15,0 |

**Grímsvötn water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |      |       |      |       |
|------|------|------|-------|------|-------|
| 1900 | 1950 | 0,4  | 0,4   | 0,1  | 0,1   |
| 1850 | 1900 | 1,4  | 1,8   | 0,3  | 0,4   |
| 1800 | 1850 | 1,7  | 3,5   | 0,5  | 0,8   |
| 1750 | 1800 | 4,9  | 8,3   | 2,1  | 2,9   |
| 1700 | 1750 | 24   | 32,3  | 11,4 | 14,4  |
| 1650 | 1700 | 48   | 80,3  | 27,4 | 41,8  |
| 1600 | 1650 | 30,7 | 111,0 | 21,0 | 62,7  |
| 1550 | 1600 | 19,6 | 130,6 | 16,1 | 78,8  |
| 1500 | 1550 | 16,2 | 146,8 | 16,2 | 95,0  |
| 1450 | 1500 | 9,5  | 156,3 | 12,5 | 107,5 |
| 1400 | 1450 | 13,7 | 170,0 | 23,5 | 130,9 |
| 1350 | 1400 | 1,2  | 171,3 | 2,1  | 133,0 |

**Kaldakvísl water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |      |       |      |       |
|------|------|------|-------|------|-------|
| 1950 | 2000 | 0,1  | 0,1   | 0,0  | 0,0   |
| 1900 | 1950 | 6,5  | 6,6   | 0,5  | 0,5   |
| 1850 | 1900 | 6,5  | 13,1  | 1,2  | 1,7   |
| 1800 | 1850 | 6,2  | 19,3  | 1,8  | 3,5   |
| 1750 | 1800 | 10,9 | 30,2  | 3,8  | 7,4   |
| 1700 | 1750 | 20,3 | 50,5  | 9,0  | 16,3  |
| 1650 | 1700 | 16,8 | 67,3  | 9,4  | 25,8  |
| 1600 | 1650 | 14,5 | 81,8  | 10,0 | 35,7  |
| 1550 | 1600 | 18,4 | 100,2 | 16,0 | 51,7  |
| 1500 | 1550 | 24,1 | 124,3 | 25,6 | 77,3  |
| 1450 | 1500 | 27,8 | 152,1 | 34,5 | 111,8 |
| 1400 | 1450 | 22,3 | 174,4 | 33,1 | 144,9 |
| 1350 | 1400 | 20,5 | 194,9 | 37,9 | 182,8 |
| 1300 | 1350 | 19,2 | 214,1 | 45,9 | 228,7 |
| 1250 | 1300 | 20,5 | 234,7 | 58,7 | 287,4 |
| 1200 | 1250 | 20   | 254,6 | 64,2 | 351,6 |
| 1150 | 1200 | 19   | 273,6 | 67,2 | 418,8 |
| 1100 | 1150 | 17   | 290,6 | 67,1 | 485,9 |
| 1050 | 1100 | 15,7 | 306,4 | 68,5 | 554,3 |
| 1000 | 1050 | 12,9 | 319,2 | 59,6 | 613,9 |
| 950  | 1000 | 7,2  | 326,5 | 35,9 | 649,9 |
| 900  | 950  | 1,2  | 327,7 | 6,1  | 656,0 |

**Jökulsá á Fjöllum water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\sum \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\sum \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|----------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|----------------------------------|-------------------------------------|--|

|      |      |      |        |       |        |
|------|------|------|--------|-------|--------|
| 1950 | 2000 | 0,9  | 0,9    | 0,0   | 0,0    |
| 1900 | 1950 | 11,5 | 12,4   | 0,9   | 1,0    |
| 1850 | 1900 | 25   | 37,4   | 5,2   | 6,1    |
| 1800 | 1850 | 18,4 | 55,8   | 5,3   | 11,5   |
| 1750 | 1800 | 21,9 | 77,7   | 7,9   | 19,4   |
| 1700 | 1750 | 39,3 | 117,0  | 16,4  | 35,8   |
| 1650 | 1700 | 81   | 198,0  | 41,2  | 77,1   |
| 1600 | 1650 | 122  | 320,3  | 73,7  | 150,8  |
| 1550 | 1600 | 101  | 421,2  | 74,1  | 224,9  |
| 1500 | 1550 | 92,6 | 513,8  | 82,1  | 307,0  |
| 1450 | 1500 | 79,5 | 593,3  | 83,6  | 390,6  |
| 1400 | 1450 | 68,7 | 662,0  | 77,0  | 467,6  |
| 1350 | 1400 | 54,2 | 716,2  | 66,5  | 534,1  |
| 1300 | 1350 | 42,7 | 758,9  | 65,4  | 599,5  |
| 1250 | 1300 | 46,3 | 805,2  | 91,1  | 690,5  |
| 1200 | 1250 | 49,3 | 854,4  | 122,9 | 813,4  |
| 1150 | 1200 | 48,7 | 903,1  | 152,5 | 965,9  |
| 1100 | 1150 | 44,1 | 947,2  | 166,1 | 1132,1 |
| 1050 | 1100 | 31   | 978,2  | 134,5 | 1266,6 |
| 1000 | 1050 | 31,1 | 1009,3 | 142,3 | 1408,9 |
| 950  | 1000 | 28,9 | 1038,1 | 141,2 | 1550,0 |
| 900  | 950  | 24,7 | 1062,8 | 129,2 | 1679,2 |
| 850  | 900  | 20,5 | 1083,3 | 115,3 | 1794,5 |
| 800  | 850  | 16,5 | 1099,8 | 103,0 | 1897,5 |
| 750  | 800  | 8,5  | 1108,4 | 58,6  | 1956,1 |
| 700  | 750  | 0,3  | 1108,7 | 2,5   | 1958,6 |

**Kreppa and Kverká water drainage basin**

| Elevation<br>(m a. s. l.) |      | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>( $10^6 \text{m}^3$ ) | $\Sigma \Delta Q_s$<br>( $10^6 \text{m}^3$ ) |
|---------------------------|------|-----------------------------|------------------------------------|---------------------------------------|--|
| 1900                      | 1950 | 0,1                         | 0,1                                | 0,1                                   | 0,1  |
| 1850                      | 1900 | 1,4                         | 1,5                                | 0,6                                   | 0,7  |
| 1800                      | 1850 | 4,4                         | 5,9                                | 1,5                                   | 2,2  |
| 1750                      | 1800 | 2,7                         | 8,6                                | 1,0                                   | 3,2  |
| 1700                      | 1750 | 3,8                         | 12,4                               | 1,6                                   | 4,9  |
| 1650                      | 1700 | 5,3                         | 17,7                               | 2,6                                   | 7,5  |
| 1600                      | 1650 | 41,6                        | 59,3                               | 25,9                                  | 33,4   |
| 1550                      | 1600 | 20,4                        | 79,7                               | 14,1                                  | 47,5   |
| 1500                      | 1550 | 13,4                        | 93,1                               | 10,8                                  | 58,2   |
| 1450                      | 1500 | 16,3                        | 109,4                              | 14,9                                  | 73,1   |
| 1400                      | 1450 | 20,1                        | 129,5                              | 20,7                                  | 93,9   |
| 1350                      | 1400 | 25,9                        | 155,4                              | 29,3                                  | 123,2  |
| 1300                      | 1350 | 20,3                        | 175,7                              | 27,0                                  | 150,2  |
| 1250                      | 1300 | 15,3                        | 191,0                              | 26,2                                  | 176,4  |
| 1200                      | 1250 | 17,7                        | 208,7                              | 43,0                                  | 219,4  |
| 1150                      | 1200 | 17,2                        | 225,8                              | 52,9                                  | 272,3  |
| 1100                      | 1150 | 16,1                        | 242,0                              | 55,3                                  | 327,6  |
| 1050                      | 1100 | 10,4                        | 252,4                              | 38,7                                  | 366,3  |
| 1000                      | 1050 | 11,6                        | 263,9                              | 46,6                                  | 412,8  |
| 950                       | 1000 | 12,7                        | 276,6                              | 55,1                                  | 468,0  |
| 900                       | 950  | 12,8                        | 289,4                              | 59,4                                  | 527,4  |
| 850                       | 900  | 11,9                        | 301,1                              | 58,8                                  | 586,2  |
| 800                       | 850  | 9,8                         | 311,0                              | 52,3                                  | 638,5  |
| 750                       | 800  | 6,7                         | 317,7                              | 38,4                                  | 676,9  |
| 700                       | 750  | 3,4                         | 33,9                               | 20,9                                  | 176,3  |
| 650                       | 700  | 0,2                         | 34,1                               | 1,0                                   | 177,3  |

