



**ORKUSTOFNUN**  
Raforkudeild

# **MAPPING OF ICELAND IN SCALE 1:50,000**

**Control Surveys in Increments: 2,3,4,5**

**Gunnar Thorbergsson**  
Electric Power Division

**OS79006/ROD03**  
Reykjavík, February 1979

By Contract with  
Iceland Geodetic Survey

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ÁGRIP (SUMMARY IN ICELANDIC)

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Fyrir tveimur áratugum var meiri hluti Íslands myndaður úr lofti. Army Map Service (sem heitir nú Defense Mapping Agency, Washington, D.C.) hóf gerð korta í mælikvarða 1:50.000 með því að kortleggja Reykjanesskaga, eftir að Landmælingar Íslands höfðu mælt inn myndpunkta þar (Mynd 1). Eftir langt hlé á kortagerðinni, sem á að ná til landsins alls, hefur nú verið hafist handa á ný.

Landmælingamenn Orkustofnunar hafa víða verið við mælingar, bæði vegna kortagerðar Orkustofnunar í mælikvarða 1:20.000, og einnig við þyngdarmælingar á landinu öllu á árunum 1968-73. Það þótti sýnt að þríhyrningapunktar, fastmerki og þyngdarmælistær (með þekktum hæðum), sem Orkustofnun hafði sett og mælt inn, kæmu að góðum notum við myndpunkta-mælingar, ef hægt væri að ganga að punktunum vísum.

Samningur milli Landmælinga Íslands og Orkustofnunar var því gerður 1977 og endurnýjaður 1978. Samkvæmt honum hafa landmælingamenn Orkustofnunar mælt inn myndpunkta vegna kortagerðar í mælikvarða 1:50.000 í nyðri hluta svæðis 2, í svæðum 3 og 4 og í hlutum svæða 5,6 og 7 (Mynd 1). Þessi númer mælisvæða eru í samræmi við áætlun um myndmælingar, sem Defense Mapping Agency hefur gert og látið fylgja með loft-myndunum sjálfum.

Skýrsla þessi fjallar um mælingar Orkustofnunar í svæðum 2,3,4 og 5. Hnit og hæðir myndpunkta og merktra punkta í þeim svæðum er að finna í hnitalista (2.2 List of Coordinates). Í samræmi við áætlun um myndmælingar, hafa lýsingar af öllum þeim punktum, sem skráðir eru í hnitalista, verið skrifðar og teiknaðar aftan á loftmyndirnar, sem notaðar voru úti á mörkinni. Myndirnar með lýsingunum verða afhentar Landmælingum Íslands með skýrslu þessari.

0. ABSTRACT

Field work, by contract with Iceland Geodetic Survey, and data processing are described. List of coordinates with ground control points, identified and described on aerial photos, is given.

1. INTRODUCTION

Two decades ago most of Iceland was photographed from the air and Army Map Service (now Defense Mapping Agency, Washington, D.C.) started mapping the country in scale 1:50.000. Maps were prepared of Reykjanes-skagi in the Southwest, after Landmælingar islands (Iceland Geodetic Survey) had established ground control in that area (Fig.1). Work necessary for continuation of the mapping has now been resumed.

Surveyors of the National Energy Authority (NEA) have been in all parts of the country, partly in connection with NEA's own maps in scale 1:20,000, and partly during the Iceland Gravity Survey in 1968-73. It was realized that triangulation points, benchmarks and gravity stations (of known elevations) established by NEA should be very useful for the work at hand, provided these points could be recovered without doubt.

A contract between the Iceland Geodetic Survey and the National Energy Authority was therefore signed in 1977 and renewed in 1978, according to which NEA's surveyors have now established ground control in the north half of Increment 2, in Increments 3 and 4, and in

parts of Increments 5,6 and 7 (Fig. 1). This identification of survey areas (as Increments) agrees with a Photogrammetric Plan compiled by the Defense Mapping Agency, provided together with the photographs used.

The present report contains results of field measurements in Increments 2 (north), 3,4 and 5 (two points). Coordinates and elevations of ground control (picture points and panelled points) in these areas are given in the List of Coordinates, Section 2.2 of this report.

As specified in the Photogrammetric Plan, descriptions of all ground control points listed in the List of Coordinates are given on the photographs used during the field work. The photographs will be handed over to the Iceland Geodetic Survey at the same time as this report.

## 2. RESULTS

The results of NEA's field work in Increments 2,3,4 and 5 consist of coordinates and elevations of ground control points as given in the List of Coordinates (2.2) and of descriptions of the same points as sketched on the aerial photographs used in the field.

### 2.1 Coordinate systems

Iceland 1956 Datum (Hjörsey Datum) was established during the first order triangulation in Iceland 1955/56. The observed astronomical coordinates of triangulation point 99 Hjörsey were used as geodetic coordinates for that point and held fixed during the

following adjustment. The International spheroid was used.

Lambert's coordinates or rectangular coordinates obtained by Lambert's orthomorphic projection of the spheroid onto a cone touching the spheroid at 65° N are in general use in Iceland and have been used in all computations. The intersection of the 65° N parallel and the 18° W (central) meridian is given coordinates (500000,500000) meters and there the y-axis is directed north and the x-axis west.

UTM-coordinates are used for the final results in the List of Coordinates. The Universal Transverse Mercator is a world-wide system of projections, each covering 6° of longitude wide grid zones (between 80° S and 84°N). Iceland lies in grid zones 26° W, 27°W, and 28°W and for these three zones a zone digit (under Z) in the List of Coordinates is 6,7 and 8 respectively. The zone digit is the leftmost digit in the east-coordinate of a point.

## 2.2 List of Coordinates

A list of coordinates is given on the following eight pages. The form of the printed list is identical to the format of coordinate cards described in Appendix A, except that ground control points are given as:

HVPP horizontal-vertical picture point  
HPP horizontal picture point  
VPP vertical picture point

followed by the number of the photograph on which the point was identified and described. For panelled

points, the number of the photo on which the point was identified is given.

The southern half of Increment 2, together with HVPP-8541 in Increment 3, was controlled by the Iceland Geodetic Survey. All other picture points in Increments 2 and 3, all picture points in Increment 4, and two picture points in Increment 5, are given in the List of Coordinates.

All panelled points, that could be identified on photographs from Increment 2,3 and 4, are given in the list. These points had been panelled a short time before the aerial photography by the National Energy Authority. In Increment 5 no such points could be identified.

## HIT &amp; COORDINATES

## PICTURE POINTS IN INCREMENT 2 (NORTH)

QUADRANT	NORTH	Z EAST	ELEV.	NOTE	NAME	DESCRIPTION	DONE
	7148405.6	7535248.3	331.4		HVPP	7759	0578
	7156286.9	7553469.4	555.9		HPP	7871	0577
	7143014.6	7547317.0	277.4		HVPP	7922	0577
	7211073.7	7519324.0	462.3		HVPP	8917	0578
	7179449.0	7522497.3	559.9		HVPP	8925	0578
	7152245.9	7523572.0	512.9		VPP	8970	0578
	7185667.3	7535710.0	559.3		HPP	8971	0578
			606.3		VPP	9212	0578
			654.2		HVPP	9215	0578
			673.3		VPP	9232	0577
	7211731.1	7531723.8	553.3		VPP	11336	0578
	7213092.4	7548677.7	752.7		HVPP	11345	0578
	7201254.7	7549206.3	727.6		HVPP	11411	0578
	7141413.6	7517640.6	443.9		VPP	11468	0578
	7192504.6	7527287.8	495.1		HVPP	11477	0578
	7197250.7	7513175.2	499.3		HVPP	11935	0578
			434.8		HVPP	12011	0578

## UTM-CORDINATES

MARKED (PANELLED) POINTS IN INCREMENT 2

	WKT	ELEV.	NAME	DESCRIPTION
5163	7112966• 4	7511865• 5	AL	ALDSE
	7106070• 5	7511501• 9	RH	BORGARHOLAR
9039	7123257• 2	7530217• 2	BJF	BJARNARFELL
	7143642• 2	7534174• 2	BRF	
	7100031• 3	7515511• 7	BT	BJORNSTANGI
	7127233• 1	7536050• 2	BM	DAGMALAAS
5162	7119683• 1	7528931• 9	DMF	FELLSFJALL
	7107361• 6	7520444• 6	EF	FJALL
5170	7092384• 9	7524811• 4	FJ	GISLHOLTSFJALL
1130	7139542• 7	7543010• 8	GHE	HAILDA
60	7003291• 4	7516102• 6	HAA	ECCENTRIC CANVAS
3077	7113522• 3	7546977• 0	HEF	HESTFJALLAHNUJKUR
	7147659• 4	7549779• 4	HV2	7912 0565
	7145543• 5	7549833• 5	M	7375 0561
	7145322• 1	7548948• 4	M	7875 0561
	7147018• 2	7543990• 4	M	7875 0561
	7141446• 9	7545290• 9	M	7839 0561
	7136424• 7	7544338• 7	M	7839 0561
60	7097347• 1	7511619• 0	KA	5097 0578
9071	7093434• 6	7529543• 4	KH	7729 0561
	7132489• 2	7533483• 2	LADG	5037 0560
	7100216• 2	7511312• 1	LHD	6003 0561
5165	7109352• 1	7532041• 6	MF	5095 0560
1073	7102053• 0	7517366• 7	MH	6005 0578
	7102527• 7	7532953• 2	MHF	5093 0560
2052	7093678• 1	7539585• 8	MDF	7827 0565
1070	7103014• 7	7543061• 0	MVH	7827 0565
2052	7089540• 0	7529201• 9	SKAF	MAFTEINSTUNGA
	7106540• 0	7516245• 6	SOT	6009 L158
	7144278• 8	754218• 2	STB	5095 0560
0037	7104222• 1	7523231• 0	SV	7761 0561
1131	7103726• 3	7515142• 2	VDF	5207 12097 0578
		935• 8	STRUTUR (CAIRN)	1181
		3BV		

UTM-CORDONNATES

PICTURE POINTS IN INCREMENT 3

NUMBER	NORTH	Z	EAST	ELEV.	NOTE	NAME	DESCRIPTION	DONE
--------	-------	---	------	-------	------	------	-------------	------

7130221.5	7600634.9	891.4	VPP	6194
7156544.4	7597464.9	587.4	HVPP	7459
7173984.2	7554333.5	595.9	HVPP	7467
7173995.7	7554314.0	973.0	HVPP	6161
7188385.5	7557838.4	HPP	8161	
		HPP	8175	
		VPP	8176	
		VPP	8186	
		VPP	8194	
		VPP	8260	
		VPP	8284	
		VPP	8298	
		VPP	8306	
		VPP	8318	
		VPP	8350	
		HVPP	8355	
		VPP	8398	
		HPP	6399	
		HVPP	8403	
		VPP	8408	
		HPP	8475	
		VPP	8480	
		HVPP	8575	
		VPP	9408	
		VPP	9860	
		VPP	9878	
		VPP	9892	
		VPP	9906	
		HPP	10901	
		VPP	10954	
		VPP	10960	
		VPP	10972	
		HPP	10975	
		VPP	10976	
		HVPP	10981	
		VPP	10992	
		VPP	10996	
7070972.1	7583023.0	471.4		
7054130.9	7579119.6	850.6		
		230.4		
		120.7		

## UTM-COORDINATES

PICTURE POINTS IN INCREMENT 3

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NUMBER	NORTH	EAST	ELEV.	NAME	DESCRIPTION
7211772.1	7558351.2	571.5	VPP11214		
7213739.0	7571109.0	663.8	HVPP11449		
		534.4	HVPP12213		

=====

DONE

## UTM-COORDINATES

MARKED (PANELLED) POINTS IN INCREMENT 3

NUMBER	NORTH	Z EAST	ELEV.	NOTE	NAME	DESCRIPTION	DONE
0195	7106569.6	7557598.3	671•8	2VBM	BF	BURFELL	9201 OS65
2074	7120619.2	7560900.4	690•0	2BVM	FA	FUSSALDA	8245 OS65
2073	7123052.4	7566007.9	550•2	3BVM	FH	FOSSEHEIDI	8245 OS65
5264	7144892.7	7537147.3	652•6	3PM	FMA	FLOAMANNAALDA	9873 OS68
9199	7091541.9	7600103.3	1189.3	2BV	HB	HABARMUR (CAIRN)	10883 OS69
2069	7132889.7	7580619.7	598.2	3BVM	LH	LANGAHLID	10957 OS68
5262	7132027.8	7572520.9	709.4	3BM	LF	LAMBAFELL	8411 OS63
2065	7154115.4	7596776.0	664.5	2BM	NA	NORDLINGAALDA	6213 OS65
2016	7132786.4	7539576.2	681•2	2BVM	NB	BUDARHALS, NORDUR	9411 OS65
2070	7119078.2	7595038.6	627•2	2BVM	NT	SSV AF PORISVATNI	6203 OS65
5263	7141285.1	7583151.0	669•0	3BM	OH	DRAEFAHNUKUR	9871 OS68
2004	7097478.0	7577932.3	1220.6	1BV	RFF	(CAIRN)	10934
2071	7105846.7	7564490.9	479•3	3BVM	SSF	SYDRA SAUDAFELL	8311 OS65
2072	7111027.7	7572843.6	722•8	2BVM	VF	VALAFELL	3417 OS65
2214	7155366.4	7588818.5	684•1	4M	HELL	9403 OS65	
2205	7155692.6	7590650.1	643•2	4M	HELL	9403 OS65	
2206	7154507.7	7590464.0	634•9	4M	HELL	9403 OS65	
2210	7115438.7	7593290.2	495•6	4M	2210	9415 OS65	
2211	7116242.4	7591967.6	498.7	4M	HELL	9415 OS65	
2212	7116093.2	7590049.7	562•9	3BM	SIGALDA	9415 OS65	
2214	7117654.5	7584768.8	531•0	3BM	HRAUNEYJAFELL	9865 OS65	
2215	7119674.4	7583911.5	388.4	4BM	2215	HRAUNEYJAR	9865 OS65
2217	7120549.7	7582734.1	344.6	4M	2217	HELL	9865 OS65

HISTO-CHEMISTRIES

PICTURE POINTS IN INCREMENT 4					
NUMBER	DIRECTION	ELEV.	NOTE	NAME	DESCRIPTION
1	NORTH	7	EAST		DONE

0577	532.8	VPP	7292
0577	532.6	VPP	7290
0577	532.5	VPP	7293
0577	650.1	VPP	8732
0577	663.5	VPP	8734
0577	831.5	VPP	8690
0577	621.0	VPP	8698
0577	7104216.5	HPP	8721
0577	7104206.9	HVPP	8722
0577	7157807.7	VPP	8738
0577	7125579.7	HVPP	8751
0577	7032643.7	VPP	8784
0577	7047881.4	VPP	8849
0577	7104216.5	HPP	9691
0577	7104206.9	VPP	9696
0577	7157807.7	VPP	9732
0577	7125579.7	VPP	9732
0577	7032643.7	VPP	1070
0577	7047881.4	VPP	1100
0577	7156521.9	HPP	11105
0577	7156047.2	HVPP	11149
0577	7126066.2	HPP	11149
0577	7082910.6	HVPP	11165
0577	7056968.0	HPP	11173
0577	7057717.1	VPP	11181
0577	7049205.6	VPP	11264
0577	7057717.1	HVPP	11272
0577	7049205.6	VPP	11292
0577	7057717.1	HPP	11299

## HTM-COORDINATES

MARKED (PANELLED) POINTS IN INCREMENT 4

NUMBER	NORTH	EAST	ELEV.	NOTE	NAME	DESCRIPTION	DONE
5149	69	7120677.4	7628646.0	0	1019.7	BB	
5152	69	7120463.8	7624351.9	5	998.5	FF	ECCENTRIC PANEL
5146		7123957.3	7613704.5	5	731.5	FQ	FONTUR
5035		7034290.3	7612610.6	6	221.7	HJH	(HIGH CAIRN)
2109		7167212.1	7624593.8	8	580.2	KA	KISTUALDA
5143	69	7117911.0	7621546.0	0	989.0	KKF	ECCENTRIC CANVAS
5159		7126799.0	7628327.6	6	902.4	MS	MOSASKEGGUR
2064		7143666.3	7609875.3	3	767.7	NSF	SAUDAFELL N.
2067		7136675.4	7603528.7	7	722.3	DA	OSALDA
2039		7160293.2	7633431.9	9	1269.0	SH	(CAIRN)
0209		7111563.3	7625767.4	4	1092.0	SVEINSTINDUR	
				1	VM		8723

LAT-LONG COORDINATES  
=====

NUMBER	NORTH	Z	FAST	ELEV.	NOTE	NAME	DESCRIPTION	DONE
7264021.2	7553229.9			128.1		HVPP12131		0573
7242219.4	7549248.2			428.4		HVPP12085		0573

THIS PICTURE POINTS IN INCREMENT 5  
=====

### 3. FIELD WORK

In Increment 2 a 60 km long traverse was measured between triangulation points 2039 OK and 5006 SMS in order to locate two new triangulation points, and elevations were obtained by trigonometric levelling over distance ranging from 5.7 to 9.6 km and totalling 59 km (Fig.2). The standard error of coordinates and the gap in elevations between the known endpoints were both within 0.3 meters.

In Increment 3 triangulation point 5246 SMF is the westernmost unknown point in a network extending from Increment 4. This point had been established and approximately located during the Gravity Survey in 1968, and the new coordinates differ by 4 m from the old coordinates. The new and old elevations of the point differ by 0.1 meter.

In Increment 4 angular measurements were started in a network (including 5246 SMF) after signals had been raised in a few, mainly old triangulation points. Because of unfavourable weather in 1977 these measurements were not concluded. In 1978 a few distances were measured with Tellurometer. After adjustment the standard error in coordinates was found to be within 0.3 meters. The triangulation network is shown in Fig. 3.

Ground control measurements were possible without further triangulation and traversing due to the large number of triangulation points and benchmarks in areas where NEA has done extensive surveying.

Transportation was by helicopter or cars. During the Gravity Survey in 1968-72 and since, NEA has used helicopter to transport field workers and their equipment between stations. The number of field workers is kept small, and the field methods are suitable for helicopter use (use of Tellurometer, simultaneous observation of vertical angles, signals light enough to be transported a few at a time). Unfortunately neither 1977 nor 1978 turned out to be a good year for helicopter use.

#### 4. METHODS

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##### 4.1 Triangulation and traversing

The same field methods, recording of measurements and computer programs are used in traversing as in triangulation.

The signals used in triangulation consist of a 2 m or 3 m long vertical pole, with four or eight horizontal bars (8 mm or 10 mm in diameter) driven through bored holes in the wooden pole. From four to 24 white or red canvas strips, 20 cm wide and 80 cm long, are stretched vertically between the iron bars. A 2 meter long signal has four wings facing, say north, east, south and west, each wing having from one to three canvas strips. On a 3 meter long signal there are two wings at each of the four sides of the signal, a red wing at top and a white wing below. Four or eight steel wires and perhaps one metric ton of stones are used to fasten the pole in a vertical position. These signals are good for ranges up to 50 km.

Horizontal angles are observed by the method of rounds. Up to seven (six if the instrument site is eccentric) distant triangulation points are observed in a clockwise order around the horizon, and then after turning the tube  $180^{\circ}$  about the horizontal axis, the points are observed in a reversed order. The point observed first and last in a round is termed the reference mark or point. In one network a definite number (say 8) of rounds involving the same points (and the same reference mark) constitute one group. It may be necessary to observe two or more groups at one station. A main group should then have at least two points in common with any of the other groups. The theodolites used are of type Wild T2 or Wild T3.

Vertical angles are measured in sets, each consisting of an observation with the theodolite in the face left (FL) attitude, then two observations FR and finally one observation FL. In traversing, simultaneous observation between two manned stations is usual.

Distance measurements are made with Tellurometer, model MRA101. This means that identical instruments are set up at the two ends of the line to be measured. One instrument is used as master instrument and the other as remote instrument. The observer at the master instrument makes two fine readings (forward and reverse) at each of 10 (or 20) different frequencies, each fine reading giving the distance between the instruments apart from a multiple of 10 meters. This multiple of 10 is resolved by a set of coarse readings. During this time the field worker at the remote instrument functions as a switch-board operator. After the

observations at one station are concluded, the instruments and operators interchange their roles, and observations are made at the other station. The observations at both stations, take 15 to 20 minutes. Dry and wet bulb temperature (from psychrometer) and barometric pressure are read and recorded three times at each station.

Eccentric measurements are not recommended nor are they forbidden. In triangulation a signal is always raised above the triangulation point itself, and during the following calculations the triangulation point with its signal is the centre of adjustment. If necessary an instrument site may, however, be eccentric. This is true of any type of observation, angular observations or measurement of distance in triangulation, as well as polar measurements, and observations for determination of auxiliary points. The eccentric angle is the observed angle between the reference point and the centre of adjustment at the observation site. The eccentric distance is the distance between the instrument (theodolite, Tellurometer) and the centre of adjustment at the observation site.

#### 4.2 Polar measurements

Polar or radial measurements are much used in the ground control surveying. One surveyor is transported to the "pole", which (at the time of computation) is a point of known location and elevation. A known triangulation point, to be used as reference point, must be visible from the pole. The pole is often

situated at a triangulation point with a big cairn, and the instrument site may then have to be eccentric. Another surveyor sets up his instrument (at or near a ground control point). This instrument site must be centric, a not to serious condition, which usually reduces to a matter of definition (the surveyor drives a peg into the ground under the instrument). At the pole, the horizontal angle between the reference point and (usually) a light set up at the other instrument site (under the instrument), is observed. The vertical angles at both instrument sites are observed simultaneously after a light beacon has been set up under the theodolite at the pole, and finally the distance between the two instrument sites is measured, the Tellurometer replacing the theodolites on the tripods. Heights of instruments and light beacons must be recorded, as well as eccentric angle and eccentric distance at the pole. In case of eccentricity at the pole, the height of instrument is obtained by using the theodolite as a level in both the FL and FR attitudes.

#### 4.3 Auxiliary points

A ground control point, as located by reference to aerial photographs, is not always a suitable instrument site, or to put the matter differently, one or more auxiliary points situated a few tens of meters away from the instrument site, will call for determination of location and elevation by one of a number of special methods or combination of methods. These methods include measurement of horizontal angle, of horizontal distance by use of tape or subtense bar, levelling and stadia tacheometry.

## 5. COMPUTATIONS

Nearly all computations are done by computer, and input to the computer is on punched cards. The types of punched cards and the computer programs used will be mentioned here, but further details are given in Appendix A.

### 5.1 Punched card types

Coordinate cards with coordinates and elevations of triangulation points and other points are used by most of the programs.

Measurements cards in triangulation may contain either observed horizontal angles or observed distances.

Polar measurement cards each contain results from two field books as recorded at the pole and at the other endpoint.

Auxiliary point measurement cards contain the results of the simple measurements used for positioning of such points.

### 5.2 Computer programs

Program GTRFX is used to compute refractive index from the observations of temperature and barometric pressure.

Program GTRIANG is for the adjustment of triangulation and traverse. Up to 44 points may be adjusted in one step.

Program GTPOL is used for computation of coordinates and elevations of points positioned by polar measurements.

Program GTAUX is used for computation of coordinates and elevation of auxiliary points.

Program GTUTM123 is used to transform Lambert's coordinates and to list UTM-coordinates and elevations of picture points.