**Hálslón water drainage basin**

| Elevation<br>(m a. s. l.) |      | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>( $10^6 \text{m}^3$ ) | $\Sigma \Delta Q_s$<br>( $10^6 \text{m}^3$ ) |
|---------------------------|------|-----------------------------|------------------------------------|---------------------------------------|--|
| 1600                      | 1650 | 11,7                        | 11,7                               | 7,8                                   | 7,8  |
| 1550                      | 1600 | 33,6                        | 45,3                               | 24,0                                  | 31,8   |
| 1500                      | 1550 | 65,2                        | 110,6                              | 51,1                                  | 82,9   |
| 1450                      | 1500 | 70                          | 180,6                              | 62,7                                  | 145,6  |
| 1400                      | 1450 | 98,9                        | 279,5                              | 94,7                                  | 240,4  |
| 1350                      | 1400 | 133                         | 412,4                              | 148,2                                 | 388,5  |
| 1300                      | 1350 | 129                         | 541,5                              | 171,8                                 | 560,3  |
| 1250                      | 1300 | 122                         | 663,9                              | 203,7                                 | 764,0  |
| 1200                      | 1250 | 97,2                        | 761,1                              | 204,0                                 | 968,1  |
| 1150                      | 1200 | 81,9                        | 843,1                              | 218,5                                 | 1186,6                                       |
| 1100                      | 1150 | 64                          | 907,0                              | 203,5                                 | 1390,2                                       |
| 1050                      | 1100 | 54,6                        | 961,6                              | 197,1                                 | 1587,3                                       |
| 1000                      | 1050 | 45,8                        | 1007,5                             | 181,7                                 | 1769,0                                       |
| 950                       | 1000 | 39,1                        | 1046,6                             | 167,6                                 | 1936,6                                       |
| 900                       | 950  | 31,9                        | 1078,4                             | 146,2                                 | 2082,8                                       |
| 850                       | 900  | 26,6                        | 1105,0                             | 130,3                                 | 2213,1                                       |
| 800                       | 850  | 24,4                        | 1129,5                             | 127,9                                 | 2341,1                                       |
| 750                       | 800  | 24,2                        | 1153,7                             | 136,4                                 | 2477,5                                       |
| 700                       | 750  | 22,7                        | 1176,4                             | 139,0                                 | 2616,4                                       |
| 650                       | 700  | 9,4                         | 1185,8                             | 61,0                                  | 2677,4                                       |
| 600                       | 650  | 0,5                         | 1186,3                             | 3,3                                   | 2680,7                                       |

**Jökulsá á Fljótsdal water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |      |       |      |       |
|------|------|------|-------|------|-------|
| 1550 | 1600 | 0    | 0,0   | 0,0  | 0,0   |
| 1500 | 1550 | 0,1  | 0,1   | 0,1  | 0,1   |
| 1450 | 1500 | 1,1  | 1,2   | 1,1  | 1,2   |
| 1400 | 1450 | 2    | 3,2   | 2,2  | 3,5   |
| 1350 | 1400 | 2,8  | 6,1   | 3,4  | 6,9   |
| 1300 | 1350 | 5,4  | 11,5  | 7,6  | 14,4  |
| 1250 | 1300 | 15,8 | 27,3  | 28,9 | 43,3  |
| 1200 | 1250 | 14,8 | 42,1  | 35,3 | 78,6  |
| 1150 | 1200 | 16,4 | 58,6  | 48,9 | 127,6 |
| 1100 | 1150 | 14   | 72,6  | 47,9 | 175,5 |
| 1050 | 1100 | 11,7 | 84,3  | 43,8 | 219,3 |
| 1000 | 1050 | 10,8 | 95,1  | 43,7 | 262,9 |
| 950  | 1000 | 8,7  | 103,8 | 38,4 | 301,4 |
| 900  | 950  | 5,5  | 109,3 | 26,0 | 327,4 |
| 850  | 900  | 4,2  | 113,5 | 20,7 | 348,1 |
| 800  | 850  | 2,9  | 116,5 | 15,0 | 363,1 |
| 750  | 800  | 1,8  | 118,2 | 9,6  | 372,7 |
| 700  | 750  | 1,6  | 119,8 | 9,4  | 382,1 |
| 650  | 700  | 0,6  | 120,5 | 3,9  | 386,0 |

**Hornafjarðarfljót water drainage basin**

| Elevation<br>(m a. s. l.) |      | $\Delta S$<br>km <sup>2</sup> | $\Sigma \Delta S$<br>km <sup>2</sup> | $\Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|---------------------------|------|-------------------------------|--------------------------------------|---|--|
| 1450                      | 1500 | 1,2                           | 1,2                                  | 1,3   | 1,3  |
| 1400                      | 1450 | 8,3                           | 9,5                                  | 7,9   | 9,2  |
| 1350                      | 1400 | 12,4                          | 21,9                                 | 13,2  | 22,4   |
| 1300                      | 1350 | 18,9                          | 40,8                                 | 23,9  | 46,3   |
| 1250                      | 1300 | 37,3                          | 78,1                                 | 60,1  | 106,4  |
| 1200                      | 1250 | 28,7                          | 106,8                                | 51,1  | 157,5  |
| 1150                      | 1200 | 19,9                          | 126,7                                | 41,6  | 199,1  |
| 1100                      | 1150 | 18,3                          | 145,0                                | 43,9  | 243,0  |
| 1050                      | 1100 | 13,8                          | 158,8                                | 38,7  | 281,7  |
| 1000                      | 1050 | 10,6                          | 169,4                                | 34,0  | 315,6  |
| 950                       | 1000 | 10,1                          | 179,5                                | 35,9  | 351,5  |
| 900                       | 950  | 8,1                           | 187,5                                | 30,9  | 382,4  |
| 850                       | 900  | 5,1                           | 192,6                                | 20,9  | 403,3  |
| 800                       | 850  | 4,2                           | 196,8                                | 18,3  | 421,6  |
| 750                       | 800  | 3,3                           | 200,1                                | 14,7  | 436,3  |
| 700                       | 750  | 3,1                           | 203,2                                | 15,0  | 451,3  |
| 650                       | 700  | 3,3                           | 206,4                                | 17,5  | 468,8  |
| 600                       | 650  | 2,6                           | 209,0                                | 14,6  | 483,4  |
| 550                       | 600  | 1,9                           | 210,9                                | 11,1  | 494,5  |
| 500                       | 550  | 1,7                           | 212,7                                | 10,3  | 504,9  |
| 450                       | 500  | 1,3                           | 214,0                                | 8,4   | 513,3  |
| 400                       | 450  | 1                             | 215,0                                | 6,9   | 520,1  |
| 350                       | 400  | 1                             | 216,0                                | 6,8   | 527,0  |
| 300                       | 350  | 0,6                           | 216,6                                | 4,4   | 531,4  |
| 250                       | 300  | 0,7                           | 217,2                                | 5,3   | 536,7  |
| 200                       | 250  | 0,9                           | 218,1                                | 7,3   | 544,0  |
| 150                       | 200  | 1,8                           | 219,9                                | 15,5  | 559,6  |
| 100                       | 150  | 2,4                           | 222,3                                | 21,6  | 581,2  |
| 50                        | 100  | 2,2                           | 224,5                                | 20,9  | 602,1  |
| 0                         | 50   | 2,9                           | 227,4                                | 29,1  | 631,2  |