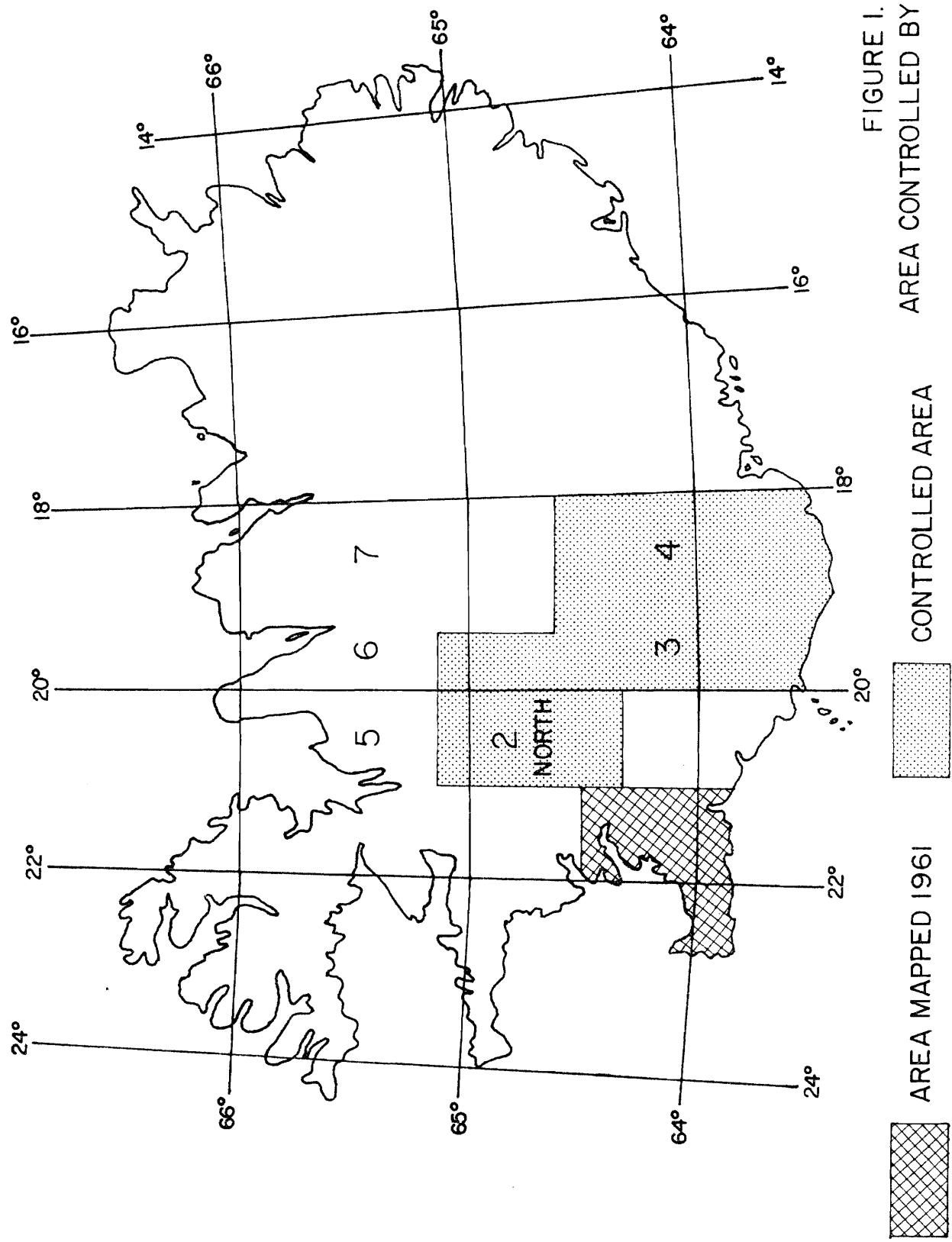


FIGURE 1.  
AREA CONTROLLED BY NEA 1977-1978

CONTROLLED AREA

AREA MAPPED 1961

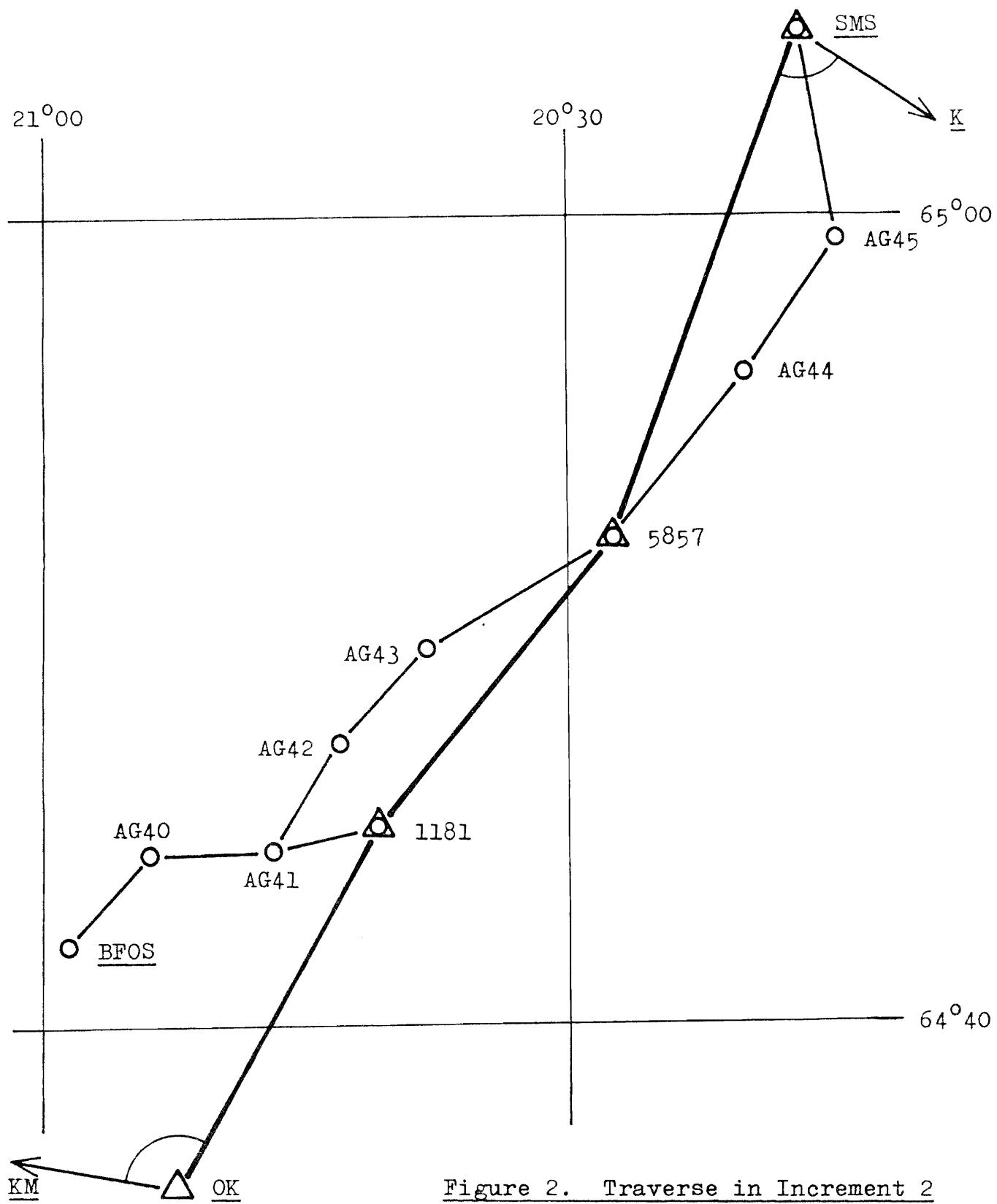


Figure 2. Traverse in Increment 2

- Traverse
- Trigonometric elevations
- △ Triangulation point
- Elevation point
- Underlined points were known.
- Scale of map 1:250,000

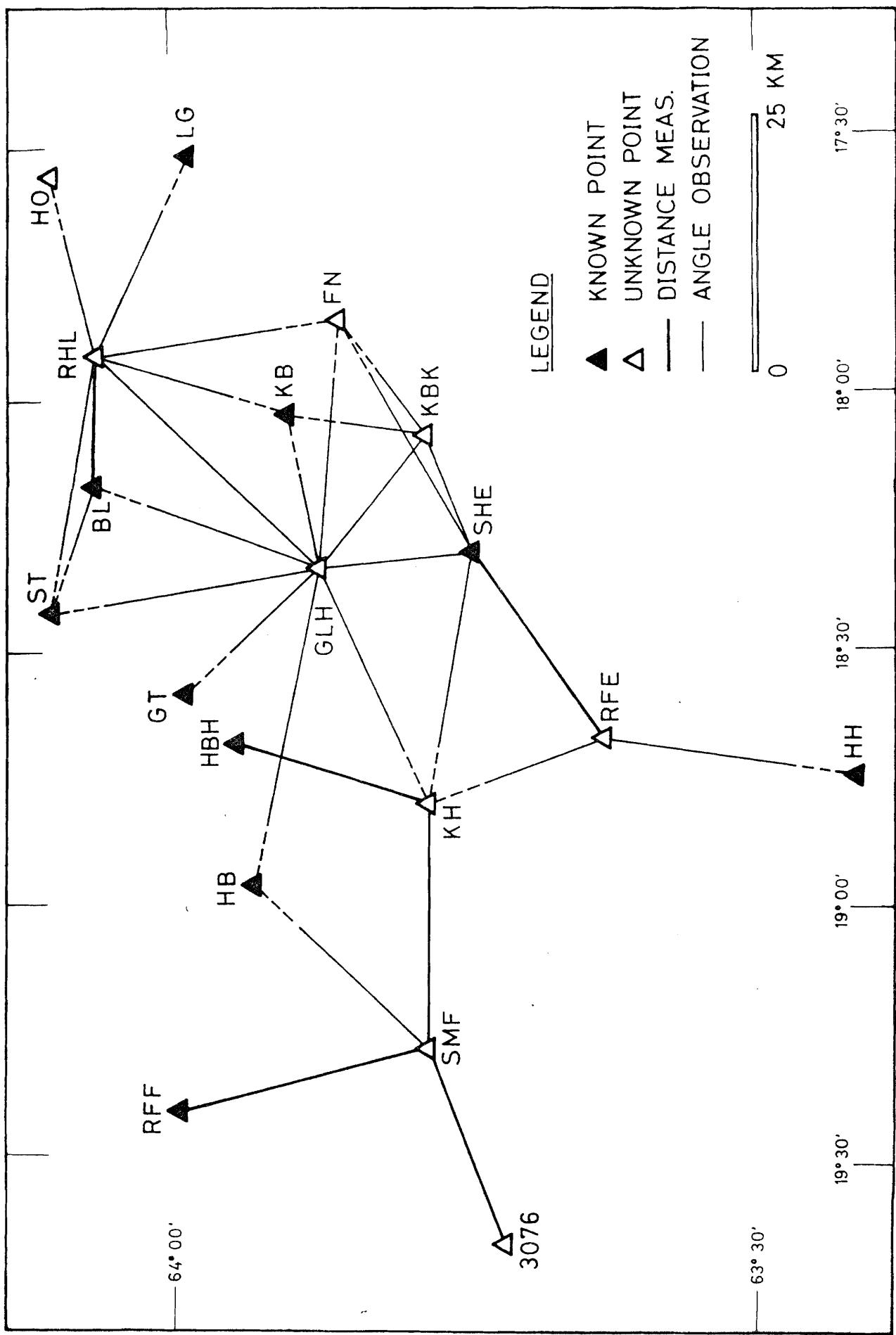


FIGURE 3. TRIANGULATION IN INCREMENTS 3 AND 4



# APPENDIX A

## CARD FORMAT AND COMPUTER PROGRAMS

Appendix A gives information necessary for understanding the following appendices. These contain data to be preserved, but are without interest to the general reader. The contents of Appendix A are as follows:

Coordinate cards

Example of eccentric instrument site

Horizontal angles in triangulation

Distances in triangulation

Polar measurement card

Auxiliary point measurement card

Input to program GTRIANG

Input to program GTPOL

Input to program GTAUXIL

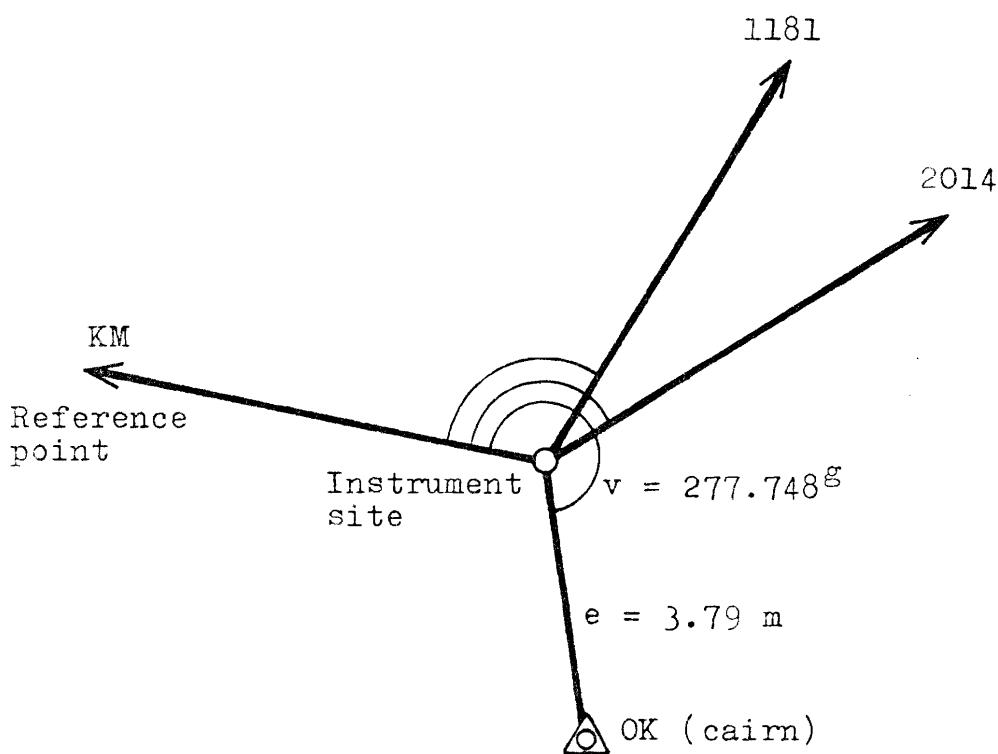
### Coordinate cards

Coordinate cards are used in the processing of triangulation and traverse, polar measurements, and positioning of auxiliary points. In all cases the same card format is used, although each computer program uses only part of the information on the card. The format of a coordinate card is as follows:

<u>Columns</u>	<u>Data</u>
01-04	Triangulation point number
06-07	Auxiliary point number
	10, 11,... Location and elevation (HVPP)
	20, 21,... Location only (HPP)
	30, 31,... Elevation only (VPP)
09-18	North coordinate (m)
19-28	West or east coordinate (m)
30-36	Elevation (m)
39	Blank or symbol for coordinate system
	* Lambert's coordinates
	U UTM-coordinates
40	Blank or order of triangulation point
41-43	Note
	B Brass plug
	R Iron tube
	H Wooden peg
	V Cairn
	M Panelled point
	F Elevation by levelling
46-49	Point name (alphabetic or numeric)
53-76	Description or local name
77-78	Surveying institution
79-80	Year of surveying or recomputation

### Example of eccentric instrument site

Due to a big cairn at triangulation point OK (Ok), the instrument site at that point was eccentric. Observation of horizontal angles were made to triangulation points KM (Kroppsmúli), 1181 (Strútur) and 2014 (Hafrafell). The distance between the eccentric site at OK and 1181 was measured with the Telluro-meter, together with simultaneous observation of vertical angles at the two instrument sites.