Jökulsá á Breiðamerkursandi water drainage basin

| Elevation<br>(m a. s. l.) | $\Delta S$<br>km <sup>2</sup> | $\Sigma \Delta S$<br>km <sup>2</sup> | $\Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|---------------------------|-------------------------------|--------------------------------------|---|--|
|---------------------------|-------------------------------|--------------------------------------|---|--|

|      |      |      |       |       |        |
|------|------|------|-------|-------|--------|
| 1700 | 1750 | 1    | 1,0   | 0,6   | 0,6    |
| 1650 | 1700 | 4,2  | 5,2   | 2,6   | 3,3    |
| 1600 | 1650 | 14,4 | 19,5  | 9,2   | 12,5   |
| 1550 | 1600 | 19,1 | 38,6  | 13,3  | 25,8   |
| 1500 | 1550 | 22,7 | 61,3  | 18,7  | 44,6   |
| 1450 | 1500 | 36,2 | 97,6  | 33,8  | 78,3   |
| 1400 | 1450 | 50,9 | 148,5 | 52,7  | 131,1  |
| 1350 | 1400 | 83   | 231,5 | 99,6  | 230,7  |
| 1300 | 1350 | 82,6 | 314,1 | 112,1 | 342,8  |
| 1250 | 1300 | 51   | 365,1 | 76,6  | 419,4  |
| 1200 | 1250 | 33,6 | 398,7 | 57,3  | 476,7  |
| 1150 | 1200 | 27,2 | 425,9 | 54,4  | 531,1  |
| 1100 | 1150 | 22,1 | 448,0 | 51,6  | 582,7  |
| 1050 | 1100 | 18,4 | 466,4 | 48,5  | 631,2  |
| 1000 | 1050 | 14,5 | 480,9 | 42,6  | 673,8  |
| 950  | 1000 | 15,2 | 496,1 | 49,4  | 723,2  |
| 900  | 950  | 15,5 | 511,7 | 54,8  | 778,0  |
| 850  | 900  | 13,1 | 524,7 | 50,5  | 828,5  |
| 800  | 850  | 15,2 | 539,9 | 63,7  | 892,2  |
| 750  | 800  | 16,9 | 556,9 | 77,1  | 969,3  |
| 700  | 750  | 12,9 | 569,8 | 63,4  | 1032,6 |
| 650  | 700  | 20,3 | 590,1 | 105,7 | 1138,3 |
| 600  | 650  | 20,9 | 611,0 | 114,8 | 1253,2 |
| 550  | 600  | 15,9 | 626,9 | 92,7  | 1345,9 |
| 500  | 550  | 14,1 | 641,0 | 85,6  | 1431,5 |
| 450  | 500  | 4,8  | 645,8 | 30,8  | 1462,3 |
| 400  | 450  | 6,1  | 651,9 | 41,2  | 1503,5 |
| 350  | 400  | 5,7  | 657,6 | 39,9  | 1543,4 |
| 300  | 350  | 4,5  | 662,1 | 32,9  | 1576,3 |
| 250  | 300  | 4,6  | 666,7 | 36,0  | 1612,3 |
| 200  | 250  | 4,9  | 671,6 | 40,4  | 1652,7 |
| 150  | 200  | 4,4  | 676,0 | 37,7  | 1690,4 |
| 100  | 150  | 4,7  | 680,7 | 42,1  | 1732,4 |
| 50   | 100  | 4,1  | 684,8 | 38,4  | 1770,8 |
| 0    | 50   | 1,2  | 686,0 | 12,1  | 1782,9 |

**Breiðárlón/Fjallsárlón water drainage basin**

| Elevation<br>(m a. s. l.) |      | $\Delta S$<br>km <sup>2</sup> | $\Sigma \Delta S$<br>km <sup>2</sup> | $\Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|---------------------------|------|-------------------------------|--------------------------------------|---|--|
| 2000                      | 2050 | 0,1                           | 0,1                                  | 0,0   | 0,0  |
| 1950                      | 2000 | 0,6                           | 0,7                                  | 0,2   | 0,2  |
| 1900                      | 1950 | 0,9                           | 1,7                                  | 0,2   | 0,4  |
| 1850                      | 1900 | 1,6                           | 3,2                                  | 0,2   | 0,7  |
| 1800                      | 1850 | 2                             | 5,2                                  | 0,1   | 0,8  |
| 1750                      | 1800 | 2,5                           | 7,7                                  | 0,2   | 1,0  |
| 1700                      | 1750 | 3                             | 10,7                                 | 0,6   | 1,5  |
| 1650                      | 1700 | 3,1                           | 13,8                                 | 1,0   | 2,5  |
| 1600                      | 1650 | 4,3                           | 18,0                                 | 1,9   | 4,5  |
| 1550                      | 1600 | 4,3                           | 22,3                                 | 2,6   | 7,1  |
| 1500                      | 1550 | 5,7                           | 28,1                                 | 4,6   | 11,7   |
| 1450                      | 1500 | 5                             | 33,1                                 | 4,8   | 16,6   |
| 1400                      | 1450 | 5,1                           | 38,1                                 | 5,9   | 22,4   |
| 1350                      | 1400 | 6,3                           | 44,5                                 | 9,8   | 32,2   |
| 1300                      | 1350 | 12,5                          | 57,0                                 | 24,6  | 56,8   |
| 1250                      | 1300 | 6,4                           | 63,4                                 | 13,6  | 70,4   |
| 1200                      | 1250 | 5,5                           | 68,9                                 | 11,1  | 81,5   |
| 1150                      | 1200 | 4,7                           | 73,6                                 | 9,3   | 90,7   |
| 1100                      | 1150 | 4,2                           | 77,8                                 | 9,3   | 100,0  |
| 1050                      | 1100 | 4,6                           | 82,5                                 | 11,2  | 111,2  |
| 1000                      | 1050 | 5,6                           | 88,0                                 | 14,9  | 126,1  |
| 950                       | 1000 | 6,2                           | 94,3                                 | 20,1  | 146,1  |
| 900                       | 950  | 7,2                           | 101,5                                | 25,5  | 171,6  |
| 850                       | 900  | 5,7                           | 107,2                                | 21,9  | 193,5  |
| 800                       | 850  | 6,8                           | 114,0                                | 28,7  | 222,1  |
| 750                       | 800  | 7,9                           | 121,9                                | 35,9  | 258,1  |
| 700                       | 750  | 6,2                           | 128,1                                | 30,6  | 288,6  |
| 650                       | 700  | 5,1                           | 133,2                                | 26,6  | 315,2  |
| 600                       | 650  | 6,2                           | 139,4                                | 34,0  | 349,3  |
| 550                       | 600  | 7                             | 146,4                                | 41,0  | 390,3  |
| 500                       | 550  | 7,6                           | 154,0                                | 46,3  | 436,6  |
| 450                       | 500  | 7,9                           | 162,0                                | 50,9  | 487,6  |
| 400                       | 450  | 8                             | 169,9                                | 53,5  | 541,0  |
| 350                       | 400  | 9,9                           | 179,8                                | 69,5  | 610,5  |
| 300                       | 350  | 8                             | 187,8                                | 59,4  | 669,9  |
| 250                       | 300  | 6                             | 193,8                                | 46,9  | 716,8  |
| 200                       | 250  | 6                             | 199,8                                | 49,0  | 765,8  |
| 150                       | 200  | 5,6                           | 205,4                                | 47,9  | 813,7  |
| 100                       | 150  | 5,6                           | 211,0                                | 50,5  | 864,2  |
| 50                        | 100  | 3,9                           | 214,9                                | 37,4  | 901,6  |
| 0                         | 50   | 5                             | 220,0                                | 52,9  | 954,5  |

**Skeiðarársandur (Gígja) water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>km <sup>2</sup> | $\Sigma \Delta S$<br>km <sup>2</sup> | $\Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|---------------------------|-------------------------------|--------------------------------------|---|--|
|---------------------------|-------------------------------|--------------------------------------|---|--|

|      |      |      |        |       |        |
|------|------|------|--------|-------|--------|
| 1700 | 1750 | 1,8  | 1,8    | 0,9   | 0,9    |
| 1650 | 1700 | 21,9 | 23,8   | 13,3  | 14,2   |
| 1600 | 1650 | 83,1 | 106,8  | 52,5  | 66,7   |
| 1550 | 1600 | 85,8 | 192,6  | 61,9  | 128,7  |
| 1500 | 1550 | 111  | 303,3  | 90,8  | 219,5  |
| 1450 | 1500 | 106  | 409,7  | 102,3 | 322,0  |
| 1400 | 1450 | 104  | 513,3  | 119,4 | 441,4  |
| 1350 | 1400 | 90,7 | 604,0  | 123,2 | 564,7  |
| 1300 | 1350 | 77,4 | 681,4  | 118,8 | 683,5  |
| 1250 | 1300 | 68,7 | 750,1  | 123,3 | 806,8  |
| 1200 | 1250 | 59,7 | 809,8  | 127,2 | 934,0  |
| 1150 | 1200 | 54,1 | 863,8  | 134,5 | 1068,5 |
| 1100 | 1150 | 50,3 | 914,2  | 139,7 | 1208,1 |
| 1050 | 1100 | 45,4 | 959,5  | 140,3 | 1348,4 |
| 1000 | 1050 | 40   | 999,5  | 134,6 | 1482,9 |
| 950  | 1000 | 39,4 | 1039,0 | 143,3 | 1626,2 |
| 900  | 950  | 35,8 | 1074,8 | 142,8 | 1769,0 |
| 850  | 900  | 37,6 | 1112,4 | 163,2 | 1932,2 |
| 800  | 850  | 32,1 | 1144,4 | 149,2 | 2081,4 |
| 750  | 800  | 28,3 | 1172,7 | 140,3 | 2221,6 |
| 700  | 750  | 23,6 | 1196,3 | 124,4 | 2346,1 |
| 650  | 700  | 21,9 | 1218,2 | 123,6 | 2469,6 |
| 600  | 650  | 14,5 | 1232,8 | 86,9  | 2556,6 |
| 550  | 600  | 20   | 1252,7 | 124,9 | 2681,6 |
| 500  | 550  | 21,9 | 1274,7 | 144,6 | 2826,1 |
| 450  | 500  | 16,5 | 1291,1 | 112,9 | 2939,0 |
| 400  | 450  | 11,4 | 1302,6 | 82,5  | 3021,5 |
| 350  | 400  | 11,5 | 1314,1 | 86,4  | 3107,9 |
| 300  | 350  | 12,9 | 1327,0 | 101,2 | 3209,1 |
| 250  | 300  | 13,1 | 1340,2 | 108,1 | 3317,2 |
| 200  | 250  | 11,6 | 1351,7 | 100,2 | 3417,3 |
| 150  | 200  | 11,6 | 1363,3 | 103,2 | 3520,5 |
| 100  | 150  | 9,6  | 1372,8 | 88,5  | 3609,0 |
| 50   | 100  | 6,8  | 1379,6 | 64,0  | 3673,0 |
| 0    | 50   | 3,5  | 1383,3 | 34,2  | 3707,2 |

**Djúpá water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |     |      |      |       |
|------|------|-----|------|------|-------|
| 1450 | 1500 | 0,1 | 0,1  | 0,1  | 0,1   |
| 1400 | 1450 | 0,3 | 0,4  | 0,4  | 0,5   |
| 1350 | 1400 | 0,6 | 1,0  | 1,0  | 1,5   |
| 1300 | 1350 | 3,4 | 4,4  | 6,4  | 7,9   |
| 1250 | 1300 | 3,2 | 7,5  | 6,8  | 14,7  |
| 1200 | 1250 | 2,9 | 10,4 | 7,1  | 21,8  |
| 1150 | 1200 | 3,2 | 13,6 | 8,8  | 30,6  |
| 1100 | 1150 | 5   | 18,7 | 15,6 | 46,3  |
| 1050 | 1100 | 5   | 23,6 | 17,8 | 64,1  |
| 1000 | 1050 | 8,4 | 32,1 | 33,6 | 97,6  |
| 950  | 1000 | 7,3 | 39,3 | 32,2 | 129,9 |
| 900  | 950  | 7,4 | 46,7 | 35,0 | 164,8 |
| 850  | 900  | 6   | 52,7 | 30,7 | 195,6 |
| 800  | 850  | 5,8 | 58,5 | 31,2 | 226,8 |
| 750  | 800  | 5,9 | 64,4 | 33,8 | 260,6 |
| 700  | 750  | 3,6 | 68,1 | 22,0 | 282,6 |
| 650  | 700  | 2   | 70,1 | 12,7 | 295,3 |
| 600  | 650  | 0,1 | 70,1 | 0,6  | 295,9 |

**Brunná water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>$\text{km}^2$ | $\Sigma \Delta S$<br>$\text{km}^2$ | $\Delta Q_s$<br>$(10^6 \text{m}^3)$ | $\Sigma \Delta Q_s$<br>$(10^6 \text{m}^3)$ |
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|
|---------------------------|-----------------------------|------------------------------------|-------------------------------------|--|

|      |      |     |      |      |       |
|------|------|-----|------|------|-------|
| 1000 | 1050 | 0,7 | 0,7  | 2,7  | 2,7   |
| 950  | 1000 | 1,8 | 2,4  | 7,8  | 10,5  |
| 900  | 950  | 3,8 | 6,2  | 17,7 | 28,2  |
| 850  | 900  | 3,9 | 10,1 | 19,4 | 47,6  |
| 800  | 850  | 3,6 | 13,7 | 19,7 | 67,2  |
| 750  | 800  | 3,9 | 17,7 | 22,4 | 89,6  |
| 700  | 750  | 4,4 | 22,1 | 26,3 | 116,0 |
| 650  | 700  | 5,2 | 27,2 | 33,1 | 149,1 |
| 600  | 650  | 2,5 | 29,8 | 17,0 | 166,1 |
| 550  | 600  | 0   | 29,8 | 0,0  | 166,1 |

**Hverfisfljót water drainage basin**

| Elevation<br>(m a. s. l.) | $\Delta S$<br>km <sup>2</sup> | $\Sigma \Delta S$<br>km <sup>2</sup> | $\Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|---------------------------|-------------------------------|--------------------------------------|---|--|
|---------------------------|-------------------------------|--------------------------------------|---|--|