The eccentric angle,  $v$ , is measured clockwise from the reference point together with the other horizontal angles. The eccentric distance,  $e$ , is measured with a tape.

## Horizontal angles in triangulation

OK	
KM	
1181	1211232.
2014	1496691.
9993	35611298

The instrument site at triangulation point OK is eccentric due to a big cairn at that point. Results of the observations of horizontal angles are shown in this schema. A measurement card is punched, reading the schema linewise from left to right.

Observations are made at triangulation point OK.

The reference point is KM.

The clockwise angle from KM to 1181 is 1211232°.

The clockwise angle from KM to 2014 is 1496691°.

The reserved name 9993 indicates eccentric instrument site, when horizontal angles are observed, and that the eccentric angle is in the third quadrant. This angle is  $v = 277.748^\circ$ . The eccentric distance is  $e = 3.79$  m and the absolute values of  $e \cdot \sin(v)$  and  $e \cdot \cos(v)$  are 3561 mm and 1298 mm respectively.

With the exception of negative numbers and the numbers from 9990 to 9999, any name of four letters or digits may be used as name of a triangulation point. When observations of horizontal angles are made at a centric instrument site, up to seven points, including the reference point, may be observed. If seven points are observed, the name of the seventh point and the corresponding angle are written in the last line of the schema. This line is blank if less than seven points are observed from a centric site.

When observations of horizontal angles are made at an eccentric instrument site, up to six points may be observed. The name in the last line in the schema is then 9991, 9992, 9993, or 9994 for eccentric angles in the first, second, third, or fourth quadrant.

## Distances in triangulation

OK	
KM	
1181	1922654.
	88
117776.	
93697.	
	1
9998	35611298

The instrument site at triangulation point OK is eccentric.

Results of distance measurement from this eccentric site to the centric site at triangulation point 1181 are given in this schema, from which a measurement card is punched.

Although observations are made at both endpoints (Tellurometer), we consider OK to be the point of observations. The instrument site at the other point must be centric.

The reference point is KM.

The measured distance to triangulation point 1181, after the corrections associated with instrument constant and refractive index have been applied, is 1922654 cm.

The assumed standard error of the distance is 88 mm.

The elevation of the instrument at OK is 117776 cm.

The elevation of the instrument at 1181 is 93697 cm.

The nonzero number in the next line will cause a cord-to-arc correction to be applied to the distance.

The reserved name 9998 in the last line of the schema, is used for distance measurements at eccentric instrument sites, when the eccentric angle is in the third (9995 + 3) quadrant.

The eccentric angle (measured clockwise from the reference point) is  $v = 277.748^\circ$  and the eccentric distance is 3.79 m.

The absolute values of  $e \cdot \sin(v)$  and  $e \cdot \cos(v)$  are 3561 mm and 1298 mm respectively.

When distance is measured from a centric instrument site, the reference point name is replaced with the station name, and the name in the last line of the schema is 9995.

### Polar measurement card

This schema gives the results of polar measurements, when the pole is situated at OK, and the point to be positioned is 1181. The site of instrument is eccentric.

This data is taken from the two field books used at OK and 1181.

The schema is in one of the books.

OK is the pole.

KM is the reference point.

ll81 is the name of the point to be positioned.

The clockwise angle from KM to 1181 is 1211232<sup>cc</sup>.

The refractive index is 1.000282

The measured distance, with instrument constant added, is 1922571 cm.

The theodolite height at OK is 116 cm.

The theodolite height at 1181 is 117 cm.

The light beacon height at 1181 is 090 cm.

The light beacon height at OK is 030 cm.

The zenith angle observed at OK is 100°88'00".

The zenith angle observed at 1181 is 992871<sup>cc</sup>.

The period (column 69 of the polar measurement card) must not be omitted from the punched card.

The eccentric angle is  $277.748^{\circ}$ .

The eccentric distance is 379 cm.

The heights of the instrument and the light beacon at the pole are measured from the mark (brass plug) at the pole.

If the instrument site is centric, the fields for the

eccentric angle and eccentric distance are left blank.  
If the field for the reference point name is left blank,

the elevation, and not the coordinates, of the point, which

### Auxiliary point measurement card

8 1 6 1	
F R E M	
- 1 0 0	3 1 9 0 1 0 9 .
- 1 0 1	2 3 5 8 .
- 1 0 3	- 7 3 .
- 2 0 0	2 5 7 6 6 8 3 .
- 2 0 1	2 5 1 9 .

In this schema, data are given for the computation of the two auxiliary points 8161/10 and 8161/20 (or HVPP-8161 and HPP-8161) positioned from 8161, a centric instrument site.  
A measurement card of 80 columns is punched from this schema.

Observations are made from point 8161.

The reference point is triangulation point FREM.

The symbols -10 stand for "auxiliary point 10".

The following symbol 0 stands for "measurement of type 0", which means horizontal angle.

The clockwise angle from FREM to -10 is 3190109°.

The distance from the instrument site to -10 is 2358 cm.

The height of -10 above 8161 is -73 cm (73 cm below 8161).

The clockwise angle from FREM to -20 is 2576683°.

The distance from the instrument site to -20 is 2519 cm.

Types of auxiliary point measurements are as follows:

Type	Measured quantity or operation
0	Horizontal angle clockwise from reference point (°)
1	Horizontal distance from instrument site (cm)
2	Angle subtended by 2 m subtense bar (°)
3	Height of auxiliary point above main point (cm)
4	Zenith angle to auxiliary point (°)
5	Instrument height minus target height (cm)
6	Unreduced distance in stadia tacheometry (cm)
9	Identify auxiliary point with instrument site

In case of an eccentric instrument site, the eccentric angle is measured clockwise from reference point to main point, and eccentric distance from instrument site to main point. The last line in the schema is written as described in the case of horizontal angles in triangulation.

### Input to program GTRIANG

The input to program GTRIANG (GTRIO-GTRII) is described below for an application restricted to less than 21 known and unknown points, less than 19 unknown points, and where approximate values are known for the coordinates of unknown points.

The input cards are as follows:

AAABC

DDDDEEEE...

FFFFGGGG...

9991HHJ KKKKLLLL...

Measurement cards with horizontal angles or distances

9993

9992MM NNNN 0000 PPPP QQQQ

Heading (Col. 41-80)

9999

RRSSTTU

Coordinate cards for known (first) and unknown (last) points

A = number of names in list of names.

B = 0 for centesimal graduation, B = 1 for sexagesimal grad.

C = 0 for Lambert's projection, C = 1 for plane coordinates.

D is name of a triangulation point (list of names).

F is triangulation number of point named D.

H = number of unknown points.

J = number of computer runs (if corrections are too large).

K is name of unknown triangulation point.

M is number of following approximation cards (assume M = 0).

N is bound for correction (no more runs, if corrections are less).

O is bound for standard error of coordinate (not used).

P is expected mean standard error in direction ( $^{\circ}$ c).

Q is bound for discrepancy in resection (not used).

R = number of known points.

S = number of known or approximately known points (S=T if M=0).

T = number of points in list of coordinates (coordinate cards).

U = number of steps or adjustments (assume U = 1).

### Input to program GTPOL

ABC	D.DDD	Heading (Col. 41-80)
Coordinate cards for known points (list of coordinates)		
9999		
Measurement cards for points to go into list of coordinates		
9999		
Measurement cards for other points (the last two points		
computed are at the end of the list of coordinates).		
9999		
9999 (or new first card)		

A = 0 for centesimal graduation, A = 1 for sexagesimal grad.  
B = 0 for lambert's coordinates, B = 1 for plane coordinates.  
C = 0 for punching, C = 1 for not punching results.  
D is constant associated with refraction (use default value).

### Input to program GTAUXIL

AB	C.CCC
Coordinate cards for known points	
9999	
Measurement cards for auxiliary points	
9999	
9999 (or new first card)	

A = 0 for centesimal graduation, A = 1 for sexagesimal grad.  
B = 0 for punching, B = 1 for not punching results.  
C is constant associated with refraction (use default value).



# APPENDIX B

## COMPUTER INPUT/OUTPUT FOR INCREMENT 2

Program GTPOL (2 pages):

Trigonometric elevations between BFOS and SMS.

Approximate coordinates for triangulation point 1181.

Program GTRIANG (4 pages):

Polygon between OK (2039) and SMS (5006).

Program GTPOL (4 pages):

Polar measurements in Increment 2.

Program GTAUXIL (3 pages):

Picture points in Increment 2.

## ÞRUGRÁM GRIPUL

## CONFIRMAL CONICAL PROJECTION

365	6.500								
36	464170.30	662577.90	306.33	*ZBV	KI				OS67
2612	456813.01	268634.47	1179.70	*ZBV	K	KRAKUR			OS67
2532	453423.39	637879.20	1176.50	*ZBV	OK	OK			
2506	509365.86	606870.66	711.55	*ZBV	SMS	SUDURMANNASANUFEILL			OS67
5130	469353.71	641944.31	122.64	*ZBV	BFUS	BARNAFÖSSAR			OS67
5857	0.0	0.0	546.20		5857				
0	0.0	0.0	239.37		A341				
9999									

SSSS

SPRÖCKÄM GTPUL

CONFORMAL CONICAL PROJECTION

INPUT GIK10

600  
K K OK SMS 11315857  
9820132039500611315857  
9931 22 11815857  
0.0 0.0 0.0  
1181 K K 1211232.0 0.0 0.0 0.0  
OK 0K 1211232.0 0.0 0.0 0.0  
SMS K 5857 2100956.0 0.0 0.0 0.0  
5857 K 5857 261492.0 0.0 0.0 0.0  
OK K 1181 SMS 1801831.0 0.0 0.0 0.0  
1181 K 5857 1181149.0 6.8 11776.0 93697.0  
5857 OK 5857 1679149.0 8.0 93704.0 54750.0  
SMS 2462058.0 10.4 54753.0 71277.0  
9993  
9992 0 1.0 1.0 10.0 10.0 0.0  
9999

POLYGON BETWEEN 2039 AND 5006. JULY 1978

## INPUT GTRII

APPROXIMATE COORDINATES

4	6	1	98	484150.30	662577.90	306.33	*2BV	KY	CS67
2015	496313.01	566604.47	1179.1				*2BV	K	OS67
2029	428458.00	627579.20	1176.0				*2BV	UK	
5006	509989.86	606670.66	711.56				*2BV	SMS	
1181	474751.00	627674.00	935.6				*2BV	1161	
5577	487367.00	646624.00	246.2				*3B	5857	

POLYGRAPH BETWEEN 2035 AND 2066 • JULY 1978

## AJUSTED COORDINATES

CORRECTION	MEAN ERROR	NUMBER	Y-NORTH	X- WEST
-0.317	-0.213	0.164	0.261	1.181
-0.290	-0.403	0.167	0.273	0.857
MAX CORR	0.493	MAX ERR	0.273	ERROR IN DIRECTION 3.848 SEC 11.876 CC

## POLYLINE BETWEEN 2039 AND 5006 • JULY 1978 ADJUSTED ELEVATIONS AND DISTANCES

STATION	NUMBER	GRADS	ERKUR	NAME	D	M	SEC	NUMB	DISTANCE	NAME
2039	EGC	3•782	0•460	OK	13	3	27•4	98	25353•68	KM
	2038	14•50844	6•16	KM	122	4	10•5	1181	15222•09	1181
	1181	135•63288	-6•16	1181						
1181	EGC	-1•247	-3•141	1181						
	2039	335•63544	4•72	OK	302	4	13•8	2039	19225•65	OK
	5857	145•73218	-4•72	5857	131	9	32•3	5857	16785•06	5857
5006	2010	235•78427	-3•47	SMS	215	49	21•0	2015	22522•95	K
	5857	325•93278	3•47	5857	293	20	22•2	5857	24617•52	5857
5857	1181	345•74391	-0•93	5857	311	13	10•3	1181	16786•18	1181
	5006	125•93283	0•93	SMS	113	20	22•4	5006	24617•52	SMS
2039	EGC	3•762	0•460	OK	DISI					
	1181	6•082	9•33	1181	0•1765D-03					
1181	EGC	-1•247	-3•141	1181	DISI					
	5857	6•086	8•31	5857	0•1963D-03					
5857	5006	6•114	10•98	5857	DIST					
				SMS	0•15100-03					
MAXIMUM ERKUR	DIRECTION	8•2 CC	DISTANCE	11•0 CC	LOCATION	0•0 CC				

PROGRAM GTPOL

CONFORMAL CONICAL PROJECTION

001	6.600	474750.68	627673.79	935.80	*3BV	1181	STRUTUR	INCREMENT 2	OS78
11181		496813.01	588604.47	1179.70	*2BV	K	KRAKUR		OS67
2015		458458.00	637879.20	1177.00	*2BV	OK	OK		
2039		509989.86	606870.66	711.55	*2B	SMS	SUDURMANNASANDFELL		OS67
5006		507553.28	592993.32	784.31	*3B	GH	GRETISHED		OS67
5192		511533.83	589040.23	711.84	*3B	SVF	SVINAFELL		OS67
5193		458169.07	579355.51	574.28	*3B	FREM	FREMRI-SKUTI		OS65
5438		448317.87	584461.49	542.99	*3B	LAM	LAMBAFELL N BLAFELLS		OS65
5455		487386.71	616623.59	546.20	*3B	5857	SAUDDAFJOLL NORDUR		OS78
5857		441279.00	599913.80	459.10	*	SVH			
0		435203.00	600222.30	281.40	*	HV7			
11130		432272.67	601777.70	283.10	*	HAA			
5158		433492.24	612699.72	594.30	*	B	MSF		
0		437139.77	604343.91	291.80	*	SV	SANDVATN		
0		441559.01	616238.01	504.30	*	B	HOLL		
0		438981.96	606093.66	292.40	*		TH61		
0		0.0	0.0	0.0	0.0	AG41	339.87		

6666

## PROGRAM GTPOL

## CONFORMAL CONICAL PROJECTION

SMS	K	8917	1395411.0	305.	1602494.0	0.0	1.22	1.14	
		0.65	1010559.0	0.64	990859.0	.	0	0.0	
SMS	K	1345	922500.0	302.	575521.0	0.0	1.22	1.57	
		0.86	1017258.0	0.64	983410.0	.	0	0.0	
GH	SVF	1411	1390450.0	295.	208660.0	0.0	0.37	1.45	
		0.70	100948.0	-0.30	990588.0	.	190148	331.0	
5857	1181	2011	742152.0	305.	1285736.0	0.0	1.45	1.43	
		0.68	1006127.0	0.67	995090.0	.	0	0.0	
5857	SMS	AG46	1068586.0	302.	17094.0	0.0	1.45	1.43	
		1.43	1007895.0	1.45	992160.0	.	0	0.0	
AG46	1181	1935	2682126.0	305.	158420.0	0.0	1.43	1.49	
		0.66	1018406.0	0.67	982443.0	.	0	0.0	
5857	9212	5857	9212	0.0	0.	1065034.0	0.0	1.45	1.41
		0.68	999746.0	0.62	1001310.0	.	0	0.0	
5857	K	GT51	37172.0	301.	2446966.0	0.0	1.45	1.33	
		0.61	995799.0	0.62	1006300.0	.	0	0.0	
GT51	5857	1415	2457738.0	294.	39778.0	0.0	1.33	1.37	
		1.00	1033388.0	0.0	0.0	.	0	0.0	
5857	1181	9215	3007844.0	301.	1308361.0	0.0	1.45	1.45	
		0.69	997471.0	0.64	1003785.0	.	0	0.0	
9215	AG48	AG48	1336	0.0	410561.0	0.0	1.38	1.43	
		0.62	990241.0	0.68	1010352.0	.	0	0.0	
AG48	1181	AG47	2560151.0	288.	598376.0	0.0	1.43	1.41	
		0.35	1055264.0	0.55	945399.0	.	33124	336.0	

PROGRAM GTPOL

CONFORMAL CONICAL PROJECTION

AG47	1181	8925	2752554.0	296.	277637.0	0.0	1.22	1.43	7.34	-0.11
	0.65	968230.0	0.34	1032410.0	0.	0	0.0	0.0	473125.36	620384.59
AG41	1468	0.0	0.	925829.0	0.0	1.41	1.37	7.07	-0.80	
	0.61	992731.0	1.30	1008162.0	0.	0	0.0	0.0	452.44	1468
HOLL	MSF	8971	2043068.0	291.	614798.0	0.0	1.39	1.26	6.56	0.03
	0.69	999488.0	0.62	1001164.0	0.	0	0.0	0.0	445890.55	620600.93
HOLL	MSF	8970	2043068.0	291.	614798.0	0.0	1.39	1.26	512.42	8971
	0.69	999488.0	0.62	1001164.0	0.	0	0.0	0.0	445890.55	620600.93
SVH		AG23	0.0	0.	251736.0	0.0	1.46	1.55	6.56	0.03
	0.67	981158.0	0.56	1019484.0	0.	0	0.0	0.0	534.76	AG23
AG23	AG24	0.0	0.	253314.0	0.0	1.49	1.50	6.65	-0.01	
	0.69	981264.0	0.69	1019355.0	0.	0	0.0	0.0	610.53	AG24
AG24	9232	0.0	0.	268891.0	0.0	1.50	1.55	6.94	-0.05	
	0.68	989067.0	0.70	1011566.0	0.	0	0.0	0.0	658.03	9232
LAM	FREM	AG21	2739060.0	304.	561419.0	0.0	1.42	1.53	6.56	0.03
	0.65	999960.0	0.64	1000697.0	0.	0	0.0	0.0	448701.07	590062.41
AG21	LAM	7871	1712648.0	304.	50758.0	0.0	1.53	1.22	8.66	-0.01
	1.22	988185.0	1.53	1011871.0	0.	0	0.0	0.0	448511.40	590533.11
AG21	LAM	7872	1712648.0	304.	50758.0	0.0	1.53	1.22	8.66	-0.01
	1.22	988185.0	1.53	1011871.0	0.	0	0.0	0.0	448511.40	590533.11
TH61	SV	AG49	2110583.0	316.	349124.0	0.0	1.53	1.50	6.78	-0.04
	0.67	983877.0	0.69	1016729.0	0.	0	0.0	0.0	441891.04	608021.85
AG49	TH61	7759	1153532.0	314.	116223.0	0.0	1.50	1.37	331.37	7759
	0.68	1028517.0	0.67	972422.0	0.	0	0.0	0.0	441499.28	609114.86
HAA	MSF	GT43	3789093.0	320.	1525808.0	0.0	1.28	1.42	-0.02	-0.53
	0.70	9887895.0	0.58	1013469.0	0.	0	0.0	0.0	435099.25	616768.45

PROGRAM GTPCL

CONFORMAL CONICAL PROJECTION

GT43	HAA	1477	1856689.0	289.	1027694.0	0.0	1.43	1.42		
	HAA	0.66	1006345.0	0.70	994659.0	.	0	0.0	435346.96	627042.03
HV7	HAA	7923	2616285.0	310.	289668.0	0.0	1.16	1.42		
	HAA	0.97	1001023.0	0.41	99473.0	.	0	0.0	435534.71	597344.61
		9999							277.46	7923
									6.30	0.05
									6.97	-0.78

							SMS	SUÐURMANNASANDFELL	OS67
							5857	SAUDAFJÖLL NORDUR	OS78
01	6.	590	509989.36	606870.66	711.55	*2B			
5006		497326.71	615623.59	546.20	*38				
5367		425223.00	600222.30	281.40	*	HV7			
0		437303.91	616474.85	544.11		A346			
0		504977.62	622055.04	463.65		8917			
0		504951.93	609647.94	558.28		1345			
0		505501.90	592627.23	752.69		1411			
0		491351.66	623853.08	434.75		2011			
0		496742.78	614932.78	499.34		1935			
0		0.0	0.0	559.27		9212			
0		493647.94	592660.82	727.57		1415			
0		478653.89	606832.28	611.06		9215			
0		0.0	0.0	673.31		1336			
0		473125.36	620394.59	559.93		8925			
0		0.0	0.0	452.44		1468			
0		445360.55	620600.93	512.42		8971			
0		445990.55	620600.93	512.42		8970			
0		0.0	0.0	658.03		9232			
0		448511.40	590533.11	555.93		7871			
0		448511.40	590533.11	555.93		7872			
0		441499.28	609114.86	331.37		7759			
0		435346.96	627042.03	495.12		1477			
0		435534.71	507344.61	277.46		7923			
		999?							

## PROGRAM STATUS

8017	845	-100	0.0	-101	0.0	-103	-90.0
1345	845	-110	920471.0	-111	1595.0	-113	0.0
1411		-119	0.0	0.0	0.0	0.0	0 11 504946.C3 609633.12 558.28 1345
2011	5857	-110	2522334.0	-111	530.0	-113	0.0
1935	8346	-110	1647039.0	-111	216.0	-113	0.0
9212		-110	0.0	0.0	0.0	0.0	0 11 486943.47 614930.73 499.34 1935
1415		-119	0.0	0.0	0.0	0.0	0.0 0 30 0.0 0.0 0.0 559.27 9212
8215	5257	-100	433872.0	-101	5662.0	-103	-426.0
8205		-100	0.0	0.0	0.0	0.0	0 10 478712.35 606836.50 606.80 5215
1336		-110	0.0	0.0	0.0	0.0	0 10 473125.36 620334.59 559.53 8925
1468		-312	-355.0	0.0	0.0	0.0	0.0 0 31 0.0 0.0 0.0 673.31 1336
8071		-209	0.0	0.0	0.0	0.0	0.0 0 20 445850.55 620600.93 512.42 8571
8970		-303	51.0	0.0	0.0	0.0	0.0 0 30 0.0 0.0 0.0 512.53 8970



# APPENDIX C

## COMPUTER INPUT/OUTPUT FOR INCREMENT 3

Program GTPOL (7 pages):  
Polar measurements in Increment 3.

Program GTAUXIL (5 pages):  
Picture points in Increment 3.

		INCREMENT 3	
		61 OS69	
001	6.600	HJÖRLEIFSHOFDI	
35	323799.00	537189.60	221.70 *2BV
38	323664.63	551407.80	230.60 *2BV
38	323664.60	551407.80	230.60 *2BV
41	329673.00	563655.60	276.30 *3BV
197	396294.71	558192.57	1074.92 *2BV
2004	388585.20	5688870.10	1220.60 *1BV
2065	444290.72	547362.05	664.50 *2B
2066	441872.96	563004.55	867.50 *2BV
2067	426545.08	541439.57	722.30 *3B
2072	402366.58	573314.94	722.80 *2BV
2213	411330.38	557855.66	540.20 *3B
2214	408426.13	561084.65	531.00 *3B
3058	381355.40	594345.00	499.30 *2BV
3076	0.0	0.0	574.80 BV
5140	393848.71	550177.48	842.05 *3H
5155	465557.52	573237.58	707.90 *3B
5160	436212.94	586973.36	484.35 *3B
5183	489107.65	570007.63	729.46 *3R
5185	501663.71	574318.70	665.04 *3R
5187	509863.05	569380.00	551.17 *3B
5246	364931.10	563016.72	948.00 * B
5262	423367.53	572644.08	709.45 *3B
5263	431915.19	561593.13	660.00 *3B
5264	435528.85	557419.75	652.56 *3R
5265	435473.05	545581.26	677.40 *3B
5458	458169.07	579355.51	574.28 *3B
0	0.0	0.0	641.20 HVER
0	0.0	0.0	*H3
0	0.0	0.0	*X2
0	0.0	0.0	287.76 FM1
0	0.0	0.0	320.21 *KT
0	0.0	0.0	233.07 FM5
0	0.0	0.0	591.12 *279
0	0.0	0.0	573.35 *264
0	0.0	0.0	1023.40 3298
9999			GRAVITY STATION OS68