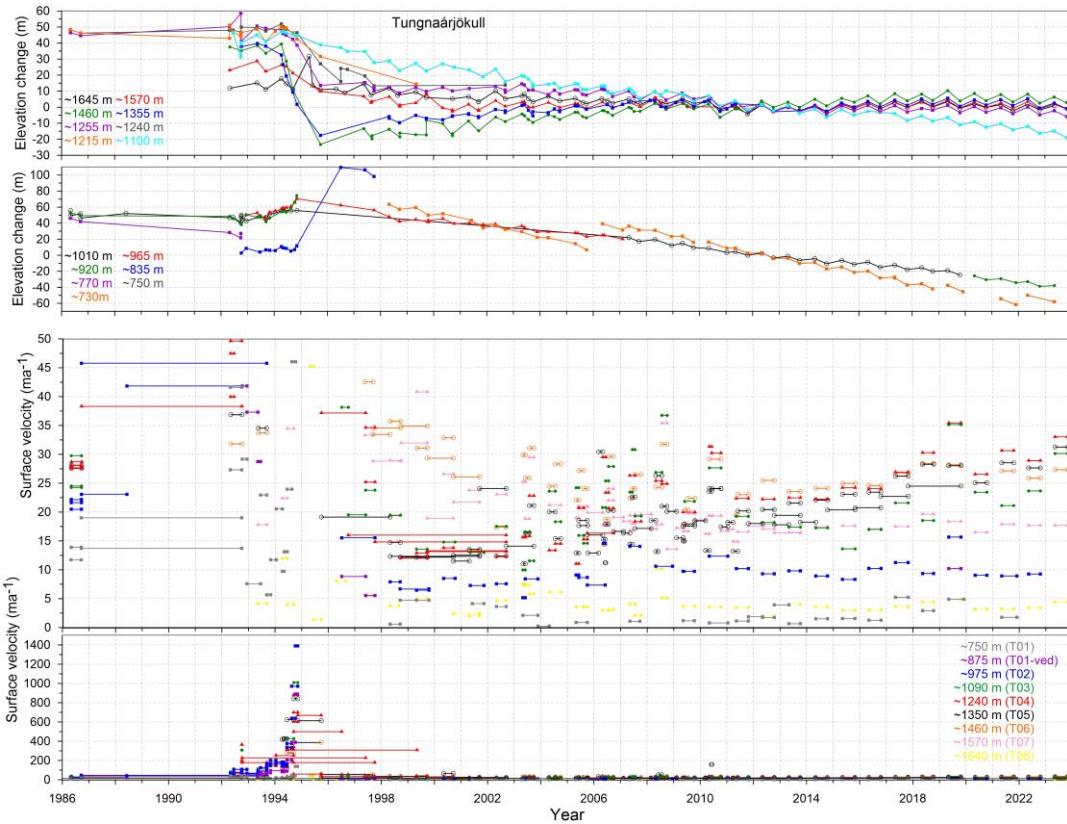
|      |      |      |       |      |       |
|------|------|------|-------|------|-------|
| 1700 | 1750 | 1    | 1,0   | 0,3  | 0,3   |
| 1650 | 1700 | 5,9  | 6,9   | 2,4  | 2,7   |
| 1600 | 1650 | 9,1  | 16,0  | 4,5  | 7,2   |
| 1550 | 1600 | 10,6 | 26,6  | 5,9  | 13,1  |
| 1500 | 1550 | 20,8 | 47,5  | 14,7 | 27,8  |
| 1450 | 1500 | 40,1 | 87,6  | 39,4 | 67,2  |
| 1400 | 1450 | 26,5 | 114,1 | 30,8 | 98,0  |
| 1350 | 1400 | 24   | 138,1 | 35,2 | 133,2 |
| 1300 | 1350 | 22,5 | 160,6 | 40,8 | 174,1 |
| 1250 | 1300 | 17,2 | 177,8 | 37,4 | 211,5 |
| 1200 | 1250 | 20,3 | 198,1 | 51,2 | 262,7 |
| 1150 | 1200 | 14,2 | 212,4 | 42,1 | 304,8 |
| 1100 | 1150 | 10,6 | 223,0 | 34,8 | 339,6 |
| 1050 | 1100 | 9,4  | 232,4 | 33,8 | 373,4 |
| 1000 | 1050 | 8,4  | 240,8 | 33,5 | 406,9 |
| 950  | 1000 | 8,5  | 249,3 | 37,2 | 444,1 |
| 900  | 950  | 7,5  | 256,8 | 34,9 | 479,0 |
| 850  | 900  | 7,9  | 264,7 | 39,3 | 518,3 |
| 800  | 850  | 6,7  | 271,3 | 35,8 | 554,1 |
| 750  | 800  | 7,5  | 278,9 | 42,7 | 596,8 |
| 700  | 750  | 9,5  | 288,3 | 56,2 | 653,0 |
| 650  | 700  | 11,1 | 299,5 | 70,2 | 723,1 |
| 600  | 650  | 6,3  | 305,7 | 41,7 | 764,9 |
| 550  | 600  | 0    | 305,8 | 0,3  | 765,1 |

**Skaftá water drainage basin**

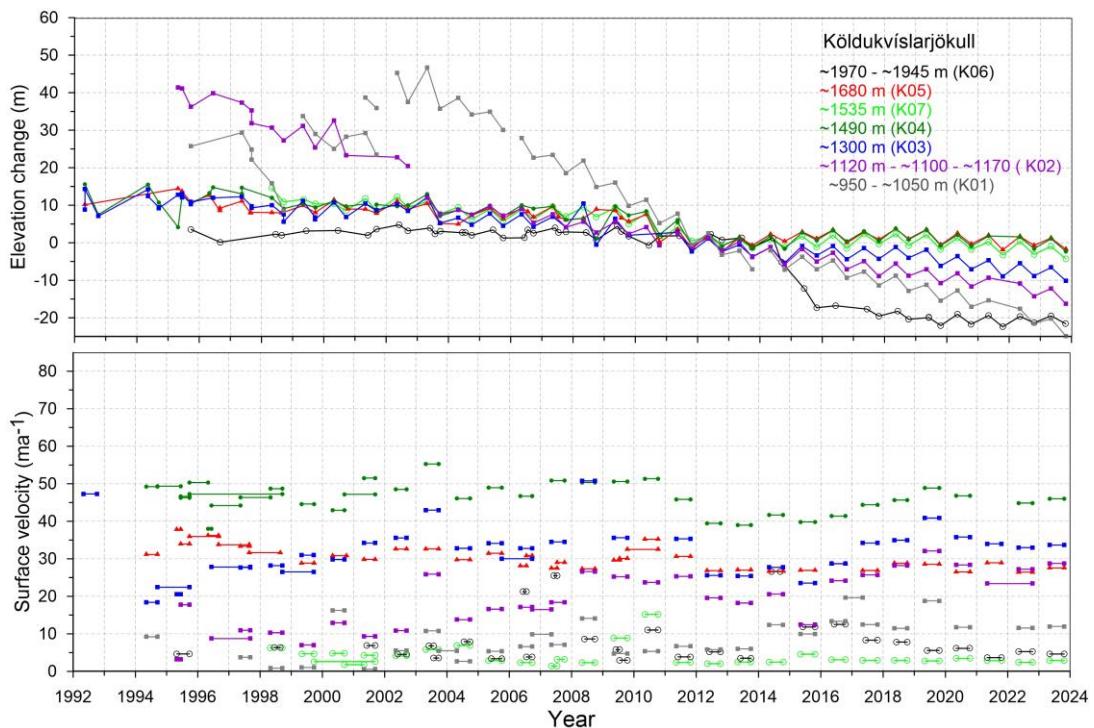
| Elevation<br>(m a. s. l.) | $\Delta S$<br>km <sup>2</sup> | $\Sigma \Delta S$<br>km <sup>2</sup> | $\Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) | $\Sigma \Delta Q_s$<br>(10 <sup>6</sup> m <sup>3</sup> ) |
|---------------------------|-------------------------------|--------------------------------------|---|--|
|---------------------------|-------------------------------|--------------------------------------|---|--|