## PROGRAM GTPOL

## CONFOMAL CONICAL PROJECTION

3076	AG36	0.0	0.	449275.0	0.0	1.33	1.39				
9999	0.64	1045178.0	1.31	955324.0	.	0	0.0	0.0	258.31	AG36	6.86 -0.10
ARN	DNF	AG55	1547796.0	296.	773230.0	0.0	1.24	1.55			
		0.69	1001064.0	0.46	999757.0	.	240143	299.0	505566.88	580992.09	656.83 AG55
AG55	ARN	1449	1193967.0	297.	274375.0	0.0	1.55	1.49	503723.36	583023.77	683.76 1449
		0.65	994114.0	0.69	1006588.0	.	0	0.0			8.80 -0.33
THV	ARN	AG39	3706079.0	287.	368375.0	0.0	1.25	1.45	506191.46	569675.98	526.00 AG39
		0.64	1004646.0	0.63	995983.0	.	0	0.0			8.14 -0.42
AG39	THV	2213	2221734.0	287.	121854.0	0.0	1.45	1.34	505083.29	570182.52	534.98 2213
		0.62	995820.0	0.64	1005131.0	.	0	0.0			9.78 -0.09
HVER		AG22	0.0	0.	72009.0	0.0	1.10	1.50	0.0	0.0	639.94 AG22
		0.57	1001604.0	0.27	999990.0	.	0	0.0			4.15 0.03
AG22		8284	0.0	0.	182862.0	0.0	1.50	1.40	0.0	0.0	6.60 0.00
		0.93	1007481.0	0.57	993160.0	.	0	0.0			
DNF	ARN	AG54	2796625.0	295.	1317950.0	0.0	1.42	1.42	481130.25	580497.17	757.77 AG54
		0.64	999226.0	1.33	1001928.0	.	0	0.0			6.63 -0.09
DNF	DNF	AG54	2048400.0	295.	209841.0	0.0	1.33	1.47	479991.67	582257.33	847.23 AG53
		0.65	973155.0	0.66	1027490.0	.	0	0.0			7.23 -0.06
AG53	DNF	8175	2509645.0	296.	242504.0	0.0	1.47	1.37	480379.03	584645.72	688.07 8175
		0.58	1042184.0	0.65	958515.0	.	0	0.0			8.96 -0.28
AG53	DNF	8176	2509645.0	296.	242504.0	0.0	1.47	1.37	480379.03	584645.72	688.07 8176
		0.58	1042184.0	0.65	958515.0	.	0	0.0			8.96 -0.28
FREM	SKUT	8161	3004368.0	304.	1240603.0	0.0	1.16	1.50	466141.97	588850.62	974.30 8161
		0.72	979992.0	0.62	1021075.0	.	0	0.0			6.32 0.85
FREM		8260	0.0	0.	423062.0	0.0	1.30	1.69	0.0	0.0	495.99 8260
		2.07	1011852.0	0.58	988573.0	.	0	0.0			6.94 -0.12

## PROGRAM GTPUL

## CONFORMAL CONICAL PROJECTION

SKUT	FREM	8399	3118040.0	299.	690601.0	0.0	1.49	1.35
		0.63	1004891.0	0.57	995834.0	.	0	0.0
SKUT	FREM	8398	3118040.0	299.	690601.0	0.0	1.49	1.35
		0.63	1004891.0	0.57	995834.0	.	0	0.0
*H3		8186	0.0	0.	0.0	0.0	0.0	0.0
		99.99	42326.0	99.99	42250.0	.	0	0.0
NA	KU	7467	2336172.0	0.	259583.0	0.0	1.57	1.42
		1.41	1016452.0	2.00	983853.0	.	0	0.0
RF	FMA	AG51	1526962.0	298.	654794.0	0.0	0.94	1.47
		0.68	1009440.0	0.39	991269.0	.	0	0.0
AG51	RF	8403	2501699.0	0.	127788.0	0.0	1.47	1.32
		0.62	1051538.0	0.67	949318.0	.	0	0.0
AG51	AG52	9878	0.0	0.	728845.0	0.0	1.47	1.27
		1.51	987937.0	0.53	1012826.0	.	0	0.0
AG52	AG50	8298	0.0	0.	480134.0	0.0	1.69	1.45
		0.67	990168.0	0.99	1010440.0	.	0	0.0
BUF	AG50	9408	0.0	0.	261326.0	0.0	1.43	1.33
		0.62	1021767.0	0.57	978528.0	.	0	0.0
FMA	OH	0.94	1039644.0	1.50	960480.0	.	1.50	1.50
		1.49	1000574.0	0.63	448308.0	0.0	1.50	1.32
LF		0.97	1000574.0	0.63	1000033.0	.	0	0.0

PROGRAM GTPOL

CONFORMAL CONICAL PROJECTION

## PROGRAM GTPOL

## CONFORMAL CONICAL PROJECTION

AG	8350	0.0	0.	556184.0	0.0	1.02 1.35	0.0	0.0	730.14	8350	7.87 -0.78	
3298	0.64	1001585.0	0.50	999113.0	.	0 0	0.0	0.0	0.0	0.0	0.0	
SMF	6194	0.0	0.	98862.0	0.0	0.59 1.42	0.0	0.0	0.0	891.38	6194	
M4	0.0	0.0	0.59	915313.0	.	0 0	0.0	0.0	0.0	0.0	0.0	
M4	0.63	1043585.0	0.24	554572.0	0.0	0.19 1.39	0.0	0.0	0.0	570.10	M4	
M4	M5	0.0	0.	584104.0	0.0	1.44 1.51	0.0	0.0	0.0	694.53	M5	
M4	0.62	986789.0	0.65	1013918.0	.	0 0	0.0	0.0	0.0	7.04	-0.30	
M4	M3	0.0	0.	141424.0	0.0	1.45 1.53	0.0	0.0	0.0	602.51	M3	
M3	0.68	985826.0	0.62	1015072.0	.	0 0	0.0	0.0	0.0	7.88	-0.05	
M3	M2	0.0	0.	538416.0	0.0	1.53 1.23	0.0	0.0	0.0	667.57	M2	
M2	0.52	992666.0	0.62	1008005.0	.	0 0	0.0	0.0	0.0	6.99	-0.23	
M2	M1	0.0	0.	405915.0	0.0	1.23 1.52	0.0	0.0	0.0	594.60	M1	
M1	0.62	1011688.0	0.52	988921.0	.	0 0	0.0	0.0	0.0	6.90	-0.10	
M1	0.972	0.0	0.	0.	0.0	0.0 0.0	0.0	0.0	0.0	617.23	0972	
SEL	99.99	0.0	99.99	2243.0	.	0 0	0.0	0.0	0.0	0.0	0.0	
SEL	8318	0.0	0.	1495622.0	0.0	0.98 2.51	0.0	0.0	0.0	682.96	8318	
SEL	1.75	992804.0	0.34	1008565.0	.	0 0	0.0	0.0	0.0	0.0	0.0	
SEL	8575	961037.0	286.	1498460.0	0.0	0.98 1.30	0.0	0.0	0.0	367212.68	589380.81	
SMF	0.71	1001742.0	0.34	999608.0	•	363881 351.0	0.0	0.0	0.0	473.84	8575	
SMF	RFF	9906	985472.0	298.	319708.0	0.0	0.19 1.40	0.0	0.0	0.0	6.80 -0.91	
SMF	RFF	0.68	1070700.0	-0.01	929716.0	.	6398 266.0	0.0	0.0	0.0	5.71 0.18	
M5	M5	972217.0	298.	922314.0	0.0	0.19 1.45	0.0	0.0	0.0	554170.75	694.55	
M5	SMF	0.62	1017855.0	-0.50	983027.0	.	6398 266.0	0.0	0.0	0.0	367531.91	554558.08
M5	G74	881044.0	0.	85558.0	0.0	1.51 1.50	0.0	0.0	0.0	368289.11	600.76	
M5	G74	1069581.0	0.0	0.0	•	0 0	0.0	0.0	0.0	GT4	6.61 -0.03	

## PROGRAM GTPOL

## CONFORMAL CONICAL PROJECTION

M5	SMF	0.889	2260532.0	300.	296192.0	0.0	1.51	1.37	
	RFF	0.60	1019825.0	0.67	980782.0	.	0	0.0	367167.84
SMF	GT3	2573561.0	299.	243802.0	0.0	1.49	1.40	551232.29	
		0.62	1093873.0	0.79	906719.0	.	0	0.0	603.84
GT3	SMF	0.975	1828691.0	304.	130673.0	0.0	1.46	1.40	0.889
		0.59	1063477.0	0.66	937418.0	.	0	0.0	6.92
GT3	SMF	0.976	1828691.0	304.	130673.0	0.0	1.46	1.40	-0.06
		0.59	1063477.0	0.66	937418.0	.	0	0.0	-0.01
AG36	GT37	0.0	0.	716376.0	0.0	1.39	1.42	0.975	
		0.60	1C13C08.0	0.64	987753.0	.	0	0.0	6.85
AG36	GT38	0.0	0.	441839.0	0.0	1.39	1.34	0.976	
		0.56	1018647.0	0.67	982002.0	.	0	0.0	-0.01
GT38	AG36	1006	0.0	0.	262582.0	0.0	1.13	1.55	0.0
		0.69	1002669.0	0.38	997918.0	.	0	0.0	0.0
AG36	GT39	0.0	0.	422646.0	0.0	1.39	1.36	0.0	
		0.60	1009023.0	0.67	991599.0	.	0	0.0	0.0
AG36	GT40	0.0	0.	455510.0	0.0	1.39	1.46	0.0	
		0.64	1005744.0	0.67	994922.0	.	0	0.0	0.0
GT40	8480	0.0	0.	98841.0	0.0	1.46	1.64	0.0	
	0.78	1002043.0	0.64	999198.0	.	0	0.0	0.0	219.57
PEY	0028	0.0	0.	988508.0	0.0	1.18	1.05	6T39	
		0.57	977616.0	0.38	1023792.0	.	0	0.0	7.42
GT42	PEY	0.981	2785476.0	290.	96185.0	0.0	1.06	1.32	-0.29
		0.0	0.0	1.06	988508.0	.	0	0.0	0.0
PEY	0038	8475	2029868.0	312.	1338196.0	0.0	1.18	1.17	0.981
		0.55	1012476.0	0.37	988732.0	.	0	0.0	6.69
GT42	PEY	336144.39	575367.23	26.67	569726.10	850.81	8475	26.67	-0.32

PROGRAM GTPOL

CONFORMAL CONICAL PROJECTION

PEY	1214	0.0	0.	763613.0	0.0	1.18	1.29		
	0.52	975752.0	0.38	1025009.0	.	0	0.0	0.0	0.0
PEY	3038								
	0899	3295966.0	296.	1350508.0	0.0	1.18	1.13		
	0.57	972480.0	0.37	1028767.0	.	1205461249.0		337837.90	552894.61
REY	HH								
	0901	2613762.0	324.	527156.0	0.0	1.56	1.50		
	0.68	1025658.0	0.67	974995.0	.	59469	870.0	327973.40	554455.84
	9999							20.92	0.901

## PROGRAM STATUSKILL

01	6.500	458169.07	579355.51	574.28	*38	FREM	FREMRI-SKUTI	DS65
5158	465557.52	573237.58	707.90	*38	SKUT	INNRI-SKUTI	DS65	
5155	444200.72	547262.05	664.50	*28	NA	NORDLINGAALDA	R65	
2955	426545.08	541439.57	722.30	*38	CA	OSALDA	R65	
2967	393349.71	550177.48	842.05	*3H	TF	TJORFAFELL	MS69	
5149	323564.60	551407.80	230.60	*2BV	REY	REYNISFJALL	MS69	
38	363023.17	564492.45	591.04	GT3				
0	367531.91	554170.75	694.55	M5				
0	344536.77	570420.60	868.49	GT42				
0	503723.36	583023.77	633.76	1449				
0	505022.29	570182.52	534.98	2213				
0	0.0	0.0	619.24	8284				
0	480379.02	584645.72	638.07	8175				
0	430379.03	584645.72	638.07	8176				
0	466141.07	589350.62	974.30	8161				
0	0.0	0.0	495.99	8260				
0	460248.41	563821.95	658.81	8399				
0	460248.41	563821.95	658.81	8398				
0	0.0	0.0	422.50	8186				
0	446746.55	546524.21	598.42	7467				
0	443553.00	570312.43	671.26	8403				
0	0.0	0.0	927.03	9878				
0	0.0	0.0	605.94	8298				
0	0.0	0.0	564.68	9408				
0	0.0	0.0	593.41	0954				
0	0.0	0.0	707.47	8403				
0	0.0	0.0	482.69	8194				
0	419957.44	544652.40	598.44	7459				
0	0.0	0.0	287.59	83C6				
0	0.0	0.0	319.79	0960				
0	0.0	0.0	503.74	9892				
0	0.0	0.0	230.40	0992				
0	470230.74	571764.85	615.83	8755				
0	391903.56	550979.99	590.88	9860				
0	0.0	0.0	572.47	0879				
0	0.0	0.0	730.14	8350				
0	0.0	0.0	891.38	6194				
0	0.0	0.0	617.23	0972				
0	0.0	0.0	682.96	8318				

0	367212.60	580380.81	473.84	8575
0	365762.05	559949.69	593.75	9906
0	367167.94	551232.29	603.84	0839
0	361919.92	564985.93	461.94	0975
0	361819.92	564986.03	461.94	0976
0	0.0	0.0	120.66	1006
0	0.0	0.0	217.20	8480
0	345202.26	569726.10	850.81	0981
0	336144.39	575367.23	26.67	8475
0	0.0	0.0	571.51	1214
0	337237.90	552894.61	873.08	0399
0	327073.40	554455.84	20.62	0901
9999				
1449	-1119	0.0	0.0	0.0
		0.0	0.0	0 11 503723.36 583023.77
2213	-1110	0.0	-1111	0.0
		0.0	-1113	-60.0
3234	-309	0.0	0.0	0.0
		0.0	0.0	0 11 0.0
3175	-299	0.0	0.0	0.0
		0.0	0.0	0 30 0.0
3176	-309	-165.0	0.0	0.0
		0.0	0.0	0 20 480379.03 584645.72
3141	EQCM	-100 3190109.0	-101 2358.0	-73.0
		-200 2576633.0	-201 2519.0	0.0
3260	-309	0.0	0.0	0.0
		0.0	0.0	0 10 466154.77 588830.82
3377 SKUT	-200 3792653.0	-204 1075464.0	-205 0.0	-15.0
		-206 5730.0	0.0	0 20 460278.00 568870.07
				688.07 8176
				973.57 8161
				0 20 466167.14 588849.73 0.0 8161
				0.0 0.0 0.0 0.0 495.99 8260



## PROGRAM STATUS

9992	-319	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	503.74	9892
9992	-319	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	230.40	0992
9355	-179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	615.63	8355
9960	-309	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	400880.74	571764.85
9370 TF	-110	0.0	-111	347.0	-113	0.0	0.0	0.0	0.0	0.0	590.88	9860
9350	-309	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	730.14	8350
6194	-319	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	891.38	6194
9972	-319	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	617.23	0972
9313	-309	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	682.96	8318
9575	-179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	367212.68	589380.81
9975 GR3	-210	3153279.0	-211	5935.0	0.0	0.0	0.0	0.0	0.0	0.0	473.84	8575
9976	-313	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	471.43	0976
9996	-309	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	365762.05	559949.68

## MEMORY STATUS

0999 M5	-110	1000833.0	-111	422.0	0.0	0 11 367172.03 551231.77	0.0 0.839
1006	-319	0.0	0.0	0.0	0.0	0 31 0.0	0.0 120.66 1036
2430	-399	0.0	0.0	0.0	0.0	0 30 0.0	0.0 217.2C 8430
0031 3T42	-110	1042759.0	-111	600.0	-113	0.0 0 11 345206.86 569729.95	850.81 0931
3475	-209	0.0	0.0	0.0	0.0	0 20 336144.39 575367.23	26.67 8475
1214	-319	0.0	0.0	0.0	0.0	0 31 0.0	0.0 571.51 1214
0899	-119	0.0	0.0	0.0	0.0	0 11 337837.90 552394.61	873.08 0899
0901 REV	-110	3211446.0	-211	630.0	0.0	0 21 327975.16 554449.79	0.0 0.901
9999				0.0			



# APPENDIX D

## COMPUTER INPUT/OUTPUT IN INCREMENT 4

Program GTRIANG (5 pages):

Triangulation net Hverfisfljöt 1978  
(Triangulation in Increments 3 and 4).

Program GTPOL (5 pages):

Polar measurements in Increment 4.

Program GTAUXIL (4 pages):

Picture points in Increment 4.

	2116	SI	BL	RFF	ST	LG	HE	KH	FN	SHT	RFF	HH	HU	RHL	GLF	SMF	KH	KEK	VU	00493076
BBH	211623023041003	235199	26	24	27	30	35523753275631524650305235	0	493076											
5234	9961	63	RFF	RHL	ULH	SMF	KH	KBK	493000.0	SHE	952534.2	RH	1664558.0	ST	2380834.9				0.0	
	FN	154736.3	KBK						FN	104530.3			0.0						0.0	
	CLH	254536.2	KB	1203020.2						1205300.8	SLH	1481233.5	BL	1953554.0	SI	2035237.6				
	LG	361920.6	FN	951413.7	KB					1850205.9	KBK	1930241.8		0.0	9993	2989252.0				
	RFE	945636.7	GLH	1184404.7	FN					1050237.4	NHL	1584428.9	KB	1931510.0	9993	3548124.6				
	KB	361420.0	ST	712302.0	ST					1584428.9		0.0	0.0	9993	3548124.6					
	SI	1050237.4	BL	1350349.4	RHL							0.0	0.0							
	SLH	701156.5	HH	2093629.5	J.0						J.0	J.0	J.0							
	KFE	KG	574315.3	RH	1042244.0						0.0	0.0	0.0	0.0	9991	267264.7				
	RFF	3045196.0	RHL	1634214.4	0.0						0.0	0.0	0.0	0.0	9994	323110.4				
	ST	3076	2045196.0	RFF	2436670.0						94944.0	94944.0	122185.0		0.1	9995	0.0			
	SMF	SMF	SMF	SMF	SMF						94944.0	94944.0	76182.0		0.1	9995	0.0			
	BL	BL	BL	BL	BL						63114.0	63114.0	94921.0		0.1	9995	0.0			
	KR	KR	KR	KR	KR						73134.0	73134.0	74583.0		0.1	9995	0.0			
	KH	KH	KH	KH	KH						73134.0	73134.0	34330.0		0.1	9998	88420.9			
	SHE	SHE	SHE	SHE	SHE						9993	9993	9993							
										9992	9992	9992								
										9991	9991	9991								

TRIANGULATION NET HVERFLISFLJOT 1978

## INPUT STKII

## APPROXIMATE COORDINATES

Vehicle	Lat	Long	Alt	Lat	Long	Alt
203	400402.70	520404.00	1091.79	*16V	SI	CS69
5276	390306.61	508147.77	830.09	*36V	BL	OS69
2004	288505.20	568870.10	1220.6	*1BV	KFF	
1603	367343.42	528360.12	935.74	*3HV	SI	OS69
23	38831.30	476254.40	766.6	*2BV	LG	OS69
2159	381606.24	546993.75	1189.34	*2BV	H6	CS69
26	377755.70	501525.70	3769.	*2BV	KB	
27	360177.60	515052.70	414.7	*2BV	SHE	OS69
35	323799.00	537189.60	221.3	*2BV	HH	OS69
5284	382978.56	533673.94	744.64	*2B	HBB	OS69
30	347960.44	533177.40	*		KFE	
5627	395830.14	495638.23	*		RHL	
5831	374900.35	516411.48	*		GLH	
5246	364931.34	563016.75	*		SWF	
5830	364731.31	539341.31	*		KH	
5235	364577.29	505565.83	*		KEK	

SVEINSTINDUR  
 BLÆNGUR  
 RAUDFOSSAFJALL  
 SJATINDUR  
 LUMAGNUPUR  
 HABARMUR • VÄRDA  
 KALDBAKUR  
 SKALARFJALL  
 HJÖRLEIFSHÖFDI  
 HERDUBREIDARHALS

UKIANGULATIÖDE NEL HVERFISFLJÓT 1975

ADJUSTED COORDINATES

CORRECTION	MEAN ERROR	NUMBER	Y-NORTH	X- WEST
-C. 137	-0. 045	0. 196	0. 134	30
C. 032	-0. 014	0. 135	0. 045	5327
C. 151	0. 142	0. 112	0. 121	5331
-C. 233	-0. 028	0. 063	0. 223	5246
C. 225	-0. 132	0. 035	0. 219	5330
C. 352	-0. 162	0. 183	0. 219	5235
MAX. ERR.		0. 223	MAX. ERR.	0. 223
ERROR IN DIRECTION		3. 036 SEC	9. 371 SEC	

## TAKEN ON LATITUDE 51° HVERFJELL 1973

## ADJUSTED DIRECTIONS AND DISTANCES

STAT	NUMB	GRADS	ERROR	NAME	D	M	SEC	NUMB	DISTANCE	NAME
------	------	-------	-------	------	---	---	-----	------	----------	------

5351	26	138.11399	-0.83	GLH	169	13	9.3	23	15352.80	KB
5235	26	142.11384	3.14	KBK	218	48	3.8	5235	16483.47	KBK
27	294.14314	-1.81	SHE	264	43	45.8	27	14791.50	SHE	
5350	573.40560	-0.80	KH	336	4	7.3	5330	25065.76	KH	
1603	52.71726	0.11	GT	47	26	43.9	1603	17697.60	GT	
5235	27	376.71097	1.53	KBK	339	2	23.5	27	12300.51	SHE
5351	43.11126	5.49	SLH	33	48	0.0	5351	16483.47	GLH	
26	110.71306	-7.02	KB	99	38	45.5	26	13368.06	KB	
5351	23	227.67164	3.92	KHL	204	54	10.1	23	21370.84	LG
26	319.40847	-18.07	LG	287	23	3.4	26	18947.29	KB	
2031	345.76380	-11.92	SLH	314	47	35.9	5331	29484.48	GLH	
5235	2.42220	0.82	BL	2	10	47.9	5298	12518.62	BL	
200	11.62100	1.24	ST	10	27	32.0	200	25184.35	ST	
27	ECC	1.069	3.760	SHE	326	0	27.5	30	21855.33	RFE
30	362.23071	-4.00	RFE	10	36	56.2	5830	24707.81	KH	
5350	111.79574	20.00	KH	84	44	33.7	5831	14790.09	GLH	
5351	94.15555	-8.61	SLH	159	3	10.0	5235	12304.04	KBK	
5235	176.72550	-8.06	KBK							
5351	ECC	2.737	2.578	GLH	336	2	36.1	5830	25034.51	KH
5350	373.46066	7.54	KB	12	21	0.9	9199	31304.28	HB	
5152	13.72249	-9.86	HB	47	26	44.5	1603	17693.84	GT	
1603	52.71743	-5.85	GT	81	6	17.5	200	25803.74	ST	
200	90.11650	1.59	ST	134	46	57.0	5827	25484.36	RHL	
5351	149.78055	1.59	KHL	169	13	51.9	26	15354.83	KB	
26	186.12712	-4.01	KE							

TRIADICULATION NET UNVERIFIED JUT 1976

ADJUSTED DIRECTIONS AND DISTANCES

SIST	JUMB	GRADS	ERROR	NAME	D	M	SEC	NUMB	DISTANCE	NAME
------	------	-------	-------	------	---	---	-----	------	----------	------

MAXIMUM RISK/OK		FIRECTION		DISTANCE		LOCATION			
		M	M	M	M	CC	CC		
5631	ECC	2.737	2.578	SLH	5830	25084.51	KH		
5630	373.40066	1.50	KH	336	38.1	17868.04	ST		
200	90.11650	-4.45	ST	61	17.5	21857.85	SHE		
5295	123.47078	7.40	BL	111	25.3	22938.61	BL		
5327	149.76055	-4.46	RHL	134	48.9.0	29484.36	RHL		
3C	5830	77.51755	-0.56	RFE	69	49.11.2	5830	17868.04	KH
27	162.24341	2.79	SHF	146	1.8.7	27	21857.85	SHE	
35	310.47571	-2.23	NH	279	25.41.3	35	24492.18	HH	
5246	ECC	-2.634	-0.377	SMF	76	6.3.7	2004	24370.22	RFF
2004	84.55670	-10.95	RFF	133	51.12.9	9199	23127.29	HB	
9179	148.72621	7.78	HB	180	28.43.6	5830	23675.59	KH	
5320	200.52198	3.17	KH						
5250	ECC	-0.044	-1.149	BL	18	28.39.3	200	12923.69	ST
200	20.53064	5.74	ST	132	10.54.4	5827	12517.47	RHL	
5327	202.42419	-5.74	RHL						
5246	2004	0.020	M	2.47	SMF	0.1988D-03	2004	24367.568	RFF
5258	5827	0.015	M	3.09	BL	0.3272D-03	5827	12518.621	RHL
5830	5246	0.012	M	1.53	KH	0.2040D-03	5246	23676.386	SMF
5630	5294	0.027	M	4.22	SHF	0.2417D-03	5294	18108.844	HBH
27	ECC	-3.550	2.263	SHF	DIST	0.2182D-03	30	21853.586	RFE
30	-0.001	M	-0.16	RFE					