|      |      |      |       |      |        |
|------|------|------|-------|------|--------|
| 1650 | 1700 | 2    | 2,0   | 1,2  | 1,2    |
| 1600 | 1650 | 14,9 | 16,9  | 9,0  | 10,2   |
| 1550 | 1600 | 22,9 | 39,8  | 15,7 | 25,9   |
| 1500 | 1550 | 31,9 | 71,7  | 25,7 | 51,6   |
| 1450 | 1500 | 24,6 | 96,3  | 21,6 | 73,3   |
| 1400 | 1450 | 22,4 | 118,6 | 25,1 | 98,3   |
| 1350 | 1400 | 20,4 | 139,0 | 30,2 | 128,6  |
| 1300 | 1350 | 22,1 | 161,1 | 40,6 | 169,2  |
| 1250 | 1300 | 14,8 | 175,9 | 32,5 | 201,7  |
| 1200 | 1250 | 20,2 | 196,1 | 52,1 | 253,8  |
| 1150 | 1200 | 22   | 218,0 | 64,8 | 318,7  |
| 1100 | 1150 | 23,1 | 241,1 | 75,7 | 394,4  |
| 1050 | 1100 | 21,8 | 262,9 | 79,1 | 473,5  |
| 1000 | 1050 | 24,8 | 287,8 | 99,5 | 573,0  |
| 950  | 1000 | 20   | 307,8 | 88,2 | 661,1  |
| 900  | 950  | 16,6 | 324,5 | 78,5 | 739,6  |
| 850  | 900  | 13,6 | 338,0 | 68,0 | 807,6  |
| 800  | 850  | 13,5 | 351,5 | 71,8 | 879,4  |
| 750  | 800  | 12,5 | 364,0 | 70,3 | 949,7  |
| 700  | 750  | 10,1 | 374,1 | 59,7 | 1009,4 |
| 650  | 700  | 5,5  | 379,5 | 33,9 | 1043,3 |
| 600  | 650  | 0,6  | 380,1 | 3,5  | 1046,8 |

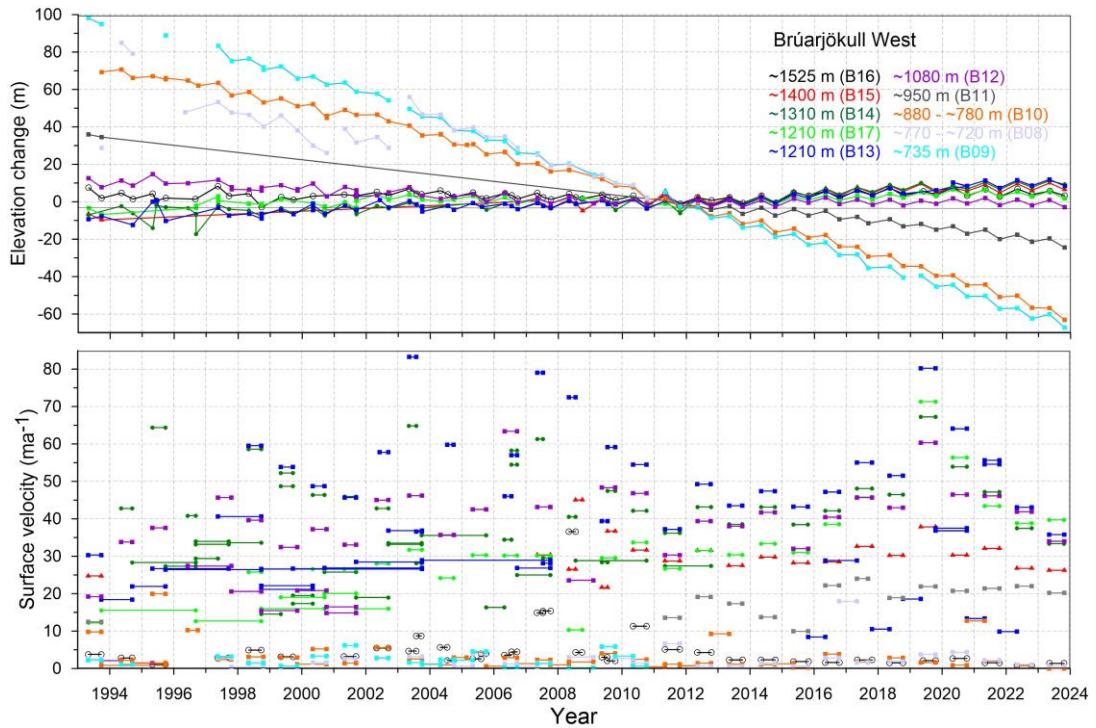
## Appendix F: Records of surface elevation change a surface velocity at mass balance survey sites on Vatnajökull.



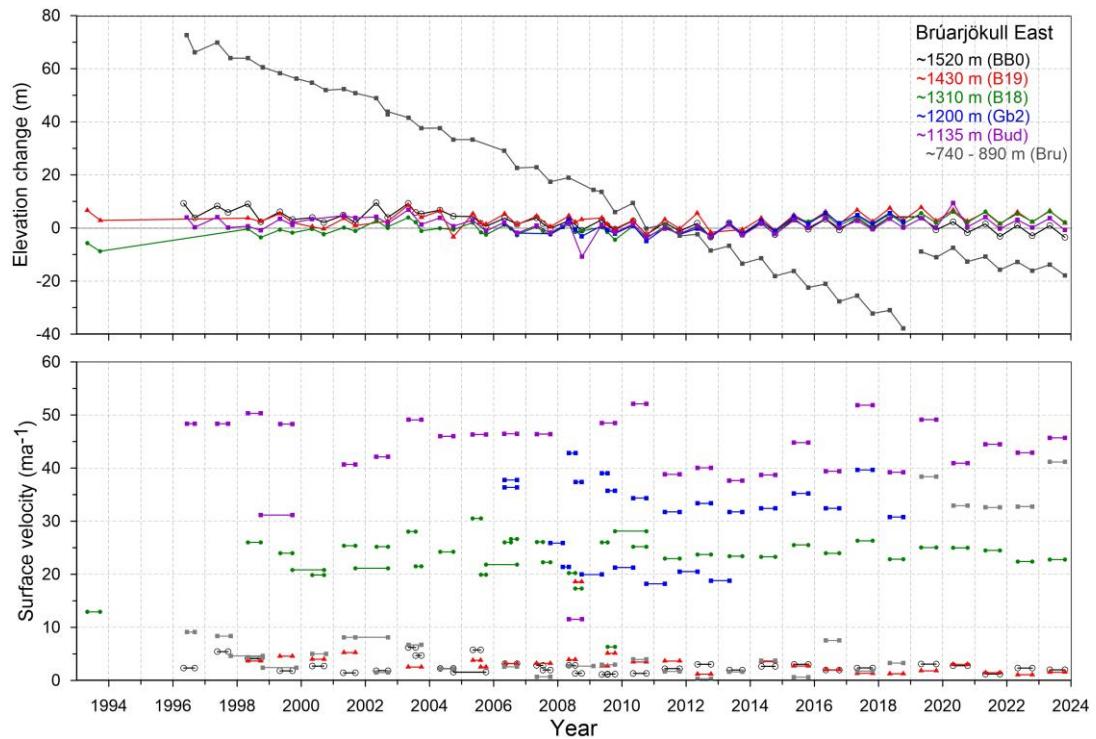
*Surface elevation change relative to summer 2012 (upper panel) and average surface velocity (lower panel) at mb sites on Tungnaárljökull in 1986 to 2023.*