## PROGRAM GTPOL

## CONFORMAL CONICAL PROJECTION

*4C7	HA	0.0	0.	343640.0	0.0	0.52 1.41			
	1.14	966304.0	-0.21	1032230.0	*	0 0	0.0	0.0	7.97 -0.32
HA	AG2	0.0	0.	691646.0	0.0	1.41 1•41			
0.59	1012148.0	0.65	988594.0	*	0 0	0.0	0.0	0.0	6.77 -0.17
AG2	7282	0.0	0.	193246.0	0.0	1.50 2•29			
1.46	1023908.0	0.58	976842.0	*	0 0	0.0	0.0	0.0	7.06 -0.03
HA	SH								
8751	3835792.0	277.	407722.0	0.0	1.41 1•41				
0.60	1020342.0	0.67	980276.0	*	0 0	0.0	446804.91	522369.88	654.75 8751
HA	SP1	2373815.0	0.	240346.0	0.0	1.41 1•20			
0.36	1045115.0	1.56	955356.0	*	0 0	0.0	445680.29	528205.59	614.41 SPI 9.41 -0.32
NK	AG8	365802.0	293.	1097452.0	0.0	1.54 1•40			
0.59	996446.0	0.67	1004698.0	*	0 0	0.0	443694.43	506348.63	953.94 AG8 7.49 -2.14
AG8	8738	0.0	0.	783943.0	0.0	1.39 1•25			
0.43	1014068.0	0.60	986770.0	*	0 0	0.0	0.0	0.0	7.08 -0.60
AG8	1149	2246508.0	290.	772348.0	0.0	1.40 1•49			
1.52	993461.0	0.59	1007336.0	*	0 0	0.0	444551.48	498673.95	1037.60 1149 7.45 -1.01
1149	SH	-21	1867288.0	0.	293322.0	0.0	1.49 1•42		
0.69	1004978.0	0.67	995620.0	*	0 0	0.0	444183.89	495764.30	1016.06 -21 7.00 -0.07
JHEI	AG7	0.0	0.	86625.0	0.0	1.28 1•37			
0.66	959350.0	0.58	1041804.0	*	0 0	0.0	0.0	0.0	10.85 -0.06
AG7	AG6	0.0	0.	559928.0	0.0	1.37 1•18			
0.99	993160.0	0.66	1007074.0	*	0 0	0.0	0.0	0.0	1.85 2.98
AG6	8690	0.0	0.	404188.0	0.0	1.18 1•84			
1.12	993692.0	1.00	1006555.0	*	0 0	0.0	0.0	0.0	831.48 8690 2.05 1.49
*205	7260	0.0	0.	0.0	0.0	0.0	0.0	0.0	582.64 7290
99.99	58504.0	99.99	58264.0	*	0 0	0.0	0.0	0.0	

## PROGRAM GTPOL

## CONFORMAL CONICAL PROJECTION

*376	AG4	0.0	0.	267176.0	0.0	1.53	1.50	0.0	0.0	650.81	AG4	6.83	-0.03		
AG4	0.62	999287.0	0.67	1001360.0	*	0	0.0	0.0	0.0	663.51	8794	7.07	-0.19		
JHEI	8794	0.0	0.	449385.0	0.0	1.50	3.58	0.0	0.0	663.51	8794	7.07	-0.19		
JHEI	2.69	998234.0	0.62	1002421.0	*	0	0.0	0.0	0.0	663.51	8794	7.07	-0.19		
AG3	0.65	998453.0	0.60	1002279.0	*	0	0.0	0.0	0.0	678.49	AG3	7.17	-0.03		
AG3	8730	0.0	0.	194270.0	0.0	1.50	1.51	0.0	0.0	650.15	8730	8.02	-0.11		
GM	1.27	1005460.0	1.50	990817.0	*	0	0.0	0.0	0.0	650.15	8730	8.02	-0.11		
GM	8849	750939.0	296.	214954.0	0.0	1.18	1.36	0.0	0.0	650.15	8730	8.02	-0.11		
ESH	0.63	1047812.0	0.54	952815.0	*	0	0.0	0.0	0.0	509677.19	678.62	8849	8.10	-0.14	
ESH	8698	0.0	0.	0.	0.0	0.0	0.0	0.0	0.0	621.03	8698				
*348	99.99	63602.0	99.99	62103.0	*	0	0.0	0.0	0.0	0.0	0.0	0.0			
UT	7298	0.0	0.	0.	0.0	0.0	0.0	0.0	0.0	0.0	580.48	7298			
UT	99.99	58270.0	99.99	58048.0	*	0	0.0	0.0	0.0	0.0	0.0	0.0			
UT	8721	703139.0	290.	239698.0	0.0	1.28	1.30	0.0	0.0	393037.65	520446.75	669.20	8721	6.97	-0.04
UT	0.57	1016986.0	0.65	983588.0	*	0	0.0	0.0	0.0	393037.65	520446.75	669.20	8722	6.97	-0.04
UT	8722	703139.0	290.	239698.0	0.0	1.28	1.30	0.0	0.0	393037.65	520446.75	669.20	8722	6.97	-0.04
RHL	0.57	1016986.0	0.65	983588.0	*	0	0.0	0.0	0.0	394144.52	495568.66	534.87	1165	6.83	-0.01
BL	1165	697030.0	0.	170210.0	0.0	1.59	1.50	0.0	0.0	395830.45	495638.20	760.24	RHL	6.89	-0.90
BL	0.69	1085010.0	1.06	915636.0	*	0	0.0	0.0	0.0	0.0	0.0	0.0			
UT	1.13	1004097.0	1.51	996992.0	*	0.381892	115.0	0.0	0.0	439.74	8784	6.97	-0.70		
GLH	8784	0.0	0.	974092.0	0.0	1.28	1.41	0.0	0.0	0.0	0.0	0.0			
GLH	0.66	1019579.0	0.65	981376.0	*	0	0.0	0.0	0.0	439.74	8784	6.97	-0.70		
GLH	1070	0.0	0.	820978.0	0.0	1.47	1.27	0.0	0.0	472.94	1070	6.79	-0.26		
GLH	0.58	1013822.0	0.68	987003.0	*	0	0.0	0.0	0.0	0.0	0.0	0.0			

## PROGRAM GTPOL

## CONFORMAL CONICAL PROJECTION

GLH	G141	0.0	0.	480466.0	0.0	1.47	1.02	0.0	0.0	413.19	G141	6.87	-0.13	
0.42	1031169.0	0.68	969436.0	*	0	0	0.0	0.0	0.0	0.0	413.19	G141	6.87	-0.13
C889	M6	0.0	0.	416720.0	0.0	1.37	1.47	0.0	0.0	0.0	596.65	M6	7.69	-0.38
0.59	1001420.0	0.60	999240.0	*	0	0	0.0	0.0	0.0	0.0	596.65	M6	7.69	-0.38
M6	M7	0.0	0.	478712.0	0.0	1.47	1.45	0.0	0.0	0.0	565.61	M7	6.77	-0.08
0.63	1004446.0	0.59	996193.0	*	0	0	0.0	0.0	0.0	0.0	565.61	M7	6.77	-0.08
M7	1264	0.0	0.	348496.0	0.0	1.51	1.41	0.0	0.0	0.0	501.12	1264	6.88	-0.07
0.59	1012102.0	0.63	988514.0	*	0	0	0.0	0.0	0.0	0.0	501.12	1264	6.88	-0.07
1264	M8	0.0	0.	264156.0	0.0	1.41	1.54	0.0	0.0	0.0	524.96	M8	7.03	-0.06
0.64	994558.0	0.59	1006093.0	*	0	0	0.0	0.0	0.0	0.0	524.96	M8	7.03	-0.06
M8	M9	0.0	0.	395488.0	0.0	1.54	1.38	0.0	0.0	0.0	433.83	M9	6.54	0.02
0.64	1014581.0	0.63	985614.0	*	0	0	0.0	0.0	0.0	0.0	433.83	M9	6.54	0.02
M9	M10	0.0	0.	353644.0	0.0	1.38	1.47	0.0	0.0	0.0	387.16	M10	6.64	-0.01
0.56	1008699.0	0.64	991897.0	*	0	0	0.0	0.0	0.0	0.0	387.16	M10	6.64	-0.01
M10	M11	0.0	0.	233216.0	0.0	1.47	1.36	0.0	0.0	0.0	362.06	M11	6.13	0.05
0.60	1007178.0	0.56	993460.0	*	0	0	0.0	0.0	0.0	0.0	362.06	M11	6.13	0.05
M11	M12	0.0	0.	225384.0	0.0	1.36	1.40	0.0	0.0	0.0	189.25	M12	5.13	0.15
0.55	1049163.0	0.60	951438.0	*	0	0	0.0	0.0	0.0	0.0	189.25	M12	5.13	0.15
M12	M13	0.0	0.	285240.0	0.0	1.50	1.37	0.0	0.0	0.0	290.07	9702	6.12	0.08
0.57	977812.0	0.63	1022783.0	*	0	0	0.0	0.0	0.0	0.0	290.07	9702	6.12	0.08
M12	M13	0.0	0.	280710.0	0.0	1.50	1.50	0.0	0.0	0.0	206.58	M13	5.18	0.22
0.62	996362.0	0.63	1004220.0	*	0	0	0.0	0.0	0.0	0.0	206.58	M13	5.18	0.22
M13	3379	0.0	0.	237442.0	0.0	1.50	0.68	0.0	0.0	0.0	119.10	3379	4.66	0.22
-0.25	1023599.0	0.62	976627.0	*	0	0	0.0	0.0	0.0	0.0	119.10	3379	4.66	0.22
5811	G12	0.0	0.	297496.0	0.0	2.71	1.36	0.0	0.0	0.0	94.79	G12	8.25	-0.29
0.57	995826.0	1.83	1004844.0	*	0	0	0.0	0.0	0.0	0.0	94.79	G12	8.25	-0.29

PROGRAM GTPOL

CONFORMAL CONICAL PROJECTION

DONGAN STANZI

21	2019	6. 500	448639.35	510449.24	1269.00	*2PV	R65		
20	347969.30	533177.36	342.30	*3B	0S78	RJUPNAFELL			
596	392642.56	522810.27	732.04	*3Q	UXATINDAR	Y69	DS69		
32	332776.20	514883.50	31.60	*3AV	TYK	DYKKVIBER			
0	0.0	0.0	582.83		7282				
0	446394.91	522369.88	654.75		8751				
0	0.0	0.0	786.03		8738				
0	444551.48	498673.95	1037.60		1149				
0	0.0	0.0	831.48		8690				
0	0.0	0.0	592.64		7290				
0	0.0	0.0	663.51		8794				
0	0.0	0.0	650.15		8730				
0	0.0	0.0	678.62		8849				
0	0.0	0.0	621.03		8698				
0	0.0	0.0	530.48		7298				
0	393037.65	520446.75	669.20		8721				
0	393037.65	520446.75	669.20		8722				
0	394144.52	495568.66	534.87		1165				
0	0.0	0.0	439.74		8784				
0	0.0	0.0	472.94		1070				
0	0.0	0.0	501.12		1264				
0	0.0	0.0	290.07		9702				
0	0.0	0.0	51.29		1292				
0	370350.40	497809.21	30.37		1173				
0	0.0	0.0	58.12		1100				
0	347422.69	540328.74	279.58		1272				
0	344779.61	500695.74	9.76		1181				
0	0.0	0.0	60.67		9696				
0	336634.71	520529.73	34.28		1105				
0	227203.27	508905.50	11.26		1299				
0	321353.27	533014.73	5.72		9691				

SOCIAL STRUCTURE



REVIEWS

96.91	-2.09	9.7	0.0	0.0
99.92		0.0	0.0	0.0



## APPENDIX E

### COMPUTER INPUT/OUTPUT IN INCREMENT 5

Program GTPOL (1 page):  
Polar measurements in Increment 5.

Program GTAUXIL (1 page):  
Picture points in Increment 5.

## PROGRAM GTPÜL

## CONFORMAL CONICAL PROJECTION

		INCREMENT 5			
		F/M X57 OS67			
		PRAMARHAUGUR			
		SKEGGJASTADAFJALL V			
		FRIDMUNDARVÖTN OS77			
001	c.600				
5C11	540646.57	583634.86	491.15	*2B	THH
5012	557563.67	585055.97	517.20	*2B	SKG
5210	534561.40	588388.72	511.80	*3B	FMV
9999					
9999					
SKG	THH				
5853	806486.0	314.	255251.0	0.0	1.19 1.34
0.67	1085571.0	0.71	914919.0	.	0 0.0
5853	SKG				
2131	401540.0	320.	179612.0	0.0	1.34 1.52
0.72	1017297.0	0.68	983371.0	.	0 0.0
FMV	THH				
2085	2580645.0	314.	229124.0	0.0	1.43 1.40
0.67	1023452.0	0.60	977125.0	.	0 0.0
9999					