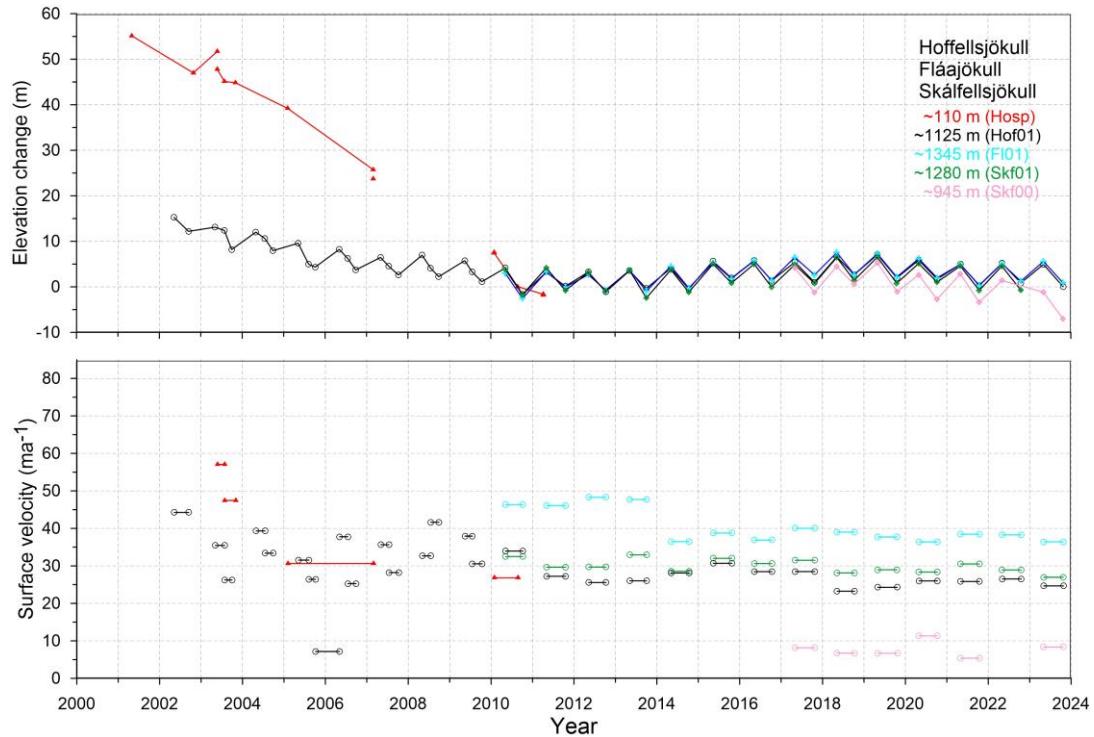
*Surface elevation change relative to summer 2011-12 (upper panel) and average surface velocity (lower panel) at mb sites on Köldukvíslarjökull in 1992 to 2023.*



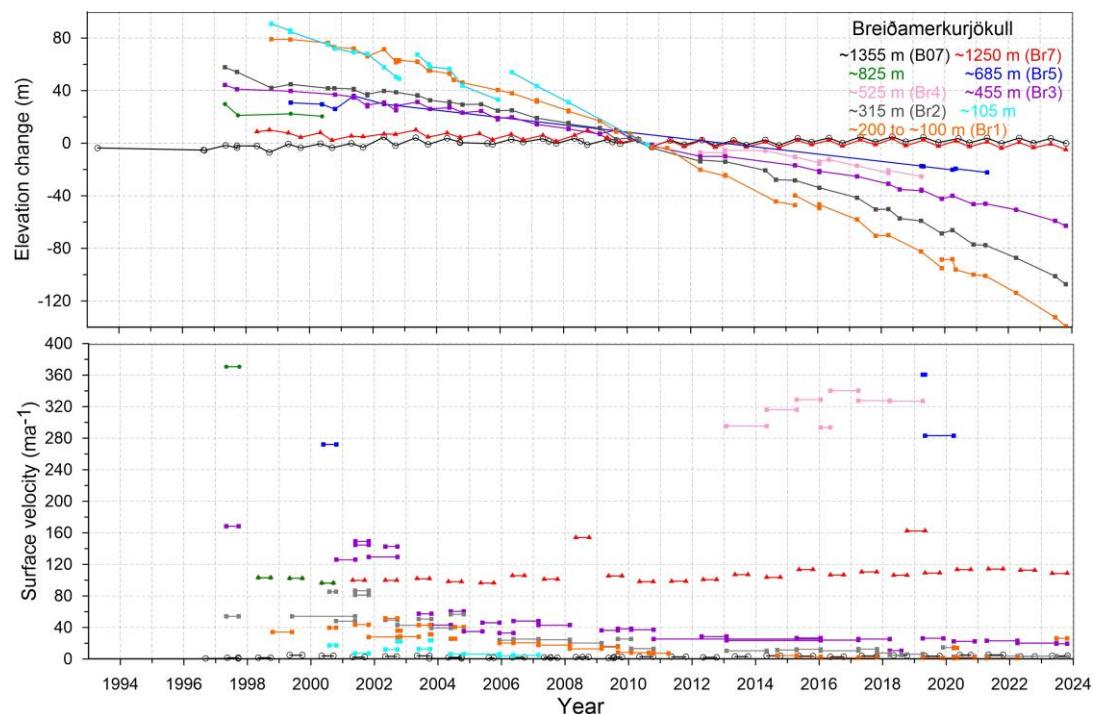
Surface elevation change relative to summer 2011 (upper panel) and average surface velocity at mb sites (lower panel) on W-Brúarjökull in 1993 to 2023.



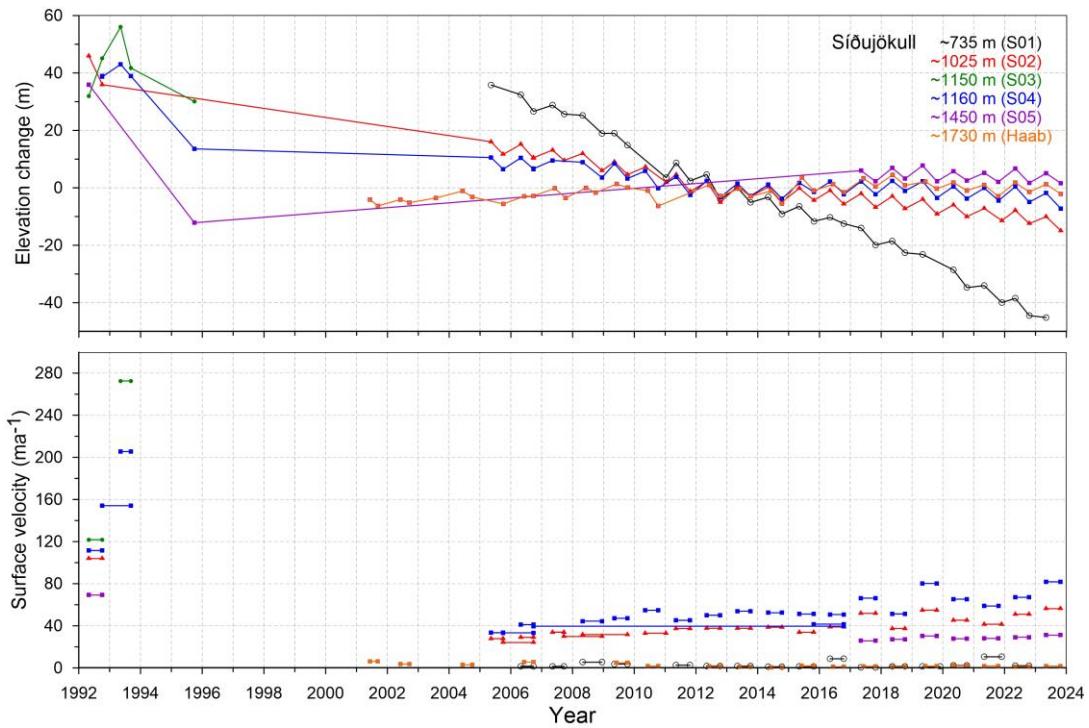
Surface elevation change relative to summer 2010 (upper panel) and average surface velocity at mb sites (lower panel) on E-Brúarjökull in 1993 to 2023.



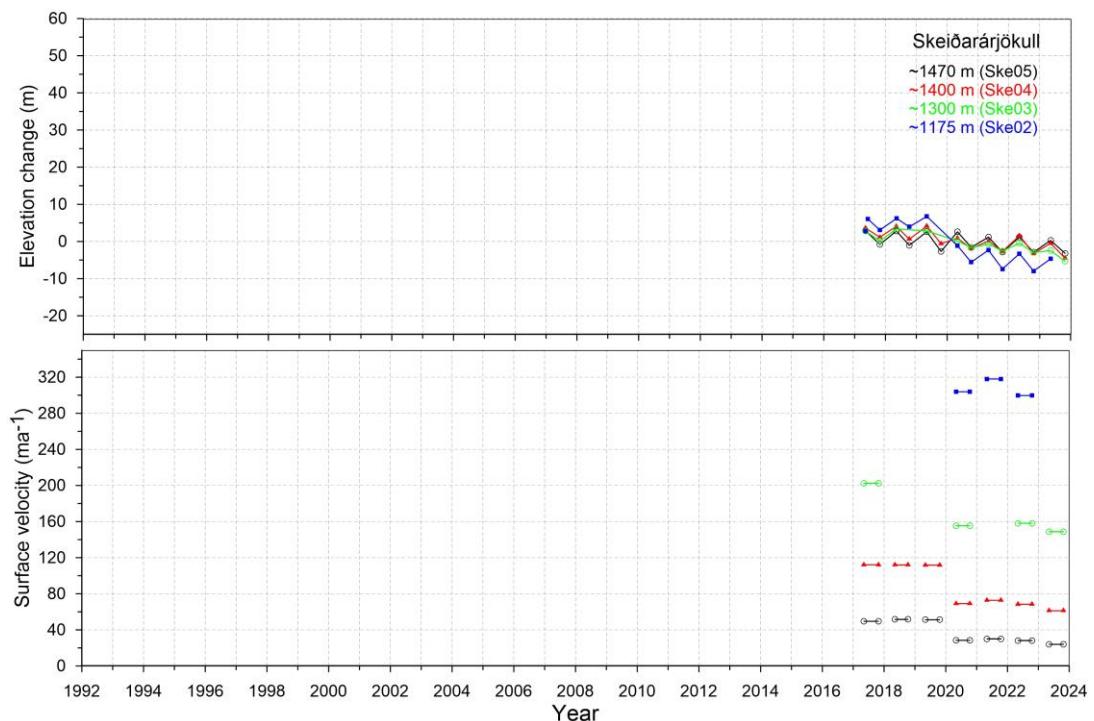
*Surface elevation change relative to summer 2010 (upper panel) and average surface velocity at mb sites (lower panel) on SE-Vatnajökull outlets in 2000 to 2023.*



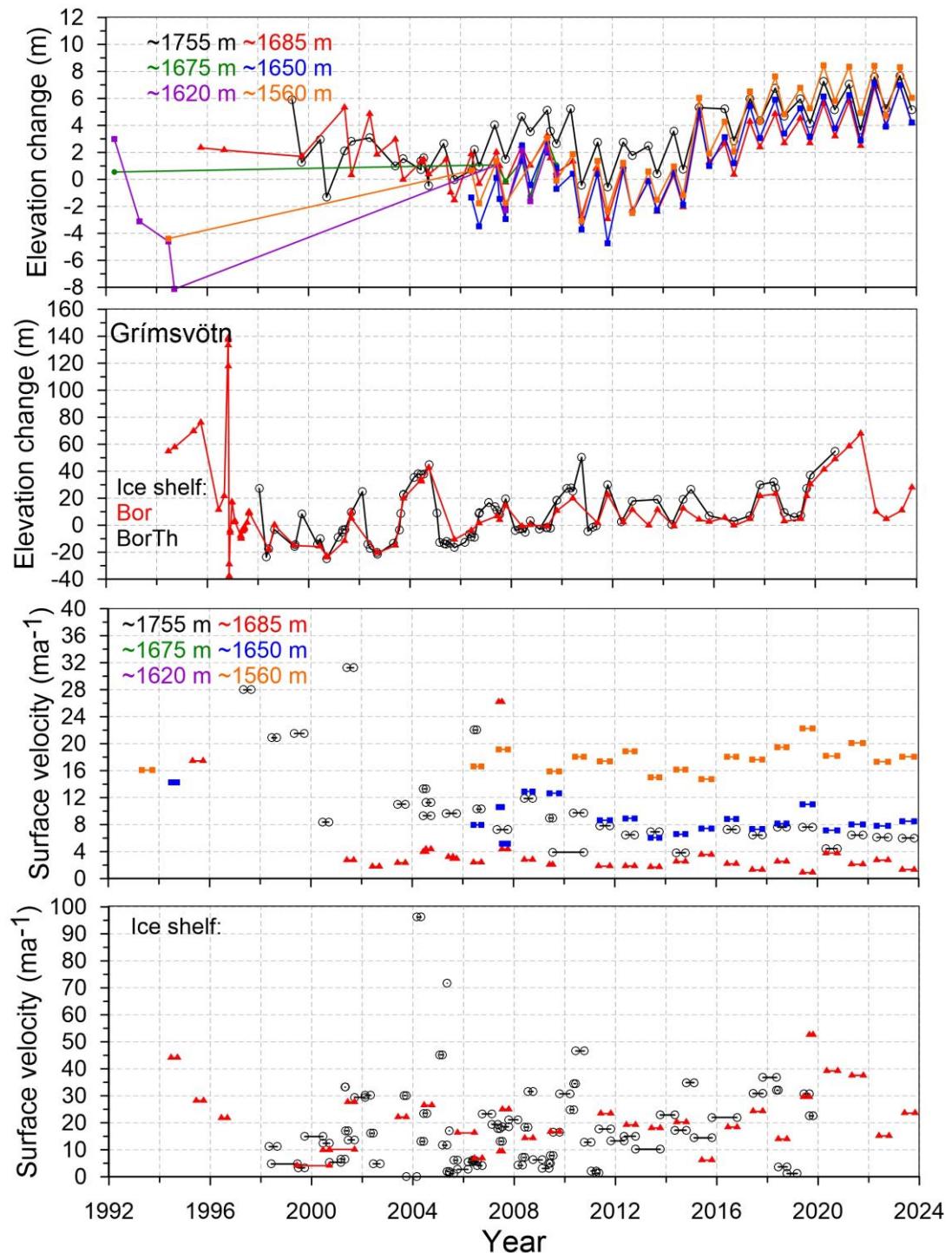
*Surface elevation change relative to summer 2010 (upper panel) and average surface velocity at mb sites (lower panel) on Breiðamerkurjökull in 1993 to 2022.*



*Surface elevation change relative to summer 2012 (upper panel) and average surface velocity at mb sites (lower panel) on Síðujökull in 1992 to 2023.*



*Surface elevation change relative to summer 2011-12 (upper panel) and average surface velocity at mb sites (lower panel) on Skeiðarárjökull in 2017 to 2023.*



Surface elevation change relative to summer 2012 (upper panels) and average surface velocity at mb sites (lower panels) in Grímsvötn ice catchment in 1993 to 2023.